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Final Report: Measuring and Modeling Deformation at a Geothermal Site in Utah Selected for the DOE FORGE Program

Kurt Feigl and Sam Batzli

1 Abstract

This report describes research activities between August 16th, 2018 and July 30th, 2024 under Subaward Agreement between the University of Utah and the University of Wisconsin System. The goals of the research activities are to conduct: InSAR analysis (Subtask 3.7.3) and Ground Surface Deformation Modeling (Subtask 3.4.4). Interferometric Synthetic Aperture Radar (InSAR) data have been obtained from two satellite missions, combined pair-wise into interferograms to assess ground deformation. The results are registered ("geo-coded") into a cartographic map projection and published on the Geothermal Data Repository. Time series of displacement inferred from InSAR data are compared with those measured by GPS surveying. The InSAR data analyzed here do not show any measurable deformation in the area immediately surrounding the FORGE wells. Nor do the time series of vertical displacement measured by GPS show any signals that would reject the null hypothesis of no internal deformation with 95 percent confidence. No vertical surface displacement that could be measurable by InSAR or GPS is expected from the stimulation experiments conducted at the Utah FORGE site in 2023 or 2024. The expected vertical displacement at the Earth's surface is less than 1 millimeter, based on modeling using an analytic solution (Mogi). Hydromechanical modeling in a poroelastic medium conducted using the finite-element method also indicates vertical surface displacements smaller than 1 millimeter in magnitude. In other words, the magnitude of the deformation produced by injection experiments is too small to be measured by InSAR or GPS. A seismic event with magnitude $M \sim 4$, however, would likely produce measurable deformation, depending on depth and focal mechanism.

2 Introduction

The scientific rationale and results of the FORGE project are described elsewhere, [e.g., *Simmons et al.*, 2019]. Here we focus on measuring and modeling deformation at the Utah FORGE site (*Figure 1*). The goals of the research activities are to conduct: InSAR analysis (Subtask 3.7.3) and Ground Surface Deformation Modeling (Subtask 3.4.4).

3 InSAR analysis (Subtask 3.7.3)

3.1 Objective from statement of work

Under this subtask, the Recipient is to obtain and interpret Interferometric Synthetic Aperture Radar (InSAR) interferograms to assess ground deformation and to complement continuous GPS monitoring. Additional scenes will be acquired from several satellite missions as available. The new scenes will be compared with previous scenes in interferometrically compatible combinations. The InSAR results will be evaluated to estimate ground deformation. Hydromechanical modeling in a poroelastic medium will be conducted. The InSAR data will be

analyzed and interpreted, and the results registered ("geo-coded") and integrated into the earth model.

3.2 Methodology

To measure deformation at the Utah FORGE site, we use InSAR — Interferometric Synthetic Aperture Radar. We have collected and analyzed SAR data covering the Utah FORGE site (Figure 1), especially FORGE wells 58-32, 68-32, and 78-32 (Table 1). The data sets spanning late 2019 through March 2024 were acquired by two independent satellite missions: TSX and S1.

The TSX data set consists of SAR images acquired by TerraSAR-X and TanDEM-X satellite missions operated by the German Space Agency (DLR). The images acquired on individual dates are listed in *Table 4*. Synthetic Aperture Radar data from the TerraSAR-X and the TanDEM-X satellite missions operated by the German Space Agency (DLR) were used under the terms and conditions of Research Project RES1236. DLR charges a fee of 200 EUR for one scene as the cost of fulfilling user requests (COFUR) under the "general science" category.

Interferometric pairs (interferograms) were created using GMT-SAR processing software [Sandwell et al., 2011]. Software is available publicly on GitHub for the General Inversion of Phase Technique (GIPhT) [*Feigl et al.*, 2019], the PoroTomo project [*Reinisch and Feigl*, 2018], and the UW Madison HTCondor InSAR Workflow [*Reinisch et al.*, 2018a]. We have analyzed TSX data from 2019 through 2024. The interferometric pairs from TSX data are publicly available as data sets on the Geothermal Data Repository:

Utah FORGE InSAR Data from 2020

Utah FORGE InSAR Data from 2021

Utah FORGE InSAR Data from 2022

Utah FORGE: InSAR Data Best Pairs

Utah FORGE: Interferometric Synthetic Aperture Radar Data from 2023 and 2024

The S1 data set includes SAR data from the SENTINEL-1 satellite mission operated by the European Space Agency (ESA). The SENTINEL-1 mission currently includes two spacecraft in orbit: SENTINEL-1A and SENTINEL-1B. These data sets cover the Utah FORGE site from late 2016 through early 2024. The SAR sensor aboard the Sentinel-1B spacecraft did not acquire any InSAR data covering the Utah FORGE site after December 2021. "Sentinel-1B experienced an anomaly which rendered it unable to deliver radar data in December 2021" [*ESA*, 2022] https://www.eoportal.org/satellite-missions/copernicus-sentinel-1]. On the other hand, Sentinel-1A acquired SAR data covering the Utah FORGE site in 2023 and 2024. To analyze the Sentinel data, we use ASF HyP3, the Alaska Satellite Facility's Hybrid Pluggable Processing Pipeline [*ASF*, 2024], which became available as a service in April 2024. The S1 pairs analyzed between 2020 and 2024 are listed in *Table 5* and *Table 6* for Sentinel-1A and Sentinel-1B, respectively.

3.3 Time series analysis

We have calculated many different interferometric pairs. We analyze the interferometric pairs as time series of displacement using the Miami INsar Time-series software in PYthon (MintPy) workflow (Yunjun et al., 2019). The MintPy workflow partially mitigates atmospheric effects and topographic artefacts.

For each data set, we show a graph of the relative positions of TSX/TDX spacecraft at the times that individual SAR images were acquired (circles) as well as the separation ("perpendicular baseline", left-hand scale) between two different positions (at different times) in the orbital trajectory. Each interferometric pair is shown as line segment, colored by average spatial coherence (right hand scale) in a so-called "network diagram" (*Figure 2, Figure 5, Figure 9,* and *Figure 14*).

The quantity of interest is the (scalar) displacement along the radar line of sight (LOS). By convention, positive values of LOS displacement correspond to motion toward the satellite. For example, *Figure 3* shows a sequence of maps of the LOS displacement at dates between 2019 and 2023.

To visualize the deformation field, we consider the mean rate of LOS displacement over the full, multi-year time interval spanned by the data. Each map in *Figure 4*, *Figure 10*, *Figure 12*, *Figure 15*, and *Figure 8* shows the mean rate of LOS displacement averaged over the time interval shown in the network diagram. In each figure, the rate is referred a reference pixel.

3.4 GPS

Here we consider the vertical component of displacement measured by GPS and provided by Ben Erickson:

Sent: Monday, May 13, 2024 8:47 AM; Subject: Re: GPS Monument Data

I've attached the most recent GPS processing; keep in mind, the comparative initial date has changed from the referenced spreadsheet. I also maintain the Foundry site with this spreadsheet, the comparative time series, and raw GPS data.

Ben Erickson (he/him); Senior Geologist | M.S., P.G

To mitigate the effects of changing reference frames, we analyze the GPS time series of vertical displacement with respect to several different references. This approach would highlight any internal deformation within the GPS network.

Figure 17 shows the relative vertical displacement of each station with respect to the continuously operating station GDM-01. Although there is a suggestion of a seasonal effect (upward displacements during the winter and downward displacements during the summer), there is no significant vertical displacement between the surveys bracketing the date of the flow test in 2023.

Figure 18 shows the vertical displacement of each station referred to the overall mean of all stations. No individual station appears to deviate consistently from the 95-percent confidence interval.

Figure 19 shows the vertical displacement of each station referred to the mean of all stations for each survey. This figure does not show any vertical displacements that would reject the null hypothesis of no deformation with 95% confidence.

3.5 Discussion

The InSAR data do not show any deformation that is obviously associated with FORGE wells 58-32, 68-32, or 78-32, shown as triangles in the figures. The large-scale patterns are probably the result of atmospheric effects that are partially correlated with topography. The wide-scale patterns are probably the result of unmodeled orbital effects in the satellite trajectories. Nor do the time series of vertical displacement measured by GPS show any signals that would reject the null hypothesis of no internal deformation with 95 percent confidence.

4 Ground Surface Deformation Modeling (Subtask 3.4.4).

4.1 Objective from amended statement of work

The Recipient will model ground surface deformation for comparison with InSAR data. The deliverable will be in the form of a report that makes comparison of modeled results with other monitoring techniques used at Utah FORGE such as GPS surveys and strain measurements. It will make reference to analogous injection-production fields elsewhere in the world.

4.2 Analytic modeling configuration

To calculate the order of magnitude of the displacement at the Earth's surface, we performed forward modeling using a simple model [*Mogi*, 1958]. This model assumes an inflating sphere buried in a half space with uniform elastic properties. The Mogi model expresses vertical displacement u_z of a point on the ground in terms of the volume change ΔV and depth d of a subsurface source, as shown in the following equation from [Segall, 2010].

$$u_{z} = \frac{(1-\nu)\Delta V}{\pi} \frac{d}{(\rho^{2}+d^{2})^{3/2}},$$

where ΔV is the injected volume, u_z is vertical displacement, v is Poisson's ratio (here assumed to be ¹/₄), d is depth, and ρ is radial horizontal distance from center of source to observation point [*Segall*, 2010]. Vertical displacement u_z is a linear function of the volume ΔV injected at depth. In contrast, displacement u_z is a non-linear function of depth d.

For simplicity, we use an (X,Y) coordinate system with an origin centered on the toe of Well 16A(78)-32. To estimate the depth of the volume change, we followed the document entitled *End* of Job Report Hydraulic Fracturing of Well 16A(78)-32 (April 2022) prepared by Kevin England and John McLennan which reports the following information.

[&]quot;The bit was run to near the end of the open-hole section of the wellbore (10,951 ft MD) while the casing scraper reached a depth of 10,761.62 ft MD within the cased-hole and ensured the absence of debris. The drift sub was run one joint above the casing scraper and reached a depth of 10,726.07 ft MD which assured that there is adequate clearance to run the bridge plug to the maximum planned depth of 10,670 ft MD.

There were some tight spots in the open-hole ($\sim 10,857 - 10,872$ ft MD) which were worked through with the bit by rotation and washing down." [*McLennan*, 2022].

To estimate the total volume for the 2023 and 2024 tests at the Utah FORGE site, we considered the details described in the following two sub-sections.

4.2.1 Modeling details - 2023

For the 2023 circulation tests, we follow Munday et al. (2024):

Two sets of circulation tests were performed in July 2023 to test connectivity between wells 16A and 16B. A comprehensive analysis of the circulation tests is given by Xing et. al. (2024). In this work we use pressure and mass data from the second set of circulation tests performed on July 18 and 19 to fit our THM model. Wellhead pressure, injection rate, and producing rate for the July 18 and 19 tests are given in Figure 3. The injection rates range from 2.5 to 7.5 bpm with a maximum pressure of 4500 psi during the July 18 circulation test. Injection well 16A contains three frac stages spaced approximately 300 feet apart where the bottom stage 1 is 200 ft of open hole at a depth of 10938 ft and stages 2 and 3 are cased and perforated. The flow rate for the July 18 and 19 The flow is partitioned between the three stages and the open hole stage 1 zone receives approximately 50% of the flow for the July 19 tests (Xing et al, 2023).

We calculated the total volume of injected fluid by visually estimating the mean flow rate at approximately 5 barrels per minute and then integrating with respect to time over the 4-hour duration for each of the two tests, as shown in *Figure 21*. Assuming that a barrel is 0.159 m³, we find a total change in volume of $\Delta V = 382$ m³ for the circulation tests in 2023.

4.2.2 Modeling details - 2024

For the 2024 test, we refer to the following message from Kevin England, dated May 9, 2024:

Subject: Fluid volumes pumped into well 16A(78)-32 during the frac stimulation treatments Please see below the actual volumes of fluid that were pumped for each of the frac stages in well 16A. We just received all of the data files from Calfrac and I will confirm all of this in the next few days. I'm pretty sure there is additional volume pumped in stage 6R after we perforated an additional 3 ft of zone (probably close to 3,000 bbl). The total fluid injected is 110,776 bbl (4,652,592 gal).

Assuming that a barrel is 0.159 m³, we find a total change in volume of $\Delta V = 18,000$ m³ for the stimulation treatments in 2024.

4.3 Analytic modeling results

We consider six different cases, as listed in Table 2.

The first two cases approximate the stimulations in July 2023 and April 2024, respectively. As shown by solid curves in *Figure 20*, the simulated ground motion forms small bulge of uplift. The maximum values of vertical displacement are 8 micrometer and 4 micrometer, respectively. These values are considerably smaller than the detection limit of 10 millimeters for InSAR.

We also consider three hypothetical cases with large modeled injection volumes (dotted curves). In Case 3, the vertical displacement u_z of 8 mm approaches the detection limit of 10 mm. Cases 4 and 5 consider injection volumes of the same order of magnitude (in absolute value) of the annual rate of net production at a commercial operation. For context, pumping at 500 GPM for 1 year is approximately equivalent to $\Delta V \sim 10^6$ m³. The values of u_z in Cases 4 and 5 are 80 mm and 800 mm, respectively. In other words, if injection at the same rate as during the 2023 FORGE tests were to continue for a year, then the surface displacement would be measurable by InSAR.

The deformation in Case 4 is similar to that observed at East Mesa in California [*Eneva et al.*, 2012; *Han et al.*, 2011; *Massonnet et al.*, 1997; 1998; *Taylor et al.*, 2013].

To illustrate the non-linear trade-off between depth d and volume change ΔV , we consider another hypothetical case (numbered 6) with a shallow depth d = 500 m and $\Delta V = 18,000$ m³ (just as in Case 2). Case 6 would produce 20 mm of vertical displacement at the surface (dark blue dotted curve).

4.4 Simulating vertical displacements using the Finite Element Method

To confirm the order of magnitude of the surface deformation expected from the stimulation experiments in July 2023 and April 2024, we apply the finite element method (FEM) to perform numerical simulations. The FEM model applies the poroelastic theory of Biot as implemented using COMSOL Multiphysics [*COMSOL*, 2024b]. This approach has been validated against the analytic solution of Terzhagi [*COMSOL*, 2024a].

In particular, we use a model developed by Larry Murdoch as Milestone 5.1 of FORGE Project 3-2514. The following description is adapted from e-mail communications with Murdoch. As shown in Figure 22, the mesh for the FEM model is symmetric about the left side. The simulated region is below the dark grey patch on the left side. This simulation treats the fracture as a permeable layer that is inflated by injecting fluid. The modulus of the layer currently is small, which would represent an open fracture, like a Mode I fracture.

This model does not include the non-linear effects related to propagation, so it cannot match the pressure history (pressure increases early and then decreases). However, it should be able to match the maximum pressure and injected volume, and the length and orientation of the fracture can be adjusted based on the microseismic interpretations. That should allow the model to predict the magnitudes and patterns of the far field deformation fairly well.

Figure 23 shows the vertical component of displacement along a profile from the center of the field to the eastern side. Each curve shows the displacement accumulated at a time step ranging from the start of injection to a time some 2.5 hours later. The maximum displacement is less than 11 micrometers, the same order of magnitude as calculated using the analytic model. *Figure 24* shows the vertical displacement field in map view.

5 Conclusions

In summary, the InSAR data analyzed do not show any measurable deformation in the area immediately surrounding the FORGE wells. Nor do the time series of vertical displacement measured by GPS show any signals that would reject the null hypothesis of no internal deformation with 95 percent confidence.

No deformation larger than 1 millimeter is expected from the stimulation experiments. This result is not surprising since the stimulation experiments injected relatively small volumes at depths on the order of ~ 2000 m. The expected deformation is less than 1 mm, i.e., based on the modeling using both an analytic solution (Mogi) and the finite element method. In other words, the magnitude of the deformation produced by injection experiments is too small to be measured by

InSAR. A seismic event with magnitude $M \sim 4$, however, would likely produce measurable deformation, depending on depth and focal mechanism.

6 Acknowledgments

Interferograms were created using GMT-SAR processing software [*Sandwell et al.*, 2011]. Several figures were created using the Generic Mapping Tools [*Wessel et al.*, 2013].

Software is available publicly on GitHub for the General Inversion of Phase Technique (GIPhT) [*Kurt L. Feigl et al.*, 2019] and the FringeFlow workflow for generating interferometric fringe patterns from synthetic aperture radar data, both developed at UW Madison [*K. L. Feigl et al.*, 2022].

Synthetic Aperture Radar data from the TerraSAR-X and the TanDEM-X satellite missions operated by the German Space Agency (DLR) were used under the terms and conditions of Research Project RES1236.

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8 Figures



Figure 1. West-southwest facing view of the Utah FORGE site in late 2020, showing drill pads, wells, power line supply, and site access. Well 58-32 is the deep pilot well that can be used to deploy downhole instruments during 2021 stimulations; the bottom 200 feet of the hole are open and the rest is lined with 7-inch casing. Well 68-32 is dedicated to seismic monitoring with a permanently installed geophone and accelerometer at depths of 921-925 ft. Well 78-32 is instrumented with a Silixa DAS cable including a Constellation fiber cemented in the annulus of the 5 $\frac{1}{2}$ " casing to 3268 ft; downhole instruments can be deployed in the casing. Well 56-32 has been drilled to 9,145 feet depth, and it is lined with 5 $\frac{1}{2}$ " casing to the toe; this well is also available for deployment of downhole instruments. Figure and caption [https://utahforge.com/site-operations/].

Table 1. Final coordinates of wells, downloaded from Hardwick, Christian. 2020. "Utah FORGE: Updated Phase 2C Well Location Coordinates". United States. <u>https://gdr.openei.org/submissions/1268</u>. File name is "Updated Utah FORGE Phase 2C Well Location"

			UTM	UTM	Elevation	h_prec	z_std
Well	Latitude (deg)	Longitude (deg)	Northing (m)	Easting (m)	(m)	(m)	(m)
58-32	38.500536	-112.887016	4263037.084	335451.380	1684.801	0.100	0.038
68-32	38.501553	-112.886647	4263155.286	335485.169	1685.667	0.100	0.030
78-32	38.500147	-112.883224	4262993.139	335780.484	1701.919	0.100	0.031



Figure 2. Plot of relative positions of TSX/TDX spacecraft at the times that individual SAR images were acquired in (descending) Track 30 (circles) as well as the orbital separation ("perpendicular baseline", left-hand scale) between two positions forming an interferometric pair (line segments, colored by average spatial coherence (right hand scale). smb://research.drive.wisc.edu/feigl/insar /FORGE/TSX/T30 /feigl_20231222/MINTPY/pic/network.pdf



Figure 3. Map of LOS displacement at the dates shown in the previous figure, after accounting for the atmospheric effects and topographic artefacts. Black square indicates the reference location where rate of LOS displacement is zero. In each panel, the black square indicates the reference location where rate of LOS displacement is zero. The spatial extent of each panel matches that shown in the following figure. [smb://research.drive.wisc.edu/feigl/insar/FORGE/TSX /T30/feigl 20231222/MINTPY/pic/timeseries tropHgt demErr wrap10.png]



Figure 4. Map of mean rate of LOS displacement averaged over the time interval [2019/02/11 through 2023/10/13]. Coordinates are longitude and longitude in degrees, respectively. Triangles indicate locations of wells 58-32, 68-32, and 78-32. smb://research.drive.wisc.edu/feigl/insar/FORGE/TSX/T30/feigl_20231222/MINTPY/pic/avgPhaseVelocity.png



Figure 5. Plot of relative positions of TerraSAR-X and TANDEM-X spacecraft at the times that individual SAR images were acquired (circles) as well as the orbital separation (left-hand scale) between two positions forming an interferometric pair (line segments, colored by average spatial coherence (right hand scale). smb://research.drive.wisc.edu/feigl/insar/ FORGE/TSX/T30/forge 2024/MINTPY6/pic/network.pdf



Figure 6. Map of LOS displacement at the dates shown in the previous figure, after accounting for atmospheric effects and topographic artefacts. Black square indicates the reference location where rate of LOS displacement is zero. In each panel, the black square indicates the reference location where rate of LOS displacement is zero. The spatial extent of each panel matches that shown in the following figure. [smb://research.drive.wisc.edu/feigl/insar/FORGE/TSX/T30/ forge_2024/MINTPY6/pic/timeseries_tropHgt_demErr_wrap10.png]



Figure 7. Map of mean rate of LOS displacement averaged over the time interval from 2023/05/01 through 2024/06/22 X and Y coordinates are longitude and longitude in degrees, respectively. Negative values of LOS displacement rate indicate motion away from the satellite. Triangles indicate locations of wells 58-32, 68-32, and 78-32. smb://research.drive.wisc.edu/feigl /insar/FORGE/TSX/T30/ forge_2024/MINTPY6/velocitymapv2_1 velocity.png



Figure 8. Time series of LOS displacement maps.. Black square indicates the reference location where rate of LOS displacement is zero. The spatial extent of each panel matches that shown in the previous figure.



Figure 9. Plot of relative positions of Sentinel 1-A and Sentinel 1-B spacecraft at the times that individual SAR images were acquired (circles) as well as the orbital separation (left-hand scale) between two positions forming an interferometric pair (line segments, colored by average spatial coherence (right hand scale). smb://research.drive.wisc.edu/feigl/insar/ FORGE/SDK/FORGE_DESCENDING2/pic/network.pdf



Figure 10. Map of mean rate of LOS displacement averaged over the time interval shown in previous figure, displayed with respect to its median value. X and Y coordinates are UTM easting and northing in km, respectively. Triangles near (E,N) = (335,4263) km indicate locations of wells 58-32, 68-32, and 78-32. Pixels with LOS displacement rates that less than twice their estimated standard deviation in absolute value are not shown. Blue trapezoid indicates bounding box of study area.



Figure 11. Map of estimated standard deviation of the mean rate of LOS displacement averaged over the time interval shown in previous figure. Plotting conventions as in previous figure.



Figure 12. Enlarged map of mean rate of LOS displacement averaged over the time interval shown in previous figure, displayed with respect to its median value. X and Y coordinates are UTM easting and northing in km, respectively. Triangles near (E,N) = (335,4263) km indicate locations of wells 58-32, 68-32, and 78-32. Pixels are approximately 80 m by 80 m. Pixels with LOS displacement rates that less than twice their estimated standard deviation in absolute value are not shown.



Figure 13. Enlarged map of estimated standard deviation of the mean rate of LOS displacement averaged over the time interval shown in previous figure. Plotting convention as in previous figure.



Figure 14. Plot of relative positions of Sentinel-1A spacecraft at the times that individual SAR images were acquired (circles) as well as the orbital separation ("perpendicular baseline", left-hand scale) between two positions forming an interferometric pair (line segments, colored by average spatial coherence (right hand scale). smb://research.drive.wisc.edu/feigl/ insar/FORGE/SDK/FORGE_ASCENDING/pic/network.pdf



Figure 15. Map of mean rate of LOS displacement averaged over the time interval shown in previous figure, displayed with respect to its median value. X and Y coordinates are UTM easting and northing in km, respectively. Triangles indicate locations of wells 58-32, 68-32, and 78-32. Pixels are approximately 80 m by 80 m. Pixels with LOS displacement rates that less than twice their estimated standard deviation in absolute value are not shown. Blue trapezoid indicates bounding box of study area.



Figure 16. Map of estimated standard deviation of the mean rate of LOS displacement averaged over the time interval shown in previous figure. Plotting convention as in previous figure.



Figure 17. Time series of relative vertical displacements referred to station GDM-01. Error bars delimit ± 2 standard deviations, i.e. 95 percent confidence. Vertical dashed lines indicate tests in July 2023 and April 2024.



Figure 18. Time series of vertical displacements referred to the initial position of each station at the time of the first survey. Thick black lines delimits interval of 95% confidence about the mean for each campaign. Vertical dashed lines indicate tests in July 2023 and April 2024.



Figure 19. Time series of vertical displacements referred to both the mean of the campaign and the mean for each station. Thick black lines delimits interval of 95% confidence about the mean for each campaign. Vertical dashed lines indicate tests in July 2023 and April 2024.

Table 2. Values of parameters in Mogi model

Case			depth		Volu	me	Change	e	Equivalent			Equivalen		
			(meter)		(cub	ic	meter)	seismic			seismic		
									mome	nt		mag	ni	tude
									M ₀ [N	.m]*		Mw		
case	=	1	depth =	3334 n	n DV =	3	.8E+02	m^3	м0 =	1.1E+13	N.m	Mw	=	2.7
case	=	2	depth =	3334 n	n DV =	: 1	.8E+04	m^3	м0 =	5.3E+14	N.m	Mw	=	3.8
case	=	3	depth =	3334 n	n DV =	3	.8E+05	m^3	м0 =	1.1E+16	N.m	Mw	=	4.7
case	=	4	depth =	3334 n	n DV =	3	.8E+06	m^3	м0 =	1.1E+17	N.m	Mw	=	5.3
case	=	5	depth =	3334 n	n DV =	3	.8E+07	m^3	м0 =	1.1E+18	N.m	Mw	=	6.0
case	=	6	depth =	500 n	n DV =	: 1	.8E+04	m^3	м0 =	5.3E+14	N.m	Mw	=	3.8

* assuming geometric potency (slip x area) equal to volume change ΔV and shear modulus of 30 GPa.



Figure 20. Plot of vertical displacement in meters calculated from the Mogi model for injected volumes approximating the stimulations in July 2023 (light blue solid line) and April 2024 (green solid line) as well as three hypothetical cases (purple, yellow, red) with different values of volume change (labels on right hand side). The dark blue curve shows a hypothetical case with a shallow depth (labels at left).



Figure 21. Circulation test 2 data showing wellhead pressure, injection rate, and producing rate for (a) July 18 and (b) July 19, 2023 (after Figure 5 in [Xing et al., 2024]). Figure and caption [Munday and Podgorney, 2024].

4

parameter	symbol	values		
fluid density	rhof	000 [kg/m^3]		
length of screened interval in well	screen_len	10 [m]		
radius of well	well_radius	0.1 [m]		
pumpingrate	pumping_rate	3E-4[m^3/s]		
gravitational acceleration	g	9.81[m/s^2]		
fracture thickness	frx_thickness	0.1 [m]		
fracture depth	frx_depth	50 [m]		
fracture dip	frx_dip	90 [m]		
property	symbol	granite	alluvium	fracture
Young's modulus	E	1E8[Pa]	1E8[Pa]	1[Pa]
permeability	k	1e-12[m^2]	1e-12[m^2]	1.5E-12[m^2]
storage (effective)	Se	1.00E-07	1.00E-07	1.00E-09
porosity	porosity	0.2	0.2	0.5
Biot coefficient	b_alpha	0.95	0.95	0.9

Table 3 Input parameters for finite-element modeling using COMSOL from L. Murdoch.



Figure 22. Block diagram for configuration of the finite element model. The model domain is symmetric about the left side and the simulated region is below the dark grey patch on the left side. The eastward X axis points toward the upper right corner of the page. The vertical Z axis points upward such that the earth surface faces the top of the page. Material properties are listed in previous table for "granite" (blue) and "alluvium" (yellow). [Larry Murdoch, Milestone 5.1 of FORGE Project 3-2514]



Figure 23. Simulated vertical displacement in micrometers at various times along a profile from west to east at Y=2 km.



Figure 24. Map view of simulated vertical component of displacement in micrometers after approximately 2.5 hours of injection. Warm colors denote positive (upward) vertical displacement.

9 Supplementary Information

Table 4. List of SAR acquisitions from TerraSAR-X and TanDEM-X radar satellite missions showing date (YearMonthDate) and orbit number. The status flags are defined as follows: "D" represents a scene that has been delivered. "C" denotes a canceled scene acquisition, usually for technical reasons at the source. "P" denotes a scene that is planned for acquisition in the future. All of these acquisitions follow Track 30 in an ascending orbital pass that crosses the equatorial plane from south to north. Earlier acquisitions are listed in previous reports. [grep forge /s12/insar/TSX/TSX_OrderList.txt | cut -c 1-78 | sort -un]

#date	site	sat	track	swath	frame	orbit	ascdes	status	source
20161108	forge	TDX	т30	strip_004	nan	35404	A	D	dlrdlr
20181115	forge	TDX	т30	strip_004R	nan	46593	A	D	dlrdlr
20190131	forge	TSX	т30	strip_004R	nan	47762	A	D	dlrdlr
20190211	forge	TSX	т30	strip_004R	nan	47929	A	D	dlrdlr
20190222	forge	TSX	т30	strip 004R	nan	48096	A	D	dlrdlr
20190418	forge	TSX	т30	strip_004R	nan	48931	A	D	dlrdlr
20190510	forge	TSX	т30	strip 004R	nan	49265	A	D	dlrdlr
20190601	forge	TSX	т30	strip_004R	nan	49599	A	D	dlrdlr
20190623	forge	TSX	т30	strip_004R	nan	nan	A	С	dlrdlr
20190715	forge	TSX	т30	strip_004R	nan	nan	A	С	dlrdlr
20200107	forge	TSX	т30	strip_004R	nan	52939	A	D	dlrdlr
20200129	forge	TSX	т30	strip 004R	nan	53273	A	D	dlrdlr
20200220	forge	TSX	т30	strip 004R	nan	53607	A	D	dlrdlr
20200302	forge	TSX	т30	strip 004R	nan	53774	A	D	dlrdlr
20200313	forge	TSX	т30	strip 004R	nan	53941	A	D	dlrdlr
20200324	forge	TSX	т30	strip 004R	nan	54108	A	D	dlrdlr
20200404	forge	TSX	т30	strip 004R	nan	54275	А	D	dlrdlr
20200415	forge	TSX	т30	strip 004R	nan	54442	А	D	dlrdlr
20200426	forge	TSX	т30	strip 004R	nan	54609	А	D	dlrdlr
20200507	forge	TSX	т30	strip 004R	nan	54776	А	D	dlrdlr
20200518	forge	TSX	т30	strip 004R	nan	54943	А	D	dlrdlr
20200529	forge	TSX	т30	strip 004R	nan	55110	А	D	dlrdlr
20200609	forge	TSX	т30	strip 004R	nan	55277	A	D	dlrdlr
20200620	forge	TSX	т30	strip 004R	nan	55444	A	D	dlrdlr
20200701	forge	TSX	т30	strip 004R	nan	55611	A	D	dlrdlr
20200712	forge	TSX	т30	strip 004R	nan	55778	A	D	dlrdlr
20200723	forge	TSX	т30	strip 004R	nan	55945	A	D	dlrdlr
20200803	forge	TSX	т30	strip 004R	nan	56112	A	D	dlrdlr
20200814	forge	TSX	т30	strip 004R	nan	56279	A	D	dlrdlr
20200825	forge	TSX	т30	strip 004R	nan	56446	А	D	dlrdlr
20200905	forge	TSX	т30	strip 004R	nan	56613	A	D	dlrdlr
20200916	forge	TSX	т30	strip 004R	nan	56780	А	D	dlrdlr
20200927	forge	TSX	т30	strip 004R	nan	56947	А	D	dlrdlr
20201008	forge	TSX	т30	strip 004R	nan	57114	А	D	dlrdlr
20201019	forge	TSX	т30	strip 004R	nan	57281	A	D	dlrdlr
20201030	forge	TSX	т30	strip 004R	nan	57448	A	D	dlrdlr
20201110	forge	TSX	т30	strip 004R	nan	57615	А	D	dlrdlr
20201121	forge	TSX	т30	strip 004R	nan	57782	А	D	dlrdlr
20201202	forge	TSX	т30	strip 004R	nan	57949	A	D	dlrdlr
20201213	forge	TSX	т30	strip 004R	nan	58116	A	D	dlrdlr
20201224	forge	TSX	т30	strip 004R	nan	58283	А	D	dlrdlr
20210104	forge	TSX	т30	strip 004R	nan	58450	А	D	dlrdlr
20210115	forge	TSX	т30	strip 004R	nan	58617	A	D	dlrdlr
20210126	forge	TSX	т30	strip 004R	nan	58784	A	D	dlrdlr
20210206	forge	TSX	т30	strip 004R	nan	58951	А	D	dlrdlr
20210217	forge	TSX	т30	strip 004R	nan	59118	A	D	dlrdlr
20210228	forge	TSX	т30	strip 004R	nan	59285	А	D	dlrdlr
20210311	forge	TSX	т30	strip 004R	nan	59452	A	D	dlrdlr
20210322	forge	TSX	т30	strip 004R	nan	59619	А	D	dlrdlr
20210402	forge	TSX	т30	strip 004R	nan		A	С	dlrdlr
20210413	forge	TSX	т30	strip 004R	nan	59953	А	D	dlrdlr
20210424	forge	TSX	т30	strip 004R	nan	60120	А	D	dlrdlr
20210505	forge	TSX	т30	strip 004R	nan	60287	A	D	dlrdlr
20210516	forge	TSX	т30	strip 004R	nan	60454	А	D	dlrdlr
20210527	forge	TSX	т30	strip 004R	nan	60621	А	D	dlrdlr
20210607	forge	TSX	т30	strip 004R	nan		А	P	dlrdlr
20210618	forge	TSX	т30	strip 004R	nan		A	P	dlrdlr
20210629	forge	тsx	т30	strip 004R	nan	61122	A	D	dlrdlr
20210710	forge	TSX	т30	strip 004R	nan	61289	А	D	dlrdlr
20210721	forge	TSX	т30	strip 004R	nan	61456	A	D	dlrdlr
20210801	forge	тѕх	т30	strip 004R	nan	61623	A	D	dlrdlr
	-								

20210812	forge	TSX	т30	strip 004R	nan	61790	Α	D	dlrdlr
00010000		mov	m 20			C10F7		-	4141
20210823	Iorge	TSX	130	Strip_004R	nan	01921	А	D	airair
20210903	forge	TSX	т30	strip 004R	nan	62124	Α	D	dlrdlr
20210014	f	mov	m20				~	<u> </u>	
20210914	Iorge	TSX	130	Strip_004R	nan		А	C	
20210925	forge	TSX	т30	strip 004R	nan	62458	А	D	dlrdlr
00011000	£	mov	m 20			COCOF	~	D	41
20211006	Iorge	TSX	130	Strip_004R	nan	02025	А	D	airair
20211017	forge	TSX	т30	strip 004R	nan		Α	С	dlrdlr
00011000	j-							-	11 . 11 .
20211028	forge	TSX	т30	strip_004R	nan		А	C	dirdir
20211108	forge	TSX	TT30	strip 004R	nan	63126	Δ	п	dlrdlr
	rorde	1011	100	berrp_oom		00120		2	arrarr
20211119	forge	TSX	т30	strip 004R	nan	63293	А	D	dlrdlr
20211130	forde	TRY	m3 0	etrip 004P	nan	63460	A	л	dirdir
20211130	rorge	IOA	100	SCITD_004K	man	03400	A	D	arrarr
20211211	forge	TSX	т30	strip 004R	nan	80357	А	D	dlrdlr
20211222	forde	TRY	m3 0	strip 004P	nan	80524	A	л	dirdir
20211222	Torde	ISA	130	SCIIP_004K	nan	80524	A	D	arrarr
20220102	forge	TSX	т30	strip 004R	nan	80691	А	D	dlrdlr
20220112	forgo	mev	m20	atrip 004B	n . n		7	C	dl mdl m
20220115	rorge	IOA	150	SCITP_004K	man		~	C	urrarr
20220124	forge	TSX	т30	strip 004R	nan	81025	А	D	dlrdlr
20220204	forgo	mev	m20	atrip 004B	n . n	01102	7	р	dl mdl m
20220204	rorge	IOA	150	SCITP_004K	man	01192	~	Ъ	urrarr
20220215	forge	TSX	т30	strip 004R	nan	81359	А	D	dlrdlr
20220226	fordo	mev	m20	atrip 004B		61796	7	D	dindin
20220220	Torde	ISA	130	SCIIP_004K	nan	04/90	A	D	arrarr
20220309	forge	TSX	т30	strip 004R	nan	64963	А	D	dlrdlr
20220220	f	mov	m20			65120	~	P	ما امما ام
20220320	rorge	TSA	130	SCLID_004K	nan	65130	A	D	arrarr
20220331	forge	TSX	т30	strip 004R	nan	65297	А	D	dlrdlr
00000411	£	mov	m 20			CEACA	~	D	41
20220411	Iorge	TSX	130	Strip_004R	nan	05404	А	D	airair
20220422	forge	TSX	т30	strip 004R	nan	65631	А	D	dlrdlr
	j-					65 8 6 6			
20220503	forge	TSX	т30	strip_004R	nan	65798	А	D	dlrdlr
20220514	forge	TSX	T 30	strip 004R	nan	65965	Δ	п	dlrdlr
20220314	rorge	IOA	150	SCITD_004K	man	00000	A	D	arrarr
20220525	forge	TSX	т30	strip 004R	nan	66132	А	D	dlrdlr
20220605	forge	TCY	ሞጓበ	strip 004B	nan	66299	Δ	л	dlrdlr
20220005	rorge	IDA	150	SCITP_004K	man	00299	~	Ъ	urrarr
20220616	forge	TSX	т30	strip 004R	nan		А	С	dlrdlr
20220627	forgo	mev	m20	atrip 004B		66633	7	D	dindin
20220027	Torde	ISA	130	SCIIP_004K	nan	00033	A	D	arrarr
20220708	forge	TSX	т30	strip 004R	nan	66800	А	D	dlrdlr
20220710	forgo	mev	m20	at min 004B		66967	7	D	dindin
20220719	Torde	ISA	130	SCIIP_004K	nan	00907	A	D	arrarr
20220730	forge	TSX	т30	strip 004R	nan	67134	А	D	dlrdlr
20220910	forgo	mev	m20	at min 004B		67201	7	D	dindin
20220810	rorge	TSA	130	SCLID_004K	nan	6/301	A	D	arrarr
20220821	forge	TSX	т30	strip 004R	nan		А	С	dlrdlr
20220001	fordo	mev	m20	atrip 004B			7	C	dindin
20220901	Torde	ISA	130	SCIIP_004K	nan		A	C	arrarr
20220912	forge	TSX	т30	strip 004R	nan		А	С	dlrdlr
20220022	f	mov	m20			67060	~	P	ما امما ام
20220923	Iorge	TSX	130	Strip_004R	nan	6/969	А	D	airair
20221004	forge	TSX	т30	strip 004R	nan		А	С	dlrdlr
0000101F	£	mov	m 20			60202	~	2	41
20221015	Iorge	TSX	130	Strip_004R	nan	68303	А	D	airair
20221026	forge	TSX	т30	strip 004R	nan	68470	А	D	dlrdlr
00001100	~					60.607	-	-	
20221106	Iorge	TSX	130	strip_004R	nan	68637	А	D	airair
20221117	forge	TSX	т30	strip 004R	nan	68804	А	D	dlrdlr
00001100	j-					60071		-	11 . 11 .
20221128	Iorge	TSX	130	strip_004R	nan	689/I	А	D	airair
20221209	forge	TSX	т30	strip 004R	nan	69138	А	D	dlrdlr
00001000	j-					60205		-	11 . 11 .
20221220	Iorge	TSX	130	strip_004R	nan	69305	А	D	airair
20221231	forge	TSX	т30	strip 004R	nan	69472	A	р	dlrdlr
	_0_90					60 600			
20230111	forge	TSX	т30	strip_004R	nan	69639	А	Б	dirdir
20230122	forge	TSX	т30	strip 004R	nan	69806	A	р	dlrdlr
	_0_90					60000			
20230202	Iorge	TSX	130	strip_004R	nan	699/3	А	D	airair
20230213	forge	TSX	т30	strip 004R	nan	70140	А	D	dlrdlr
0000000	~					70007	-	-	
20230224	Iorge	TSX	130	strip_004R	nan	/030/	А	D	airair
20230307	forge	TSX	т30	strip 004R	nan	70474	А	D	dlrdlr
00000010	£	mov	m 20			70641	~	D	41 41
20230318	Iorge	TSX	130	Strip_004R	nan	70641	А	D	airair
20230329	forge	TSX	т30	strip 004R	nan	70808	А	D	dlrdlr
00000400	£	mov	m 20			70075	~	D	41
20230409	Iorge	TSX	130	Strip_004R	nan	10915	А	D	airair
20230420	forge	TSX	т30	strip 004R	nan	71142	Α	D	dlrdlr
20220501	fores	mov	m 2 0			71200	7	P	d] = -1 =
20230301	Torge	TOY	130	SCFIP_004R	nan	11309	А	ע	arrarr
20230512	forae	TSX	т30	strip 004R	nan	71476	А	D	dlrdlr
20220522		mov	m20			71 640	~	P	
20230323	LOLGE	TOX	130	strip_004R	nañ	/1043	А	u	arrarr
20230603	force	TSX	т30	strip 004R	nan	71810	Α	D	dlrdlr
20220614	fame	mov	m o o			71077	7	~	41-41-
20230014	Torge	TOY	130	SCFIP_004R	nan	11911	А	ע	arrarr
20230625	forge	TSX	т30	strip 004R	nan	72144	Α	D	dlrdlr
20220706	£	mov	m20			70011	~		al
20230/06	rorde	TSX	130	strip_004R	nan	12311	А	U	arrarr
20230717	force	TSX	т30	strip 004R	nan	72478	А	D	dlrdlr
20220220	fores	mev	m 2 0			79645	7	P	d] = -1
20230120	rorde	TOV	130	SCIIP_004R	nan	/2045	A	U	arrarr
20230808	forge	TSX	т30	strip 004R	nan	72812	Α	D	dlrdlr
20220010	form	mev	m 2 0	at min 0045		72070	7	P	d] = -1 =
Z0Z208TA	LOLGE	TOX	130	strip_004R	nañ	12919	А	u	arrarr
20230830	forge	TSX	т30	strip 004R	nan	73146	Α	D	dlrdlr
20220010	form	mov	m 2 0			72212	7	P	d] = -1 =
20220AT0	Torge	TOY	130	strip_004R	nan	13213	А	ע	arrarr
20230921	force	TSX	т30	strip 004R	nan	73480	Α	D	dlrdlr
			-	· _ · · · · ·					

20231002	forge	TSX	т30	strip_004R	nan		А	с	dlrdlr
20231013	forge	TSX	т30	strip_004R	nan	73814	Α	D	dlrdlr
20231024	forge	TSX	т30	strip_004R	nan		Α	С	dlrdlr
20231104	forge	TSX	т30	strip_004R	nan	74148	Α	D	dlrdlr
20231115	forge	TSX	т30	strip_004R	nan	74315	А	D	dlrdlr
20231126	forge	TSX	т30	strip_004R	nan	74482	Α	D	dlrdlr
20231207	forge	TSX	т30	strip_004R	nan	74649	Α	D	dlrdlr
20231218	forge	TSX	т30	strip_004R	nan	74816	Α	D	dlrdlr
20231229	forge	TSX	т30	strip_004R	nan	74983	Α	D	dlrdlr
20240109	forge	TSX	т30	strip 004R	nan	75150	А	D	dlrdlr
20240120	forge	TSX	т30	strip_004R	nan	75317	Α	D	dlrdlr
20240131	forge	TSX	т30	strip_004R	nan	75484	А	D	dlrdlr
20240211	forge	TSX	т30	strip_004R	nan	75651	А	D	dlrdlr
20240222	forge	TSX	т30	strip_004R	nan	75818	А	D	dlrdlr
20240304	forge	TSX	т30	strip_004R	nan	75985	Α	D	dlrdlr
20240315	forge	TSX	т30	strip_004R	nan	76152	Α	D	dlrdlr
20240326	forge	TSX	т30	strip_004R	nan	76319	Α	D	dlrdlr
20240406	forge	TSX	т30	strip 004R	nan	76486	А	D	dlrdlr
20240417	forge	TSX	т30	strip_004R	nan	76653	Α	D	dlrdlr
20240428	forge	TSX	т30	strip_004R	nan	76820	Α	D	dlrdlr
20240509	forge	TSX	т30	strip_004R	nan	76987	Α	D	dlrdlr
20240520	forge	TSX	т30	strip_004R	nan	77154	Α	D	dlrdlr
20240531	forge	TSX	т30	strip_004R	nan	77321	Α	D	dlrdlr
20240611	forge	TSX	т30	strip_004R	nan	77488	А	D	dlrdlr
20240622	forge	TSX	т30	strip_004R	nan	77655	А	D	dlrdlr

Table 5. List of interferometric pairs calculated by ASF HYP3 from data acquired by Sentinel-1A satellite mission showing spacecraft, date and time of first and second acquisitions, respectively. (hyp3-mintpy) [feigl@emidio SDK]\$ find F^* -name "S1*unw phase.tif" | tr '/' ',' | awk -F, '{print \$4}' | tr I ',' | awk -F, '{print \$1}' | sort -n | uniq

SAT YYYYMMDD hhmmss YYYYMMDD hhmmss polarization SIAA 20200102T133453 20200114T133453 VVP012 S1AA_20200114T133453_20200126T133452_VVP012_ SIAA 20200126T133452 20200207T133452 VVP012 S1AA 20200207T133452 20200219T133452 VVP012 S1AA_20200219T133452_20200302T133452_VVP012_ S1AA 20200302T133452 20200314T133452 VVP012 S1AA 20200314T133452 20200326T133452 VVP012 S1AA 20200326T133452 20200407T133452 VVP012 S1AA_20200407T133452_20200419T133453_VVP012 S1AA 20200419T133453 20200501T133453 VVP012 S1AA_20200501T133453_20200513T133454_VVP012_ S1AA_20200513T133454_20200525T133455_VVP012_ S1AA_20200525T133455_20200606T133455_VVP012 S1AA_20200630T133456_20200712T133457_VVP012_ SIAA 20200712T133457 20200724T133458 VVP012 S1AA_20200724T133458_20200805T133459_VVP012_ S1AA_20200805T133459_20200817T133459_VVP012 SIAA 20200817T133459 20200829T133500 VVP012 S1AA_20200829T133500_20200910T133501_VVP012_ S1AA_20200910T133501_20200922T133501_VVP012 S1AA_20200922T133501_20201004T133501_VVP012_ S1AA 20201004T133501 20201016T133502 VVP012 S1AA_20201016T133502_20201028T133501_VVP012_ SIAA 20201028T133501 20201109T133501 VVP012 S1AA_20201109T133501_20201121T133501_VVP012_ S1AA_20201121T133501_20201203T133501_VVP012_ S1AA_20201203T133501_20201215T133500_VVP012 S1AA 20201215T133500 20201227T133500 VVP012 S1AA 20201227T133500 20210108T133459 VVP012 S1AA 20210108T133459 20210120T133458 VVP012 S1AA 20210120T133458 20210201T133458 VVP012 SIAA 20210201T133458 20210213T133458 VVP012 S1AA_20210213T133458_20210225T133457_VVP012_ S1AA_20210225T133457_20210309T133457_VVP012 S1AA 20210309T133457 20210321T133458 VVP012 S1AA 20210321T133458 20210402T133458 VVP012 S1AA 20210402T133458 20210414T133458 VVP012 SIAA 20210414T133458 20210426T133459 VVP012 S1AA_20210426T133459_20210508T133459_VVP012_ S1AA 20210508T133459 20210520T133500 VVP012 S1AA_20210520T133500_20210601T133501_VVP012_ S1AA 20210601T133501 20210613T133502 VVP012 S1AA 20210613T133502 20210625T133502 VVP012 S1AA_20210625T133502_20210707T133503_VVP012_ S1AA 20210707T133503 20210719T133504 VVP012 S1AA 20210719T133504 20210731T133504 VVP012 S1AA 20210731T133504 20210812T133505 VVP012 S1AA_20210812T133505_20210824T133506_VVP012_ S1AA 20210824T133506 20210905T133506 VVP012 S1AA 20210905T133506 20210917T133507 VVP012 S1AA_20210917T133507_20210929T133507_VVP012_ SIAA 20210929T133507 20211011T133507 VVP012 S1AA 20211011T133507 20211023T133507 VVP012 S1AA_20211023T133507_20211104T133507_VVP012_ S1AA_20211128T133506_20211210T133506_VVP012_ S1AA 20211210T133506 20211222T133505 VVP012 S1AA 20211222T133505 20220103T133505 VVP012 S1AA_20220103T133505_20220115T133504_VVP012_ S1AA 20220115T133504 20220127T133504 VVP012 S1AA_20220127T133504_20220208T133503_VVP012 SIAA 20220208T133503 20220220T133506 VVP012 S1AA_20220220T133506_20220304T133506_VVP012_ S1AA 20220304T133506 20220316T133506 VVP012 S1AA 20220316T133506 20220328T133506 VVP012 S1AA_20220328T133506_20220409T133504_VVP012_

S1AA_20220409T133504_20220421T133504_VVP012_
S1AA 20220421T133504 20220503T133504 VVP012
S1AA 20220503T133504 20220515T133506 VVP012
S1AA 20220515T133506 20220527T133506 VVP012
S1AA 20220527T133506 20220608T133507 VVP012
S1AA 20220608T133507 20220620T133508 VVP012
S1AA 20220620T133508 20220702T133509 VVP012
S1AA 20220702T133509 20220714T133501 VVP012
S1AA 20220714T133501 20220726T133502 VVP012
S1AA 20220726T133502 20220807T133503 VVP012
S1AA 20220807T133503 20220819T133503 VVP012
S1AA 20220912T133505 20220924T133504 VVP012
S1AA 20220924T133504 20221006T133505 VVP012
S1AA 20221006T133505 20221018T133505 VVP012
S1AA 20221018T133505 20221030T133505 VVP012
S1AA 20221030T133505 20221111T133504 VVP012
S1AA 20221111T133504 20221123T133505 VVP012
S1AA 20221123T133505 20221205T133504 VVP012
S1AA 20221205T133504 20221217T133503 VVP012
S1AA 20221217T133503 20221229T133502 VVP012
S1AA 20221229T133502 20230110T133502 VVP012
S1AA 20230110T133502 20230122T133502 VVP012
S1AA 20230122T133502 20230203T133501 VVP012
S1AA 20230203T133501 20230215T133500 VVP012
S1AA 20230215T133500 20230227T133501 VVP012
S1AA 20230227T133501 20230311T133501 VVP012
S1AA 20230311T133501 20230323T133501 VVP012
S1AA 20230323T133501 20230404T133501 VVP012
S1AA 20230404T133501 20230416T133501 VVP012
SIAA 20230416T133501 20230428T133502 VVP012
S1AA 20230428T133502 20230510T133502 VVP012
SIAA 20230510T133502 20230522T133503 VVP012
S1AA 20230522T133503 20230603T133504 VVP012
S1AA 20230603T133504 20230615T133504 VVP012
SIAA 20230615T133504 20230627T133505 VVP012
S1AA 20230627T133505 20230709T133506 VVP012
SIAA 20230709T133506 20230721T133507 VVP012
S1AA 20230721T133507 20230802T133507 VVP012
S1AA 20230802T133507 20230814T133508 VVP012
S1AA 20230814T133508 20230826T133509 VVP012
S1AA 20230826T133509 20230907T133509 VVP012
S1AA 20230907T133509 20230919T133510 VVP012
SIAA 20230919T133510 20231001T133510 VVP012
S1AA 20231001T133510 20231013T133510 VVP012
S1AA 20231013T133510 20231025T133510 VVP012
S1AA 20231025T133510 20231106T133509 VVP012
S122 20231106T133509 20231118T133509 WVD012
SIAA 20231118T133509 20231130T133509 VVP012
SIAA 20231130T133509 20231212T133509 VVP012
SIAA 20231212T133509 20231224T133508 WVP012
SIAA 20231224T133508 20240105T133507 VVP012
SIAA 20240105T133507 20240117T133506 VVP012
SIAA 20240117T133506 20240129T133506 VVP012
SIAA 20240129T133506 20240210T133506 VVP012
STAA 202402101133506 202402221133506 VVP012

Table 6. List of interferometric pairs calculated by ASF HYP3 from data acquired by Sentinel-1B satellite mission showing spacecraft, date and time of first and second acquisitions, respectively. (hyp3-mintpy) [feigl@emidio SDK]\$ find F^* -name "S1*unw_phase.tif" | tr '/' ',' | awk -F, '{print \$4}' | tr I ',' | awk -F, '{print \$1}' | sort -n | uniq

SAT YYYYMMDD hhmmss YYYYMMDD hhmmss polarization S1BB 20200103T012610 20200115T012610 VVP012 S1BB 20200115T012610 20200127T012610 VVP012 S1BB_20200127T012610_20200208T012609_VVP012_ S1BB 20200208T012609 20200220T012609 VVP012 S1BB 20200220T012609 20200303T012609 VVP012 S1BB_20200303T012609_20200315T012609_VVP012_ S1BB 20200315T012609 20200327T012609 VVP012 S1BB 20200327T012609 20200408T012609 VVP012 S1BB 20200408T012609 20200420T012610 VVP012 S1BB_20200420T012610_20200502T012611_VVP012 S1BB 20200502T012611 20200514T012611 VVP012 S1BB 20200514T012611 20200526T012612 VVP012 S1BB_20200526T012612_20200607T012613_VVP012_ S1BB_20200607T012613_20200619T012613_VVP012 S1BB_20200619T012613_20200701T012614_VVP012_ S1BB 20200701T012614 20200713T012615 VVP012 S1BB_20200713T012615_20200725T012615_VVP012 S1BB_20200725T012615_20200806T012616_VVP012 S1BB 20200806T012616 20200818T012617 VVP012 S1BB 20200818T012617 20200830T012618 VVP012 S1BB 20200830T012618 20200911T012618 VVP012 S1BB 20200911T012618 20200923T012618 VVP012 S1BB 20200923T012618 20201005T012619 VVP012 S1BB_20201005T012619_20201017T012619_VVP012 S1BB 20201017T012619 20201029T012619 VVP012 S1BB 20201029T012619 20201110T012619 VVP012 S1BB 20201110T012619 20201122T012618 VVP012 S1BB_20201122T012618_20201204T012618_VVP012 S1BB 20201204T012618 20201216T012617 VVP012 S1BB 20201216T012617 20201228T012617 VVP012 S1BB_20201228T012617_20210109T012616_VVP012_ S1BB 20210109T012616 20210121T012616 VVP012 S1BB 20210121T012616 20210202T012615 VVP012 S1BB_20210202T012615_20210214T012615_VVP012_ S1BB_20210214T012615_20210226T012615_VVP012 S1BB 20210226T012615 20210310T012615 VVP012 S1BB 20210310T012615 20210322T012615 VVP012 S1BB_20210322T012615_20210403T012615_VVP012_ S1BB 20210403T012615 20210415T012616 VVP012 S1BB_20210415T012616_20210427T012616_VVP012_ S1BB 20210427T012616 20210509T012617 VVP012 S1BB_20210509T012617_20210521T012617_VVP012 S1BB_20210521T012617_20210602T012618_VVP012 S1BB 20210602T012618 20210614T012619 VVP012 S1BB 20210614T012619 20210626T012620 VVP012 S1BB 20210626T012620 20210708T012620 VVP012 S1BB 20210708T012620 20210720T012621 VVP012 S1BB 20210720T012621 20210801T012622 VVP012 S1BB_20210801T012622_20210813T012622_VVP012 S1BB 20210813T012622 20210825T012623 VVP012 S1BB 20210825T012623 20210906T012624 VVP012 S1BB_20210906T012624_20210918T012624_VVP012_ S1BB 20210918T012624 20210930T012624 VVP012 S1BB 20210930T012624 20211012T012624 VVP012 S1BB_20211012T012624_20211024T012625_VVP012_ S1BB_20211024T012625_20211105T012624_VVP012 S1BB 20211105T012624 20211117T012624 VVP012 S1BB 20211117T012624 20211129T012624 VVP012 S1BB 20211129T012624 20211211T012623 VVP012 S1BB 20211211T012623 20211223T012622 VVP012