



45th US Rock Mechanics/Geomechanics Symposium

American Rock Mechanics Association

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Simulating Complex Fracture Systems in Geothermal Reservoirs Using an Explicitly Coupled Hydro- Geomechanical Model

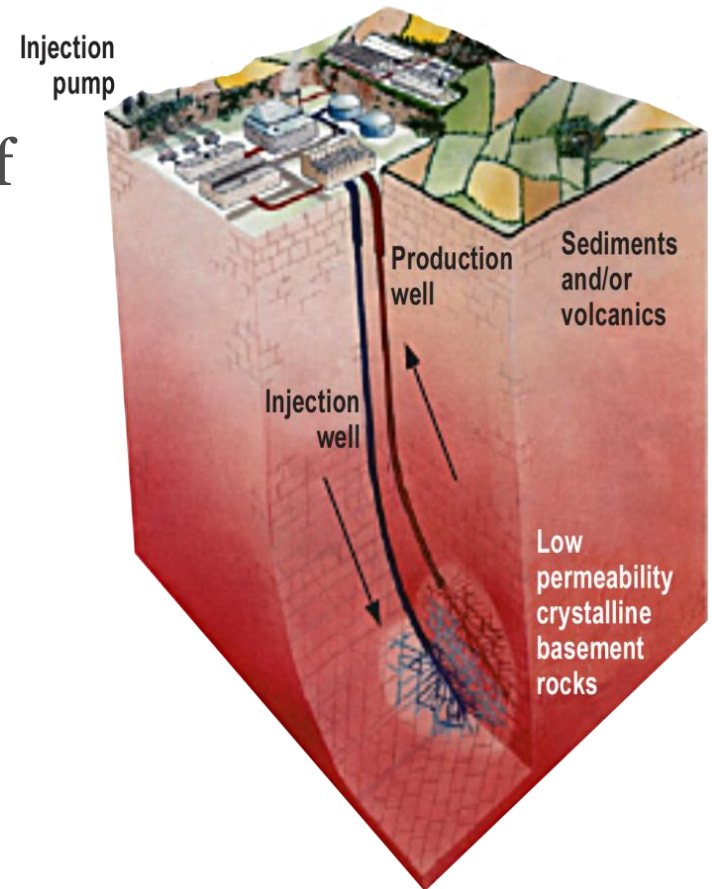
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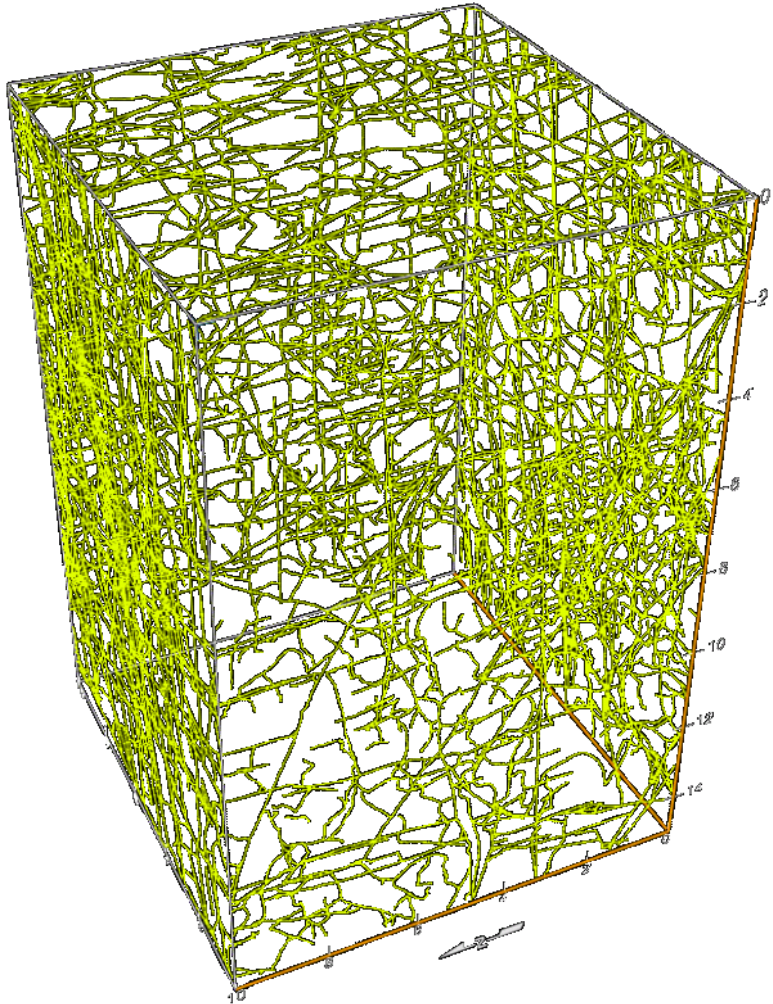


Background

- Hydraulic fracturing is an effective method for enhancing permeability of geological formations.



How real fracture system looks like



(Large Block Test, Yucca Mountain.
Wagoner, 2000)

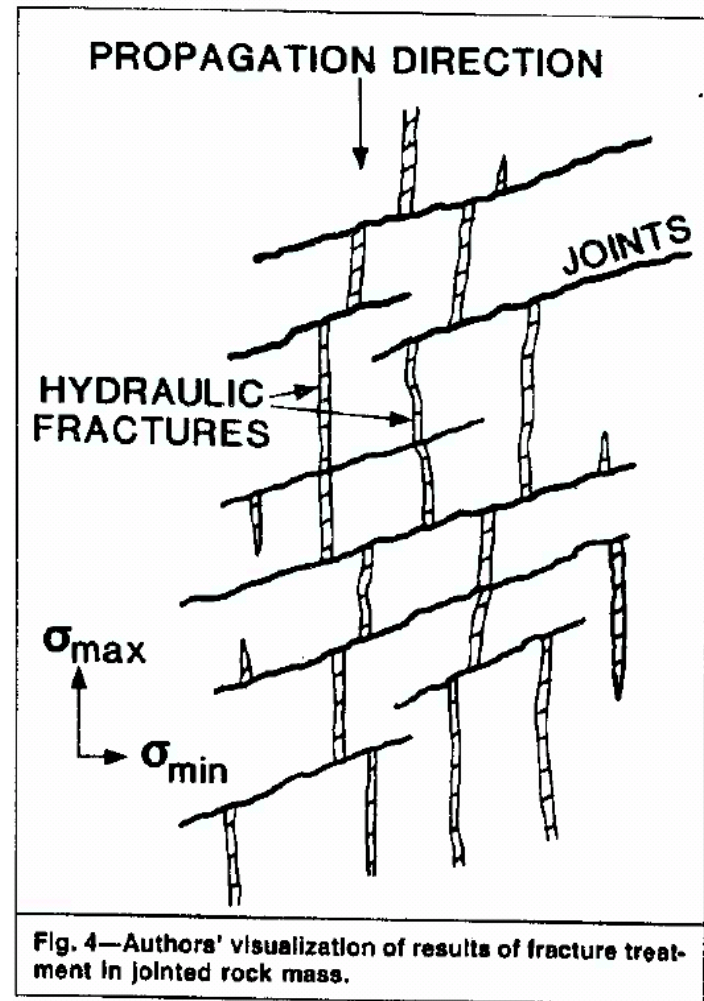
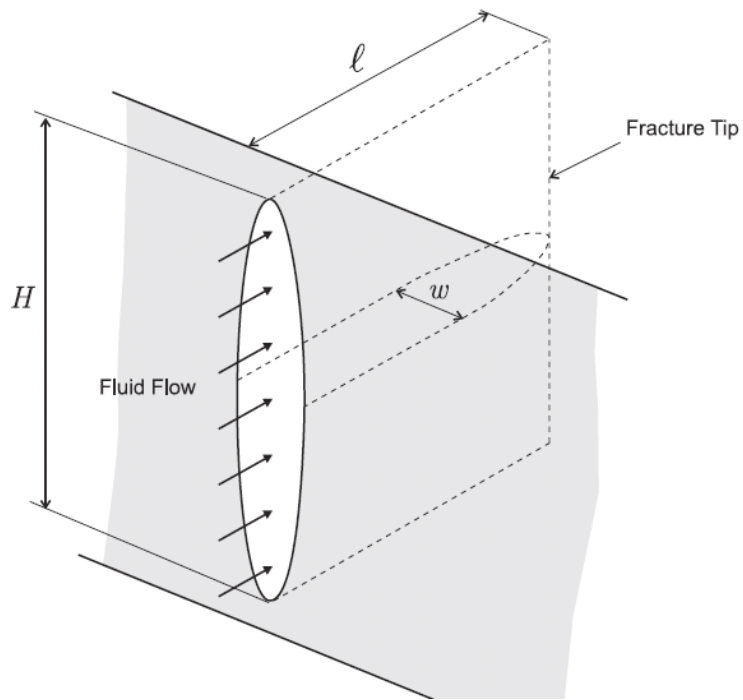


Fig. 4—Authors' visualization of results of fracture treatment in jointed rock mass.

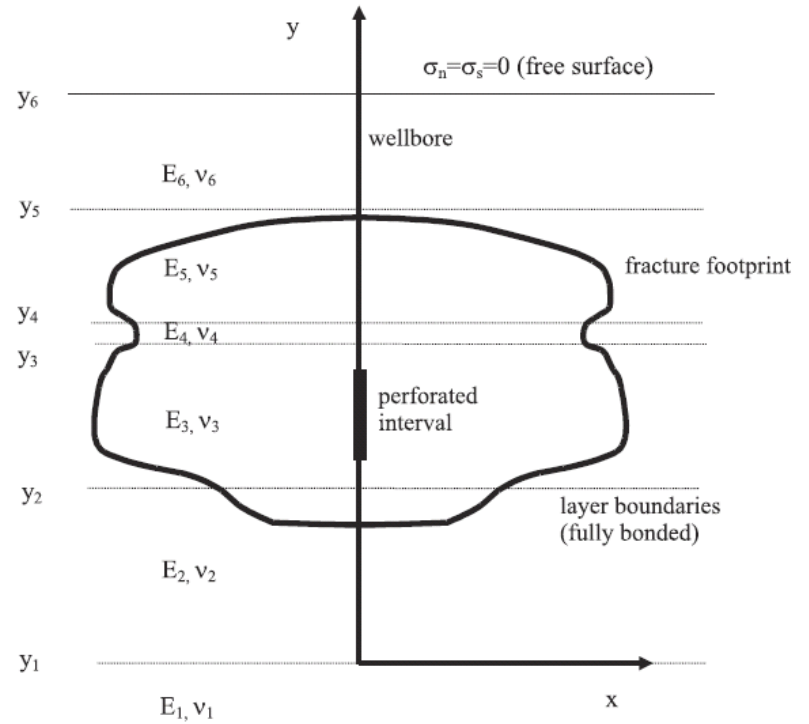
(Warpinski and Teufel, 1987)



State of the art



PKN model



PL3D model

(Adachi et al. 2000)

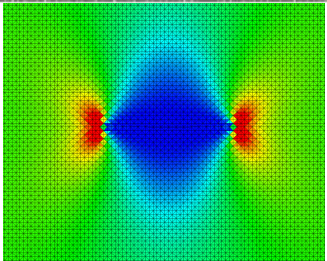


What do we need to simulate hydrofrac?

- Physical processes need to be covered:
 - Fluid flow due to pressure gradient;
 - Rock deformation;
 - Variation of aperture width; and
 - Rock fracturing.



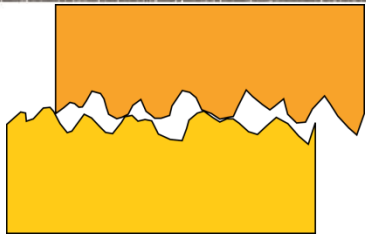
Modules and their coupling



Solid Solver

Joint displacement

Joint Model



Fracturing Criteria
New Solid Mesh

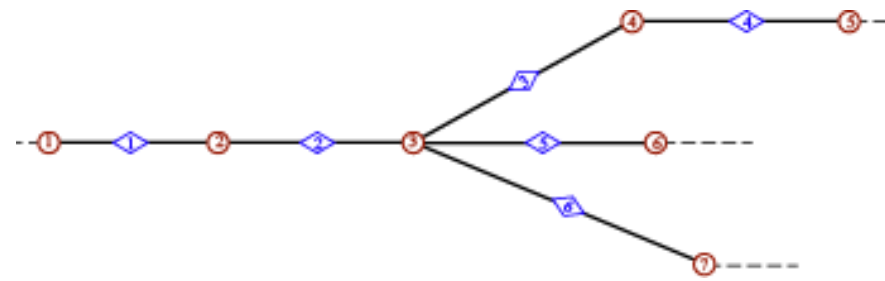
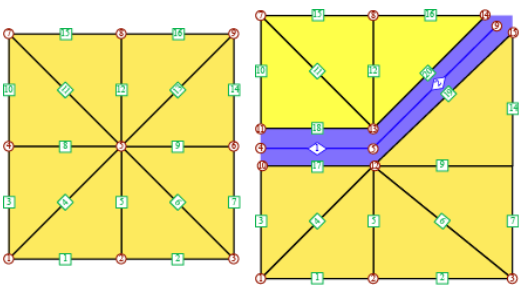
Pressure field along fractures

Aperture Size

Remeshing Module

New Frac. Network

Flow Solver





Important Components

- Flow solver – Finite volume method

$$\frac{\partial q}{\partial l} + \frac{\partial w^h}{\partial t} = 0 \quad \kappa \frac{\partial P}{\partial l} = -q$$

$$\kappa_{ij} = \frac{w_{ij}^{h3}}{6\mu(L_i + L_j)}$$

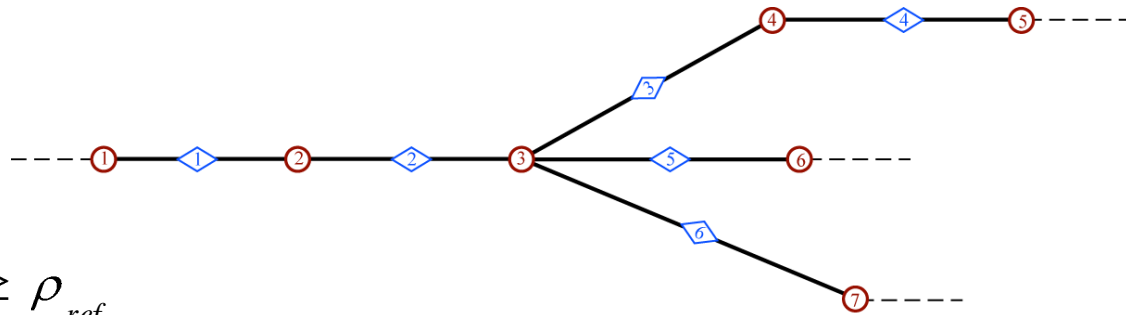
$$w_{ij}^{h3} = \frac{w_i^{h3} w_j^{h3} (L_i + L_j)}{w_i^{h3} L_j + w_j^{h3} L_i}$$

$$\dot{V}_{ij} = \kappa_{ij} (P_i - P_j)$$

$$P_i = \begin{cases} K \left(\frac{m_i}{V_i \rho_{ref}} - 1 \right) & \text{if } m_i / V_i \geq \rho_{ref} \\ P_{vap} & \text{if } m_i / V_i < \rho_{ref} \end{cases}$$

Two mechanisms:

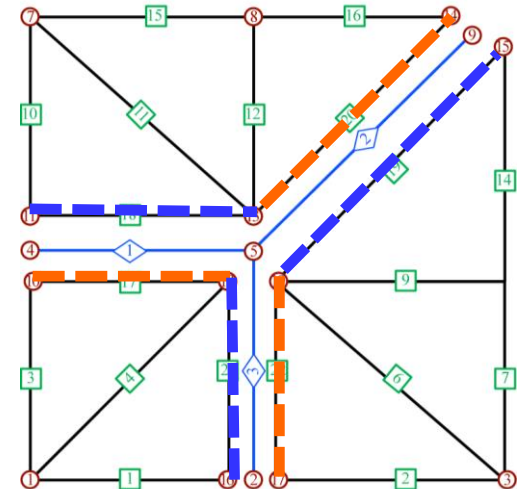
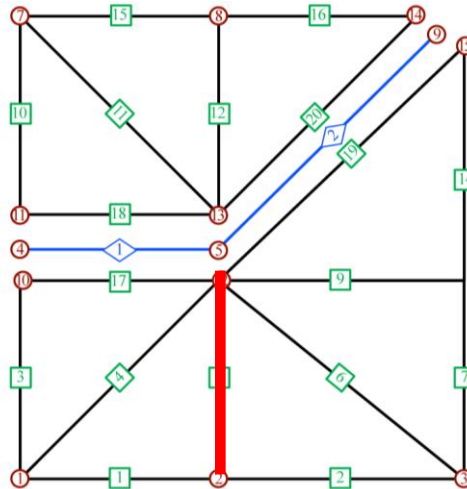
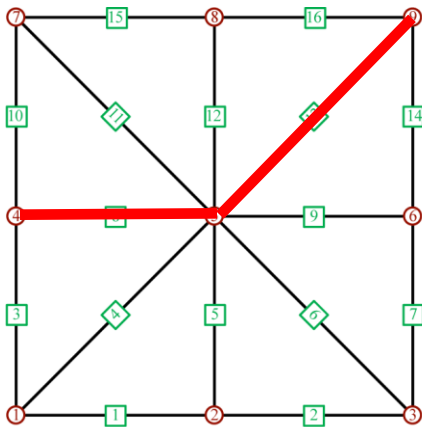
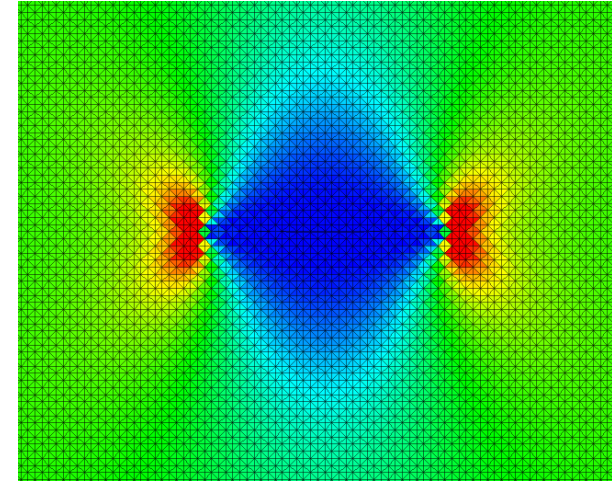
- Flow in fractures due to pressure gradient.
- Mass conservation with varying total fracture volume.



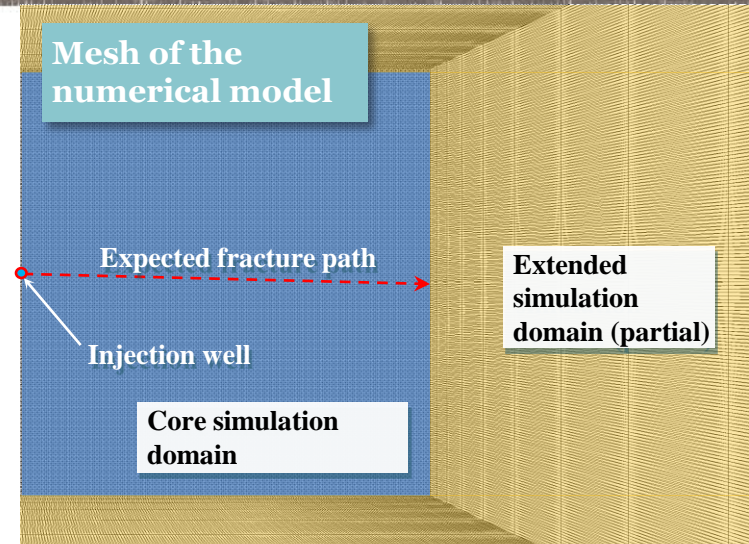
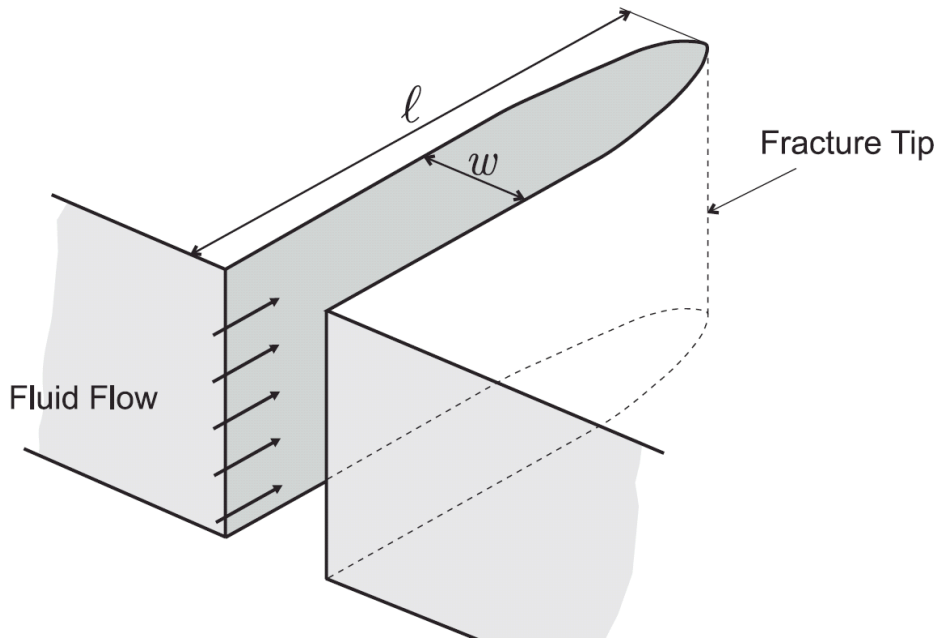


Important Components

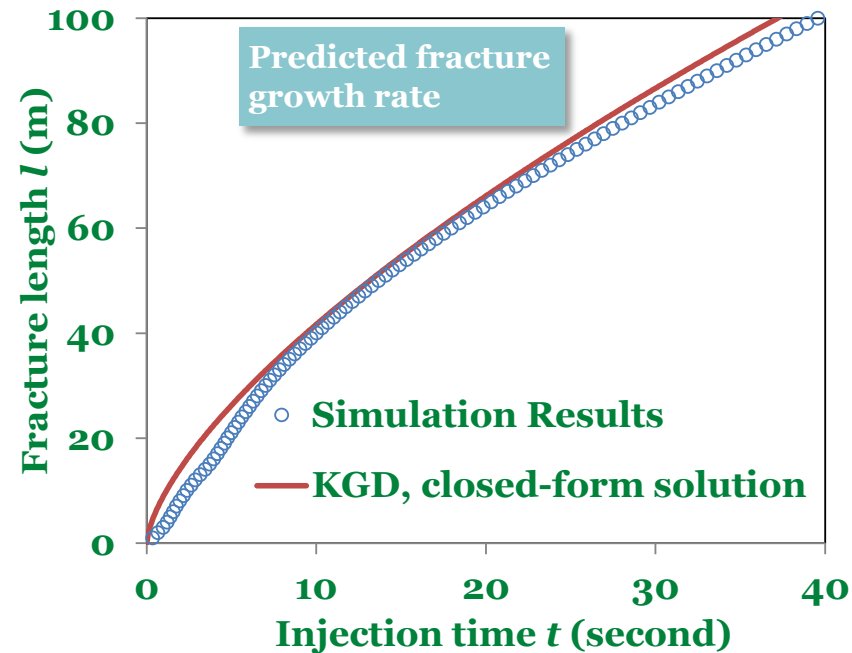
- Fracturing criterion
 - Estimates stress intensity factors using a generalized displacement correlation method
 - Handles mixed mode fractures
- Adaptive remeshing



Model verification: classical KGD model

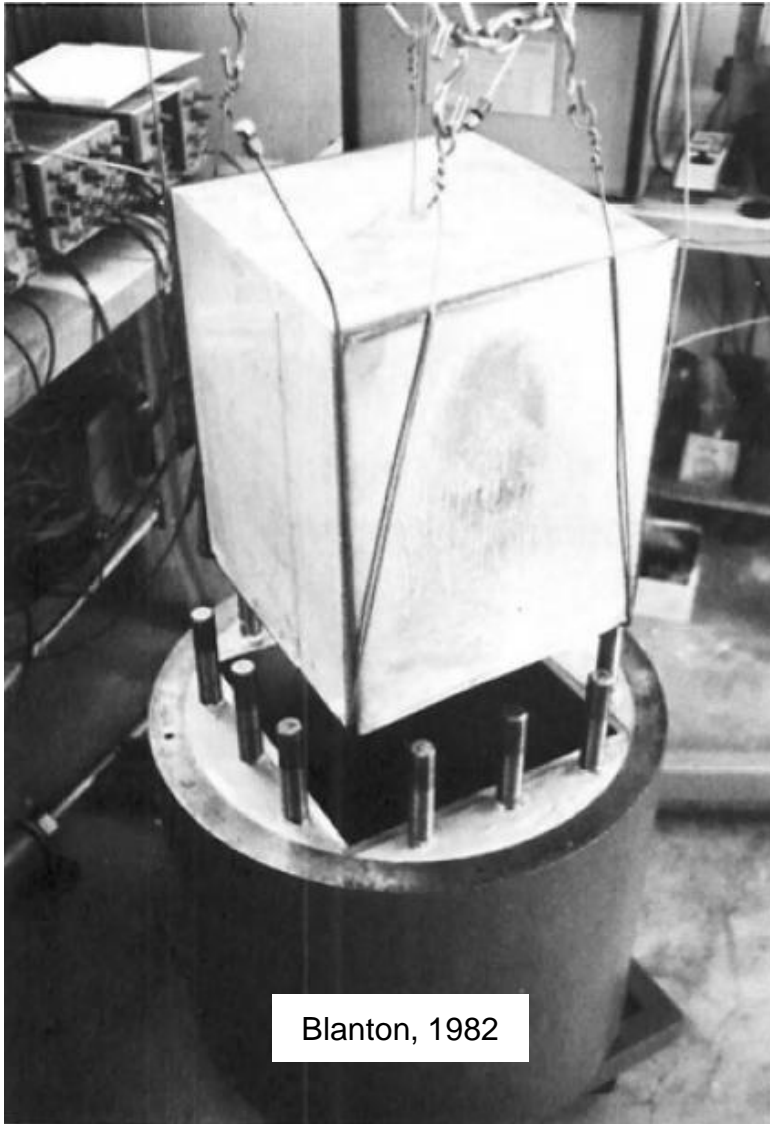


$$l(t) = 0.679 \left[\frac{Gq_0^3}{\mu(1-\nu)} \right]^{\frac{1}{6}} t^{\frac{2}{3}}$$

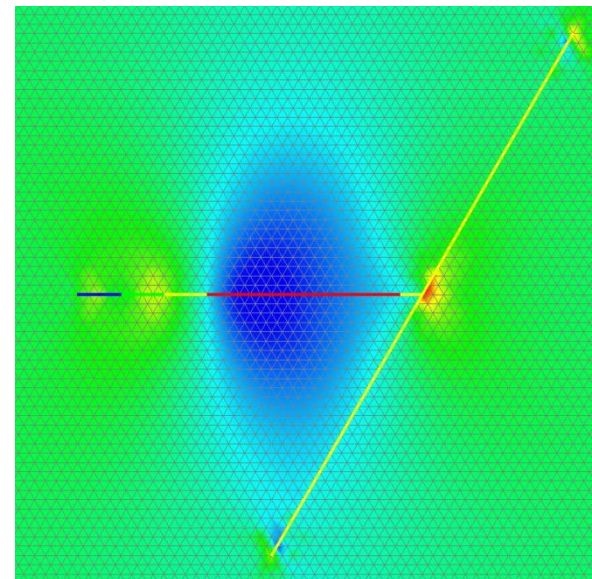
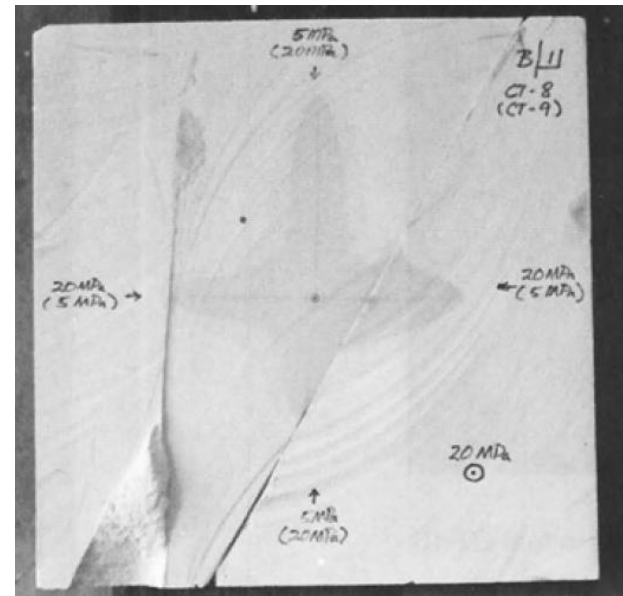




Model validation: lab test results

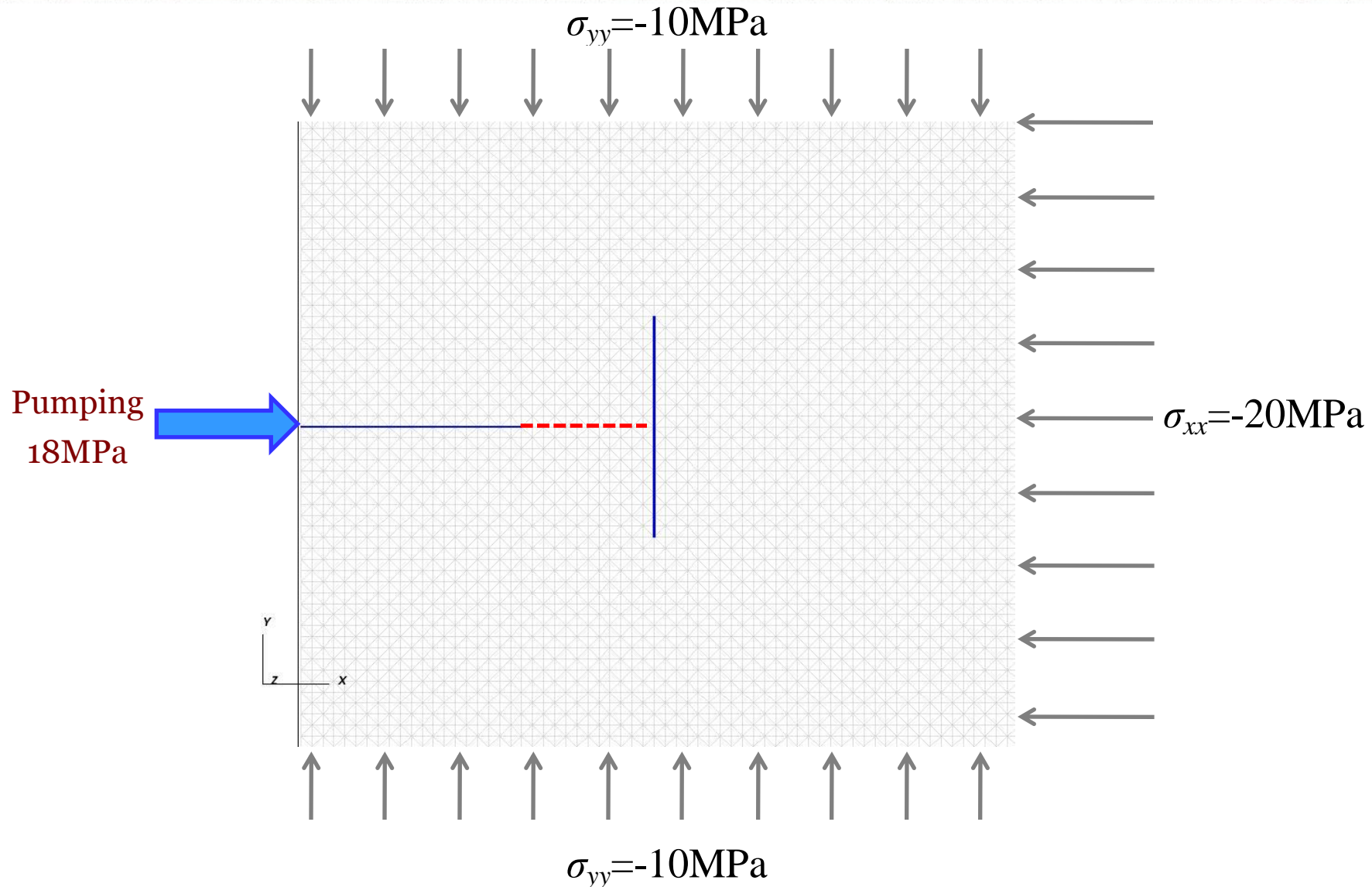


Blanton, 1982



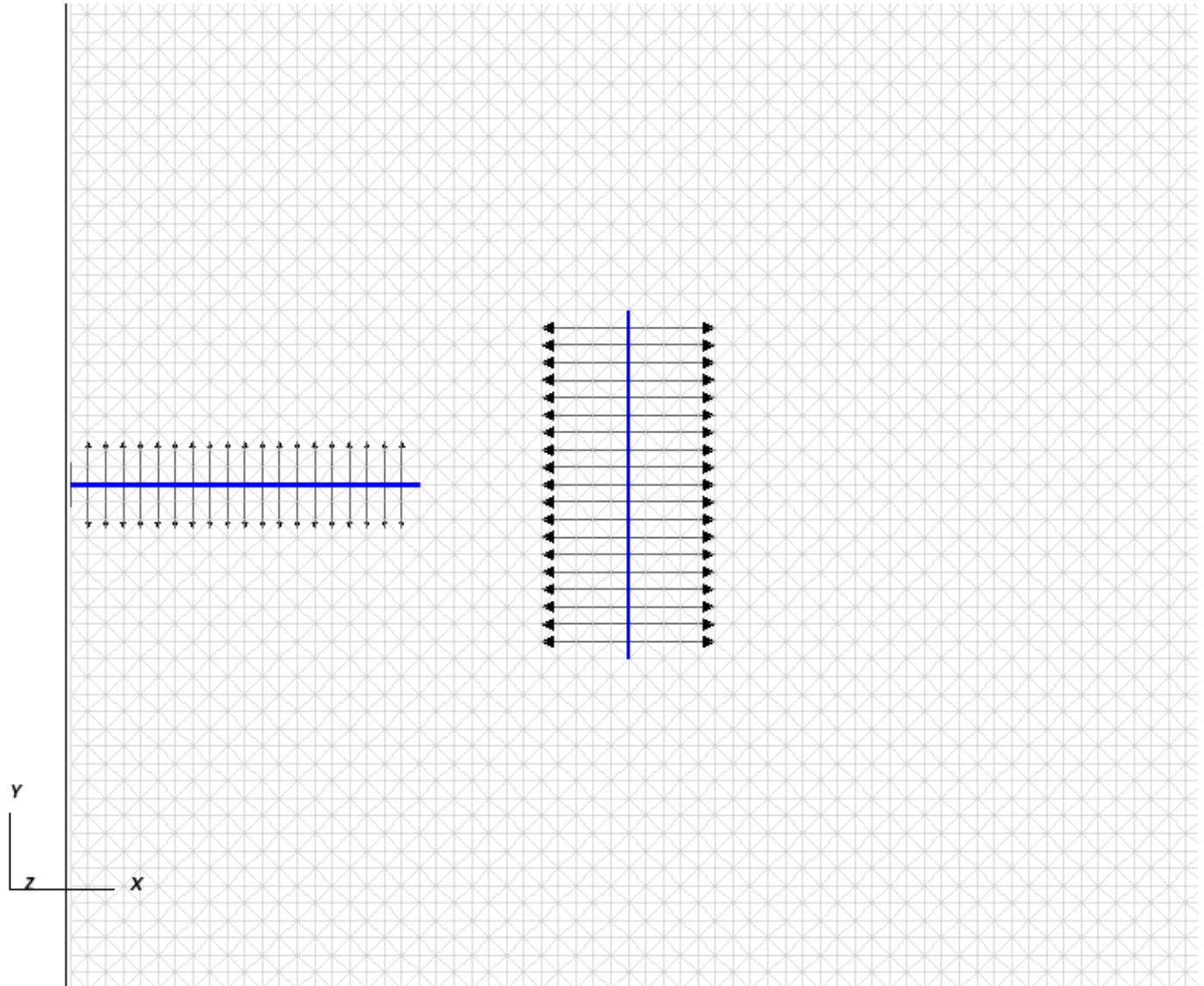


Interaction Between Propagating and Existing Fractures



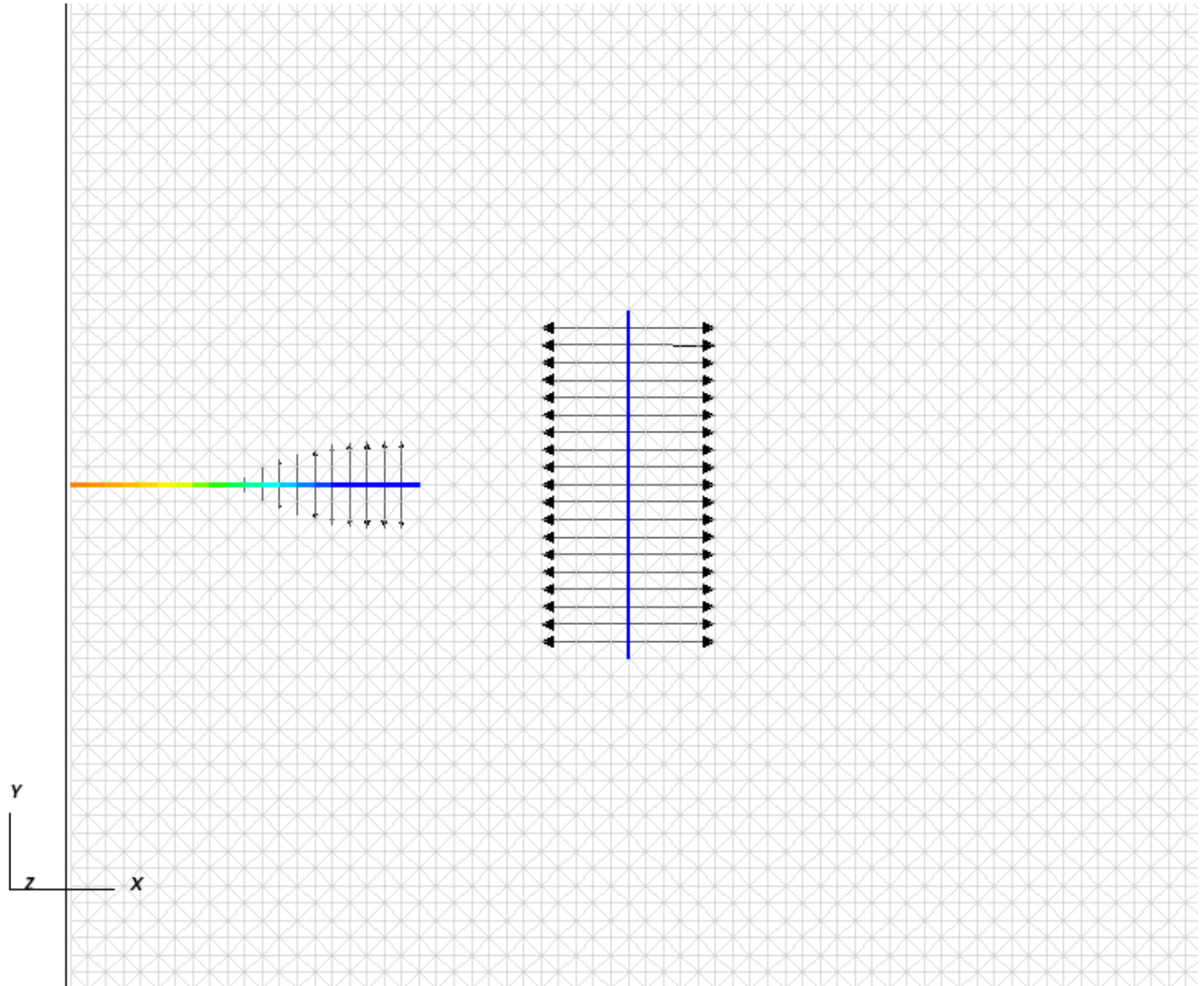


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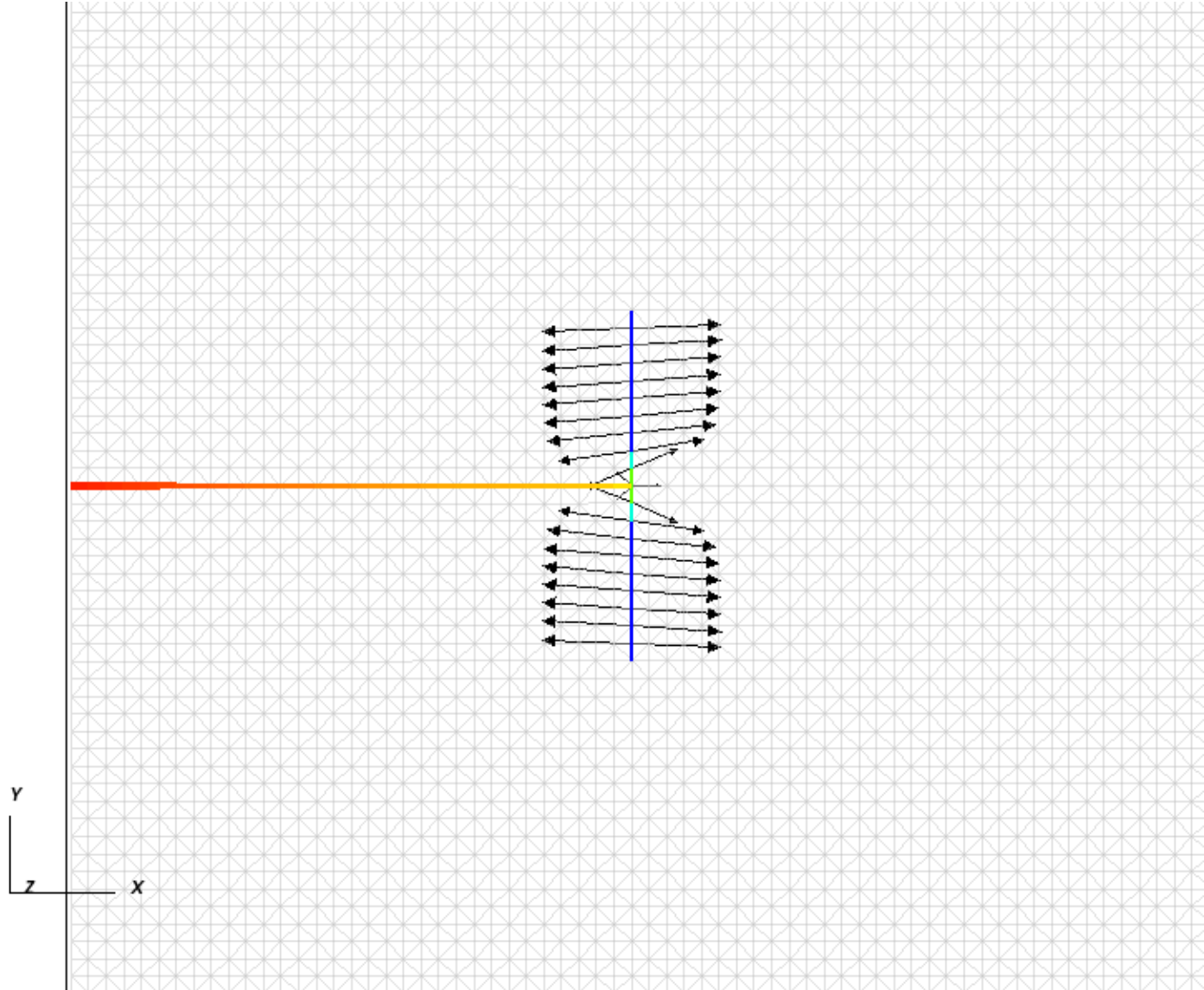


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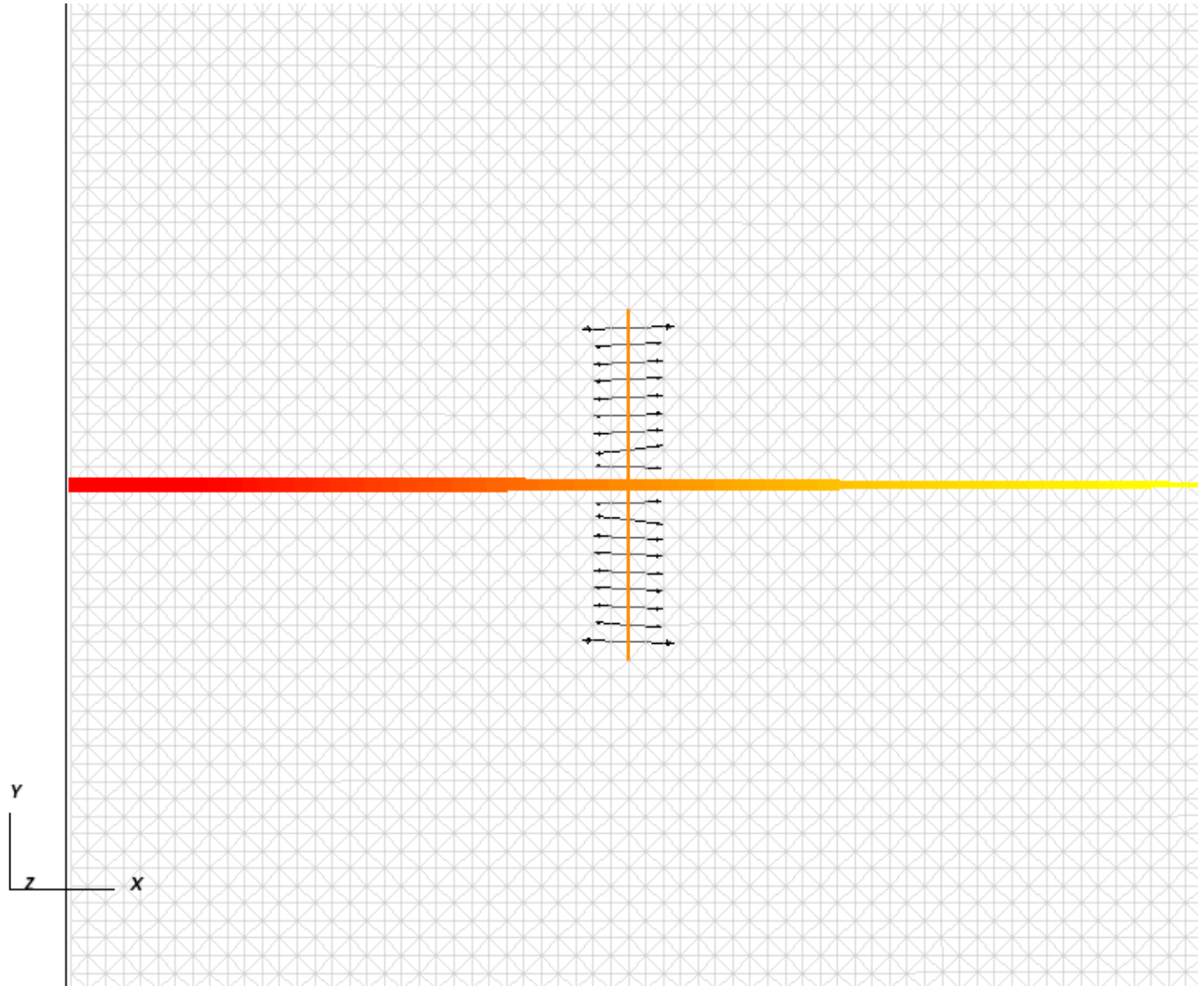


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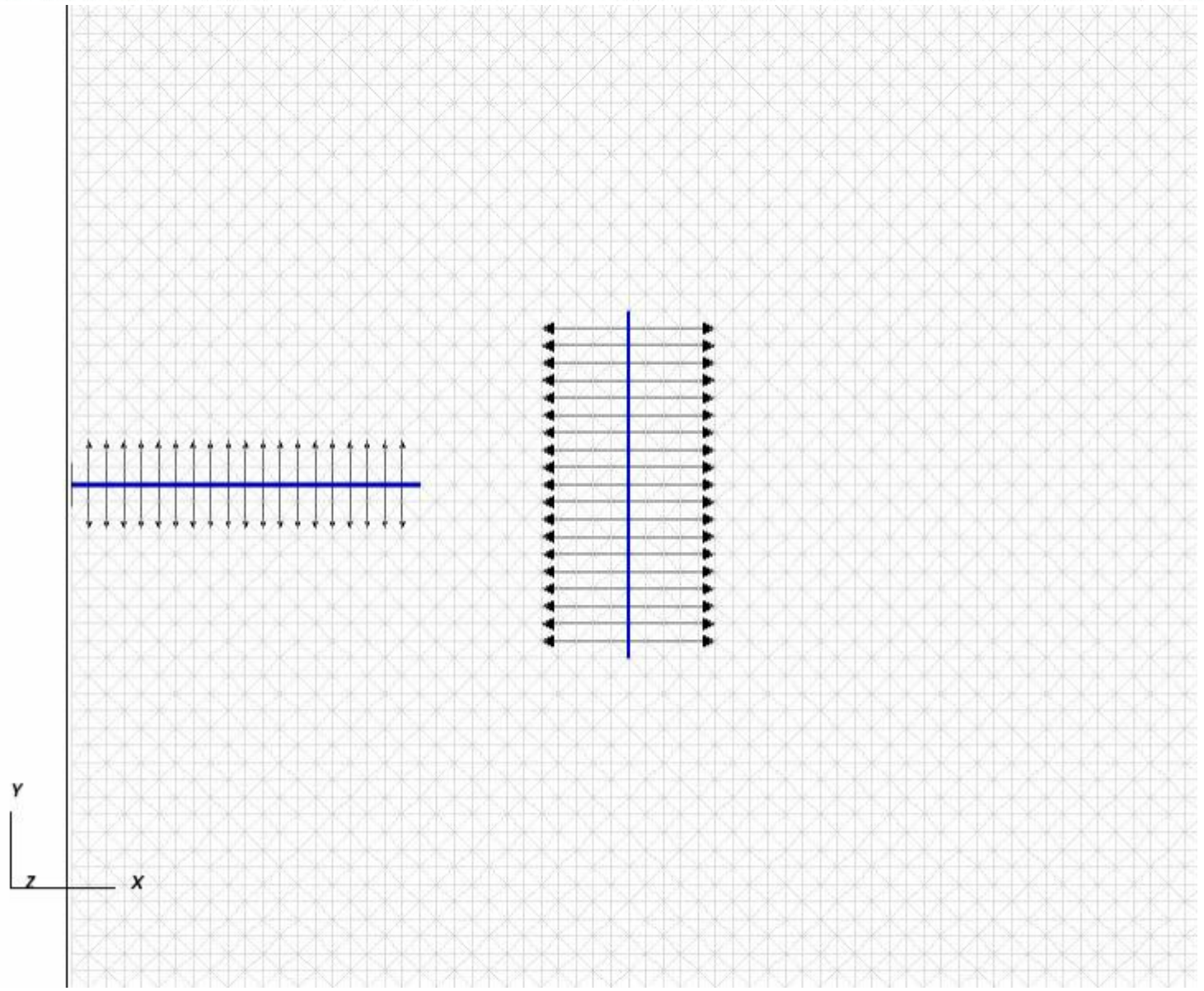


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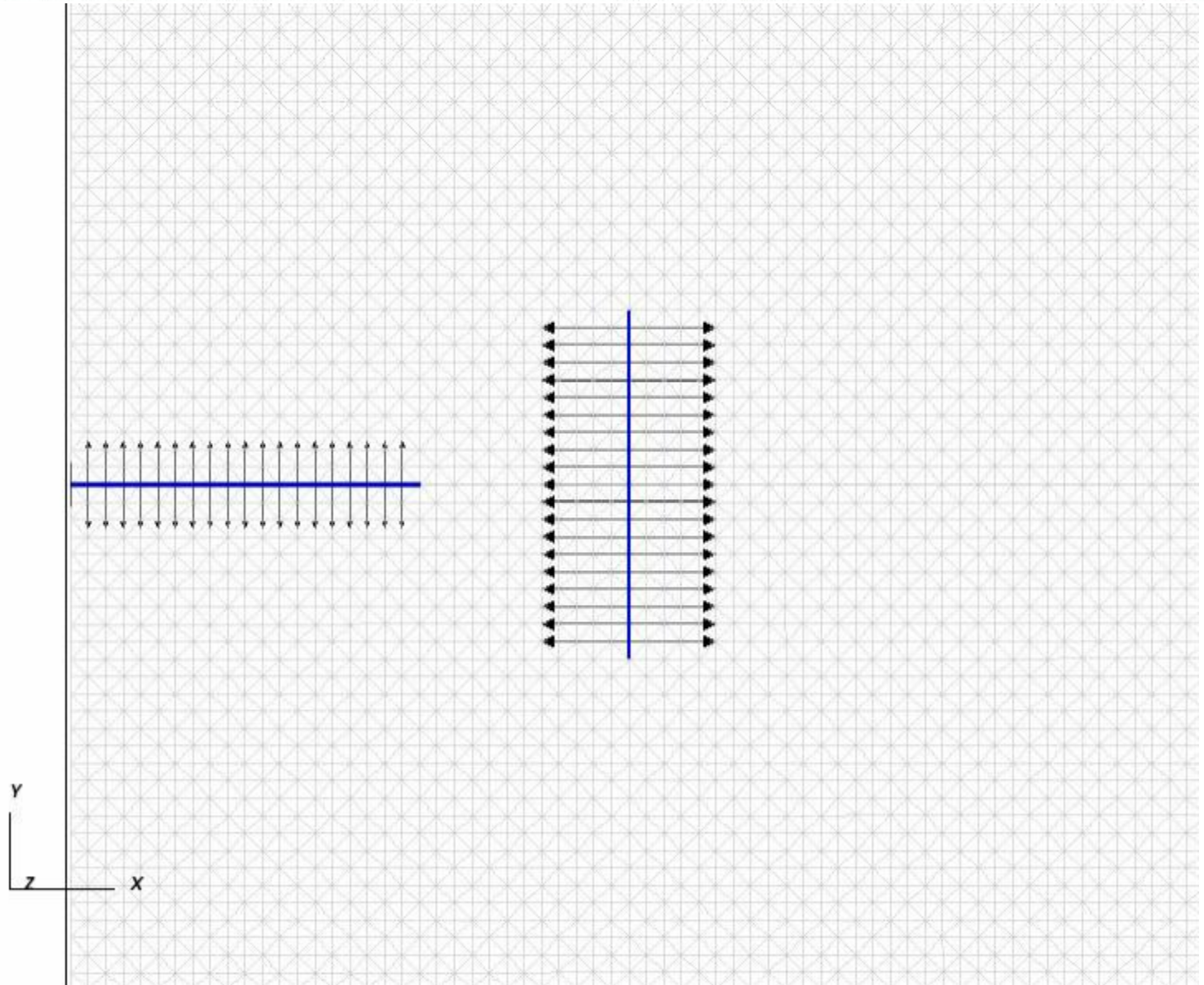


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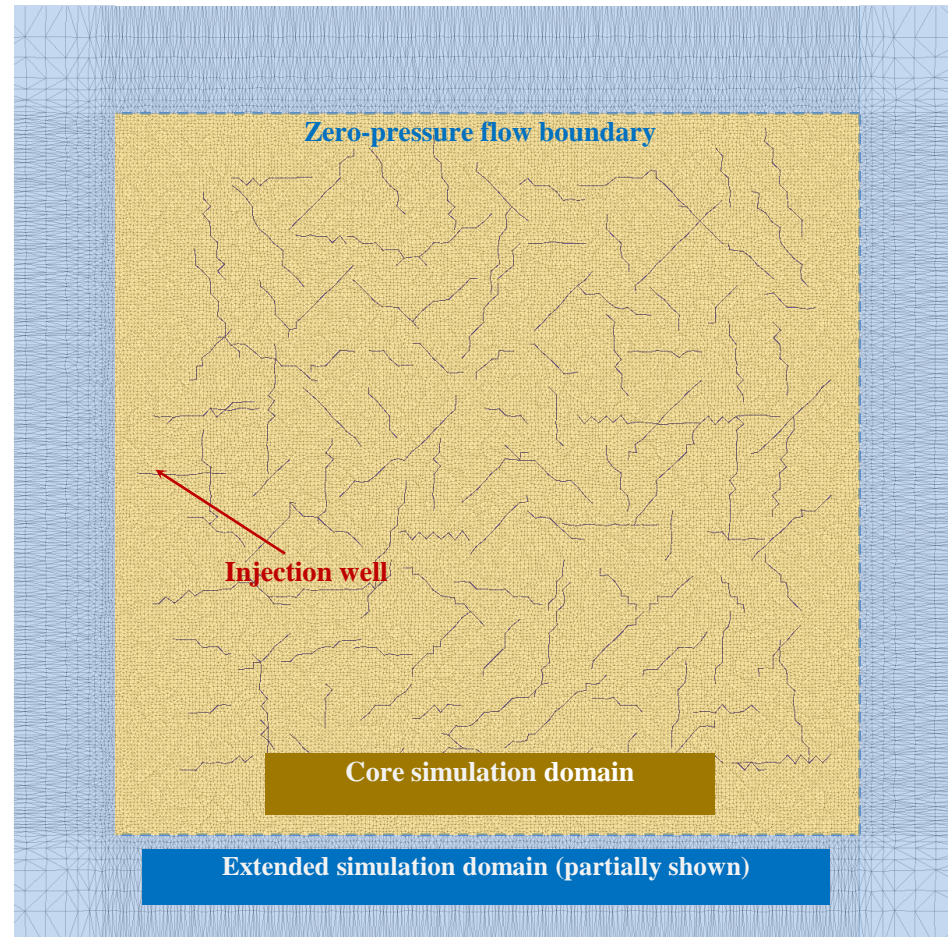
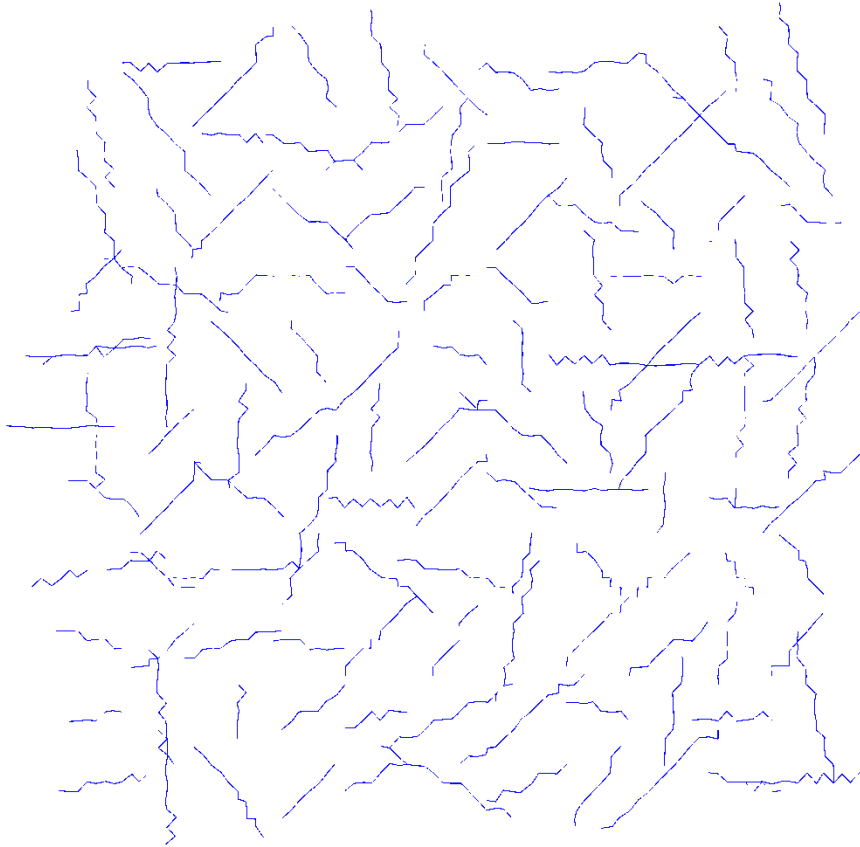


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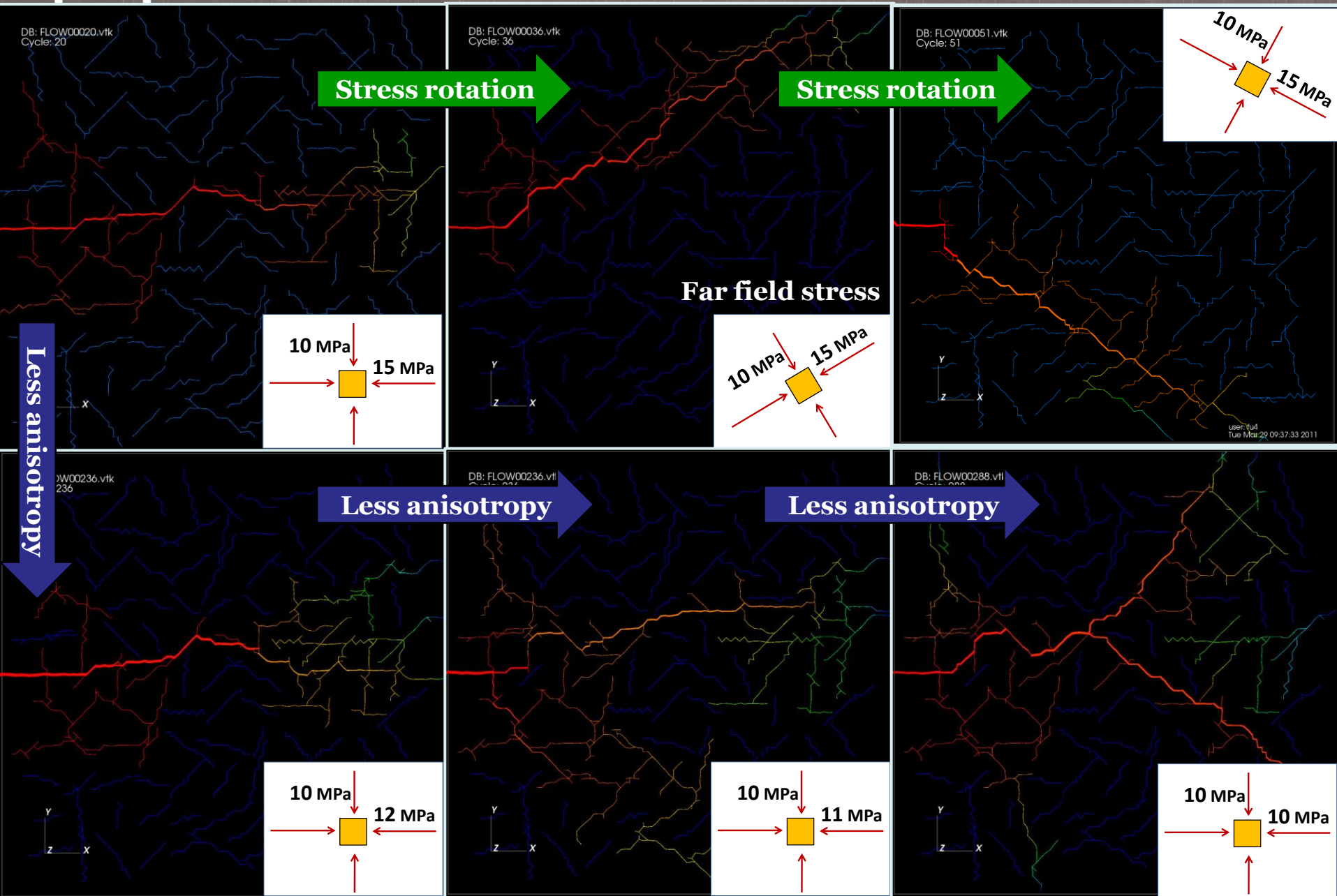




Application to more complex fracture networks

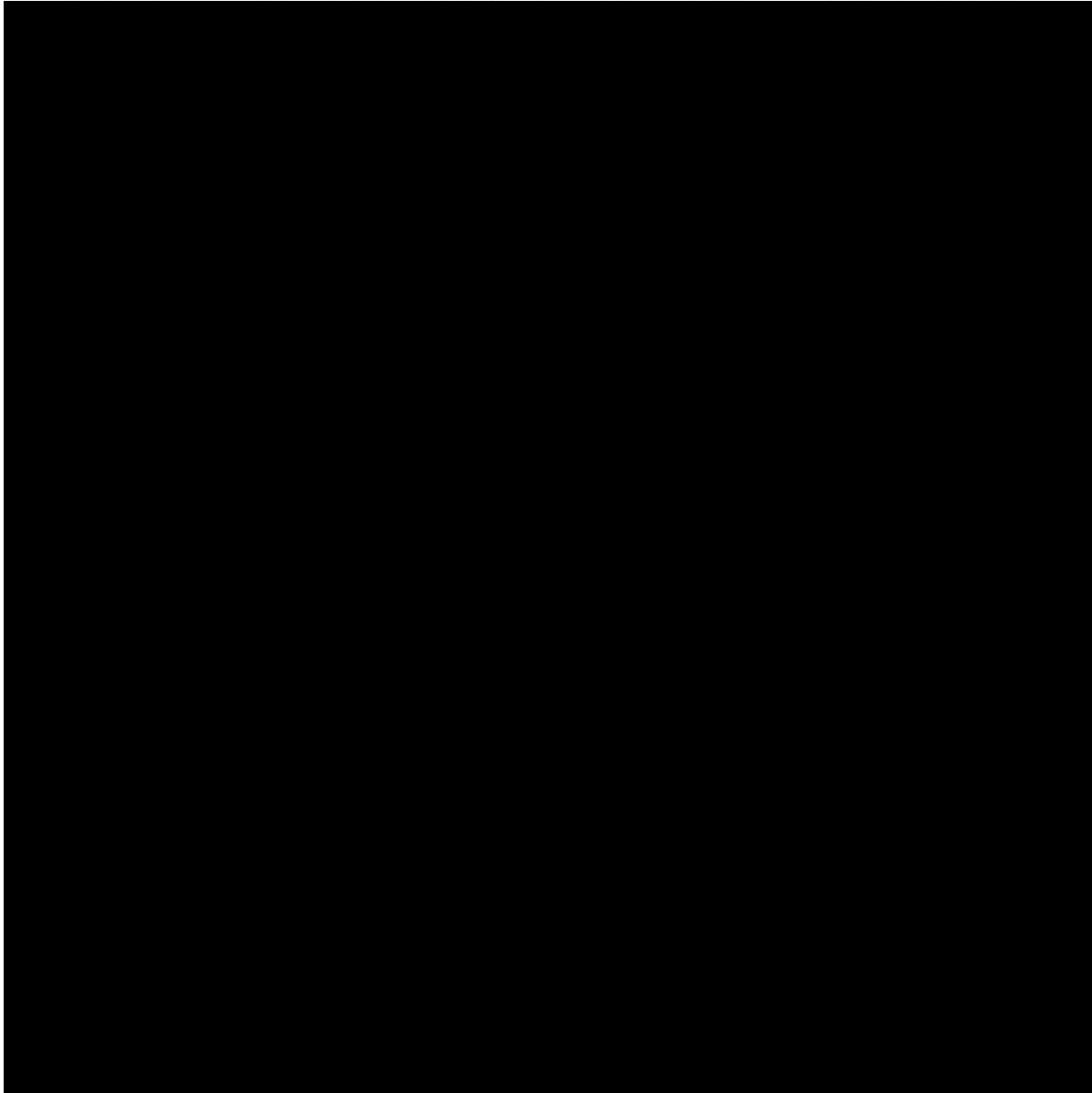


Application to more complex fracture networks





Application to more complex fracture networks





Concluding Remarks

- Challenges:
 - The coupling of multiple modules.
 - High computational cost.
- Benefits:
 - Explicit simulation of fracture-fracture and fracture-fluid interaction.
 - Capable of handling complex fracture networks.
 - Simple and physically meaningful input parameters.
 - Induced seismicity naturally emerges in the simulation.
- Further development, enhancement, and validation



Acknowledgements

- This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344.

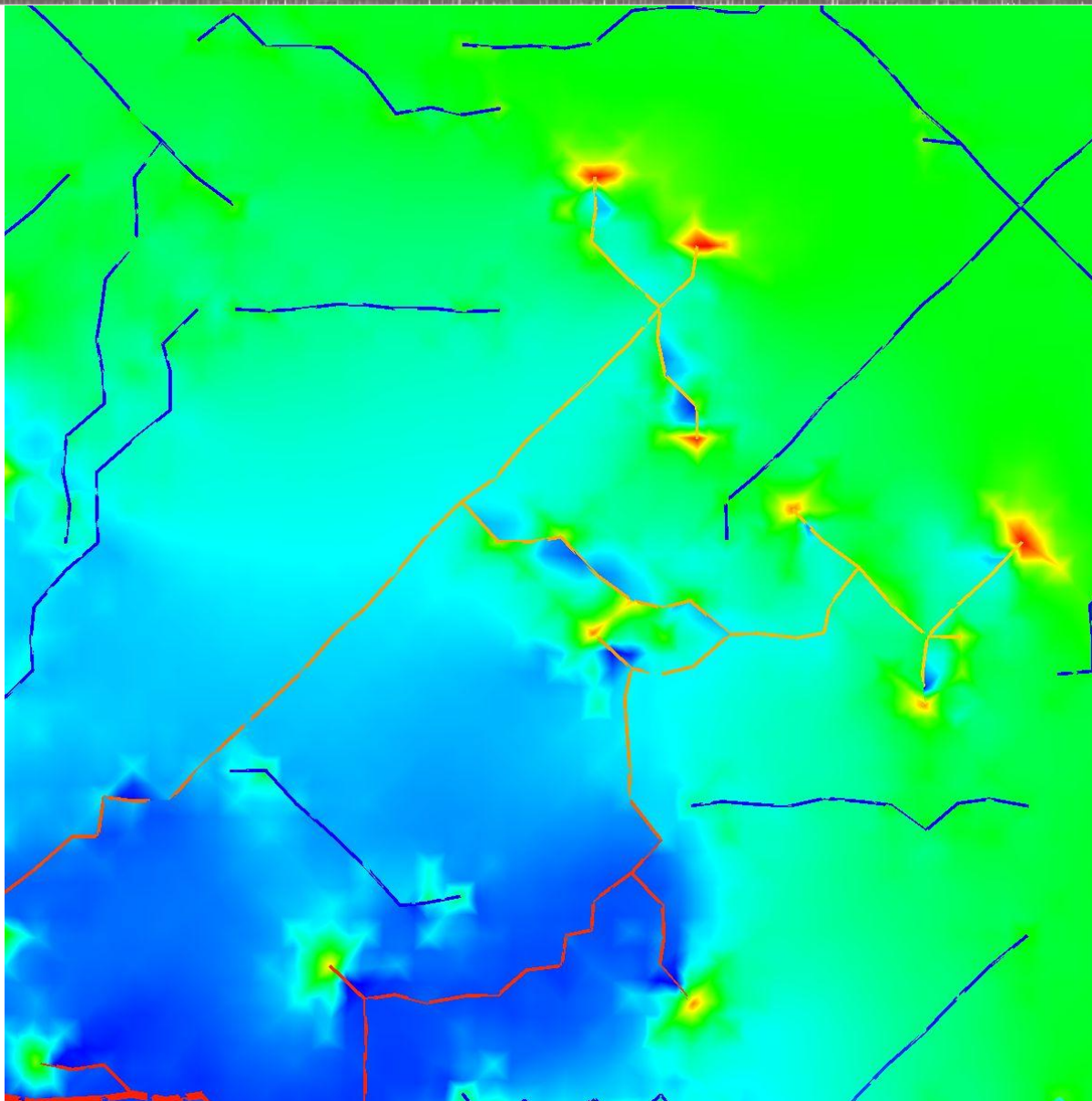


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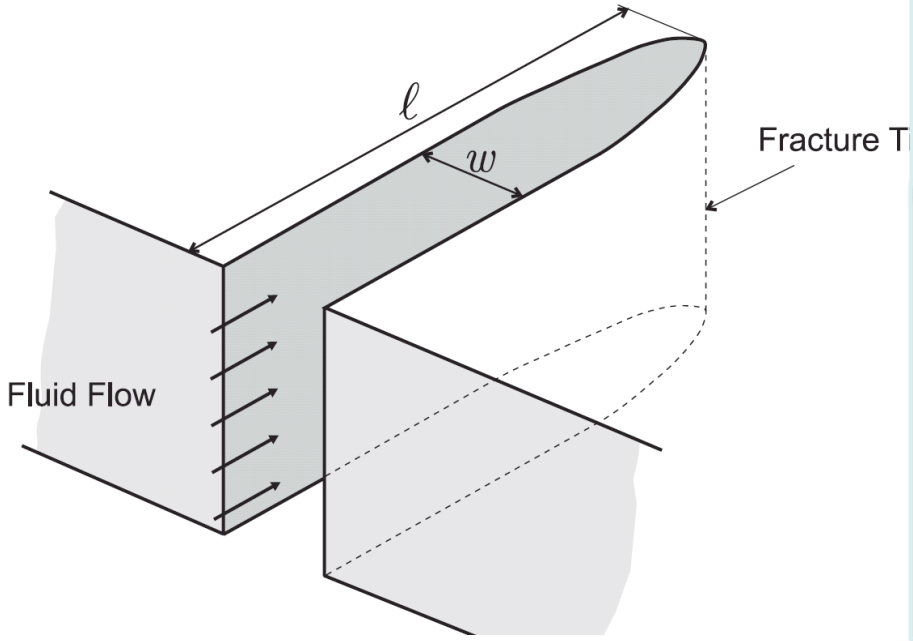


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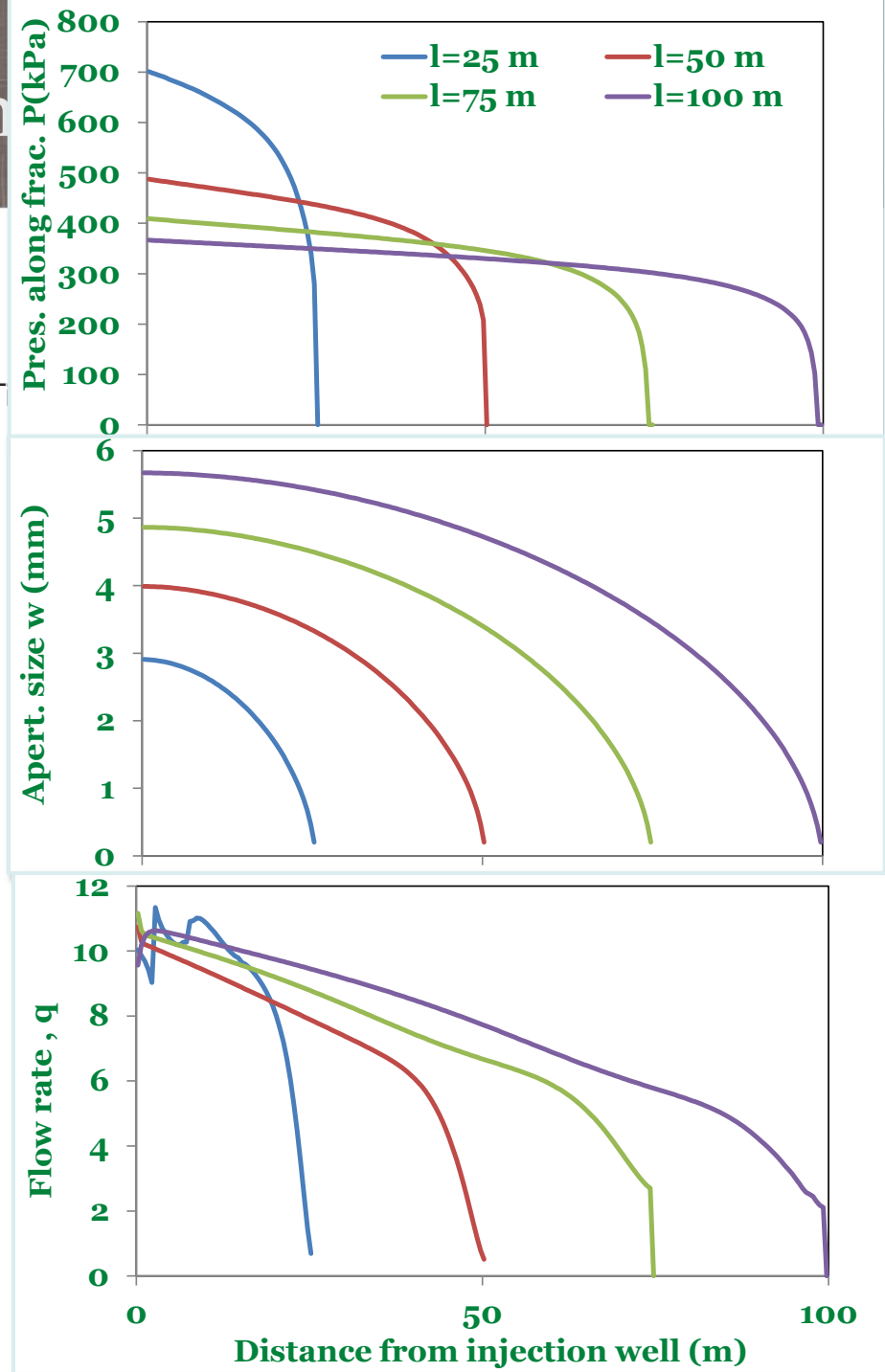




Model verification

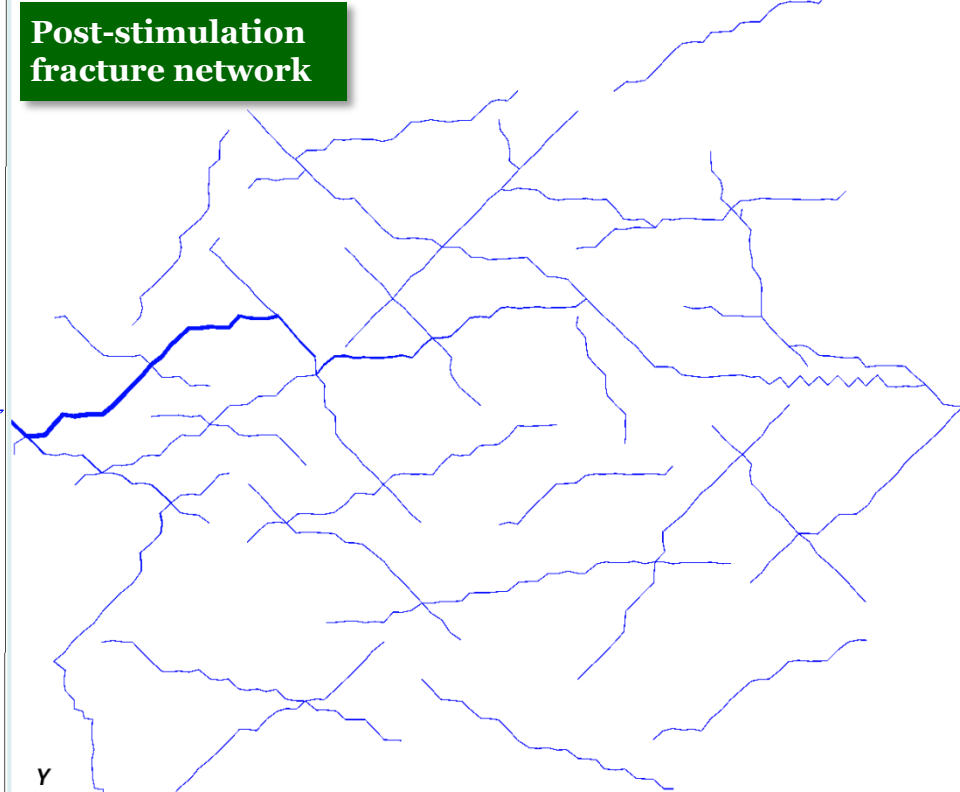
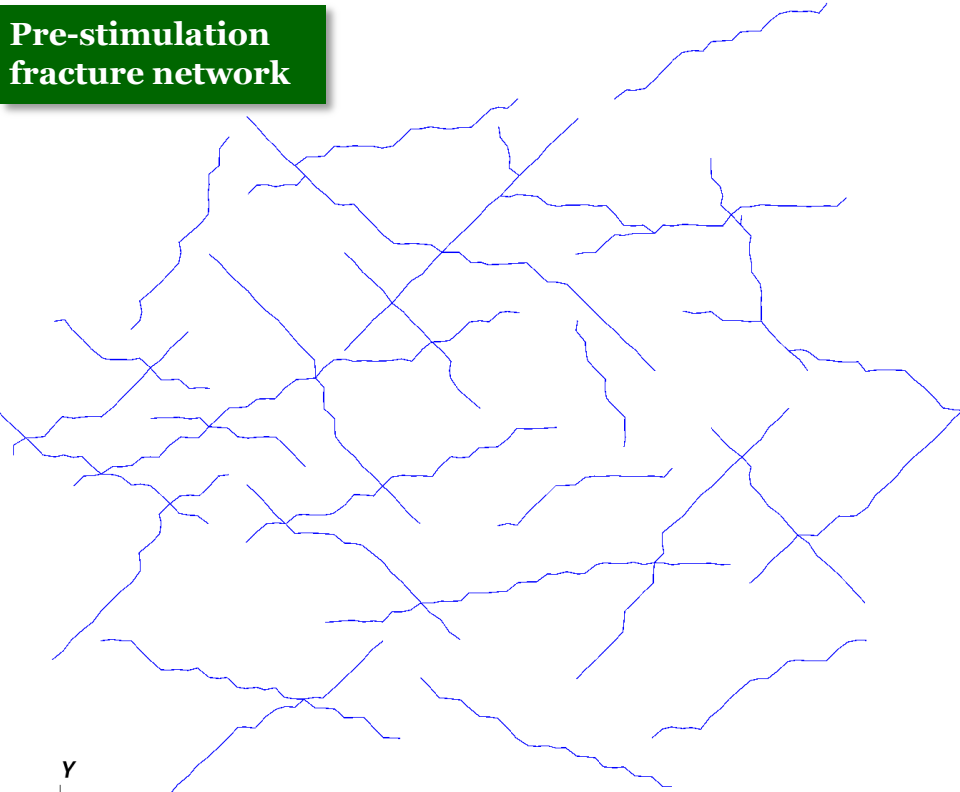


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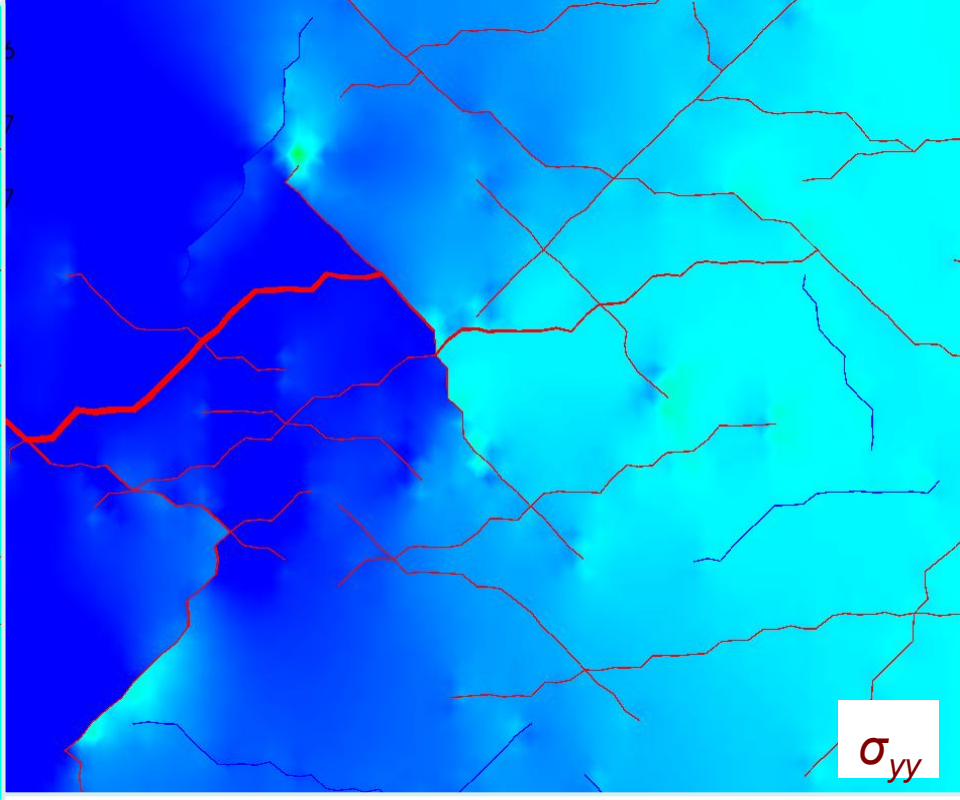
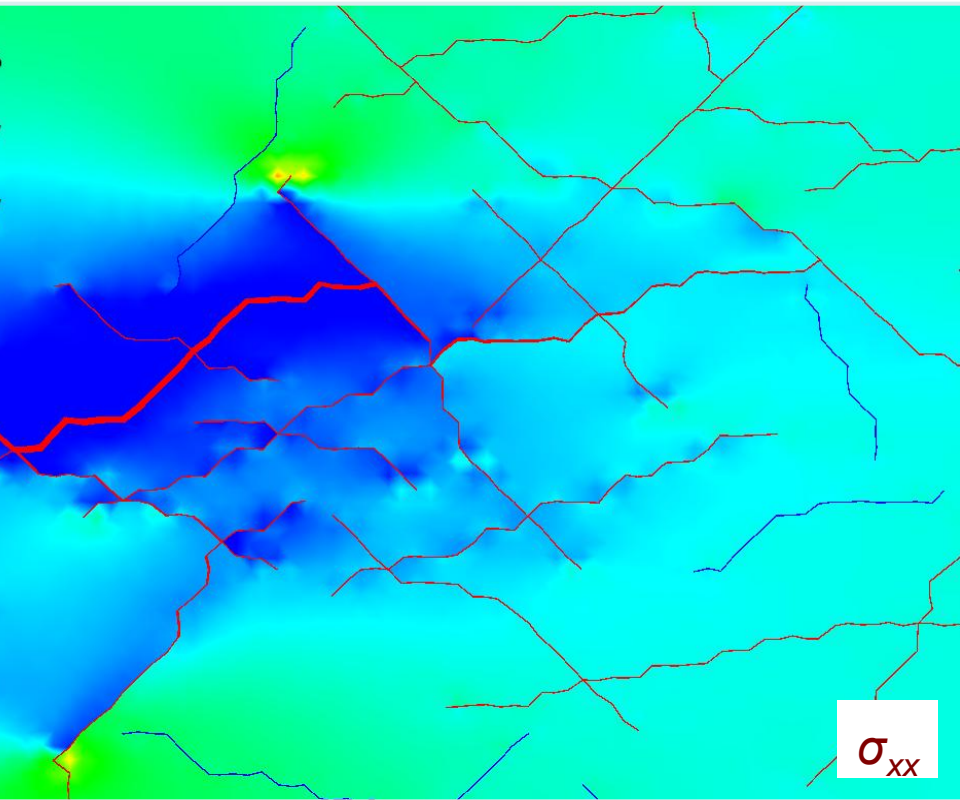


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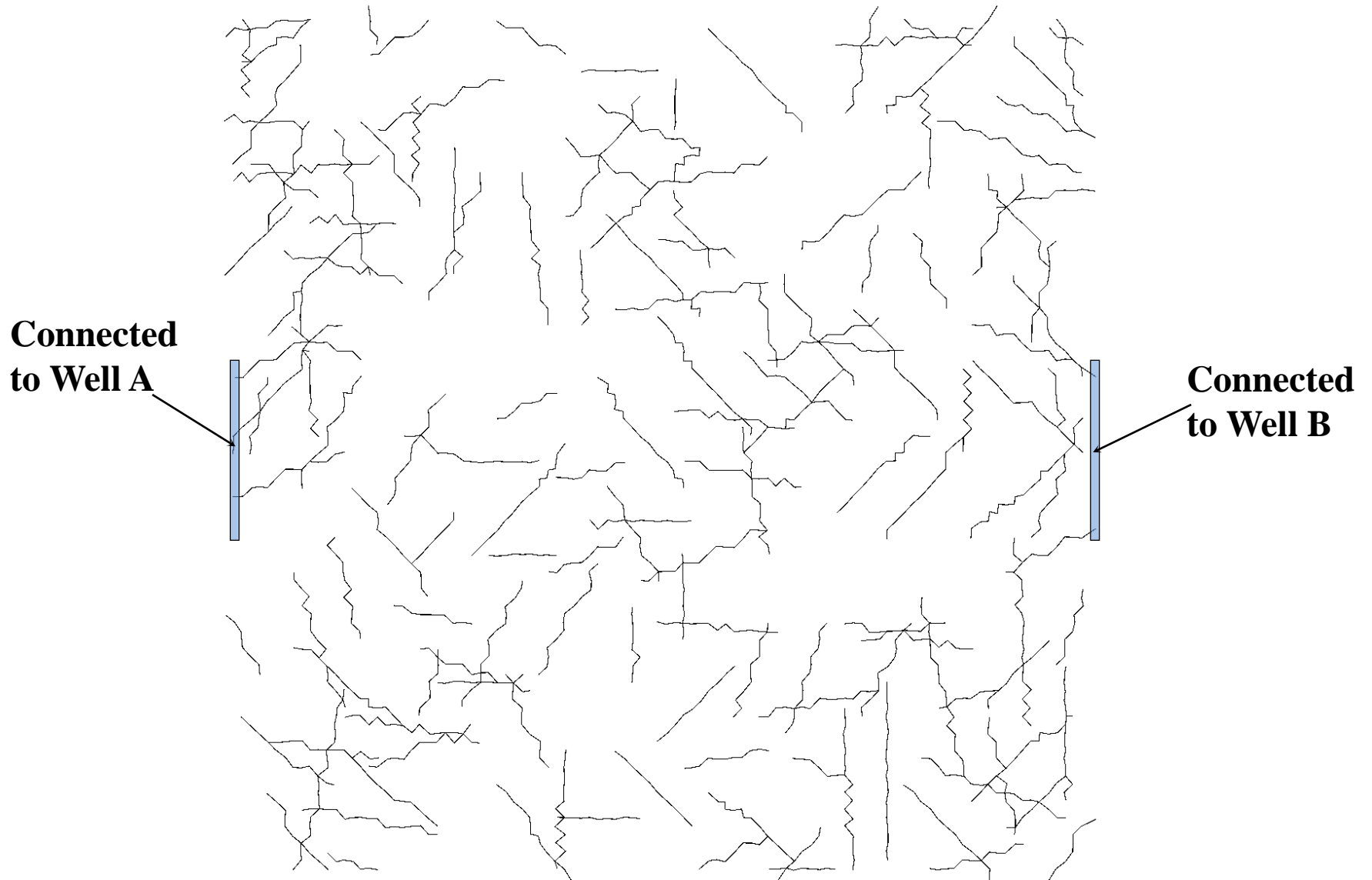


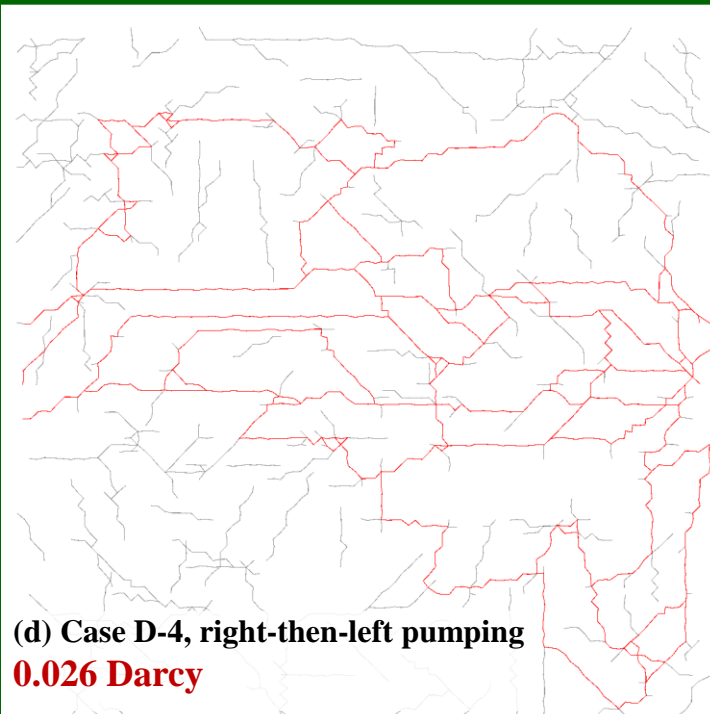
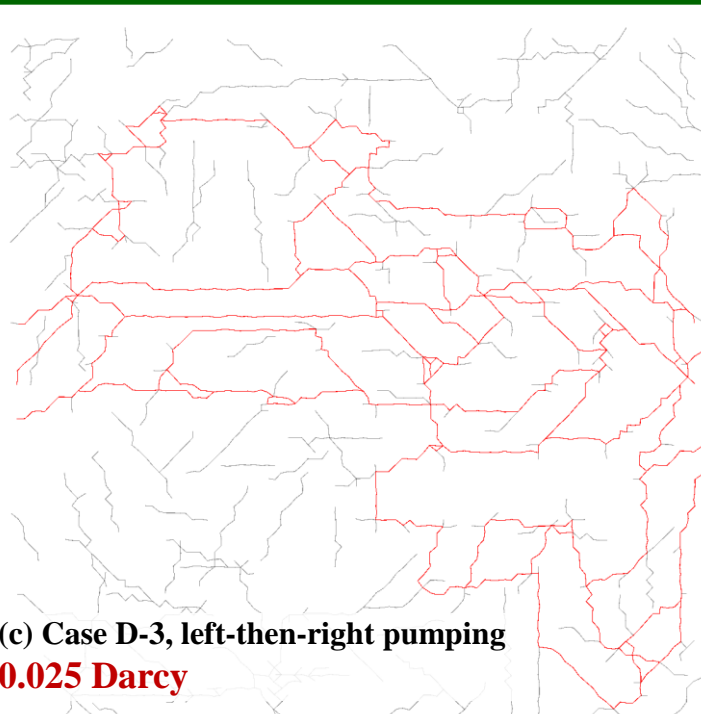
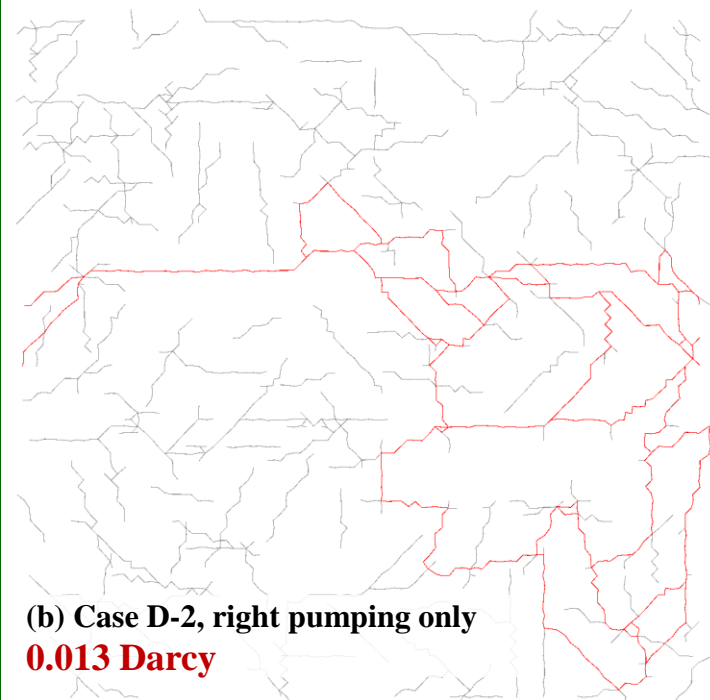
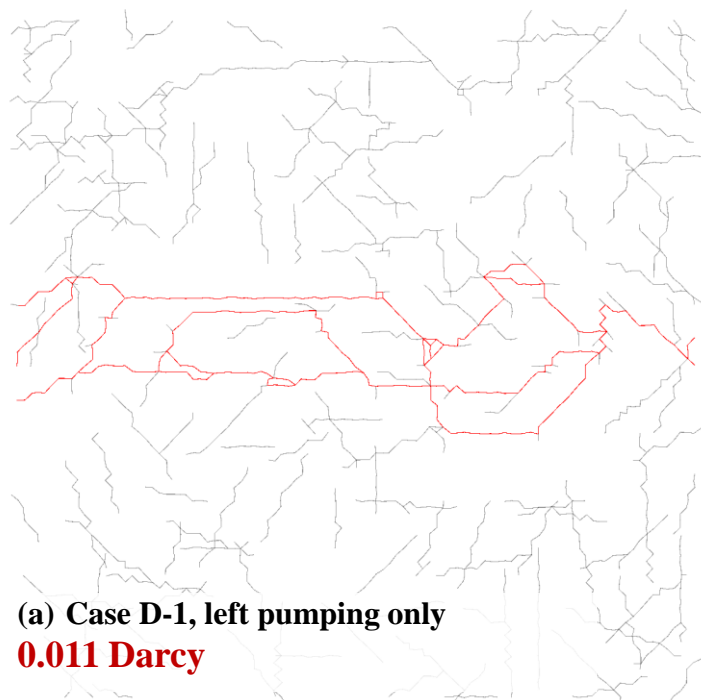
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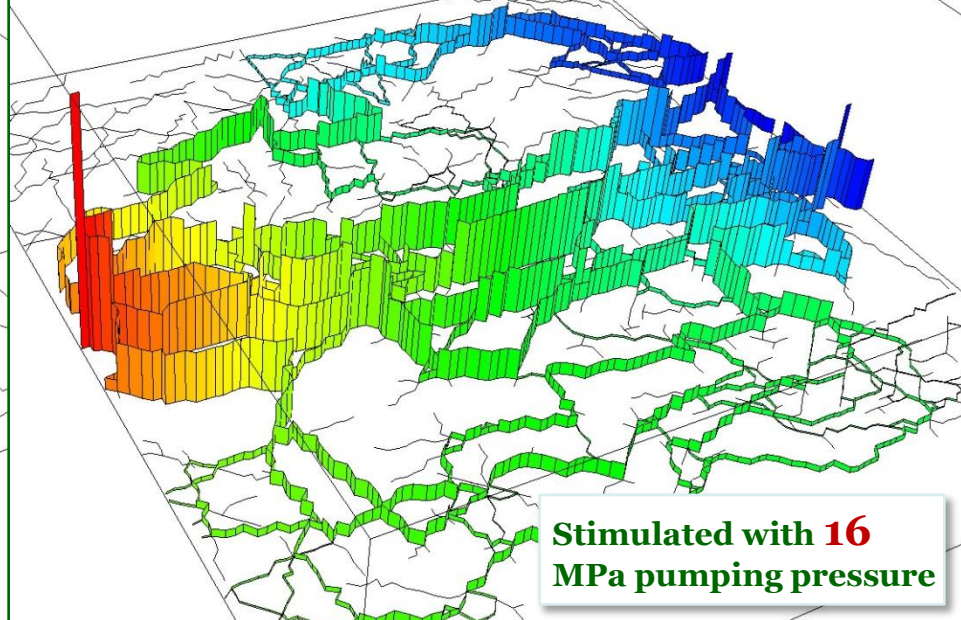
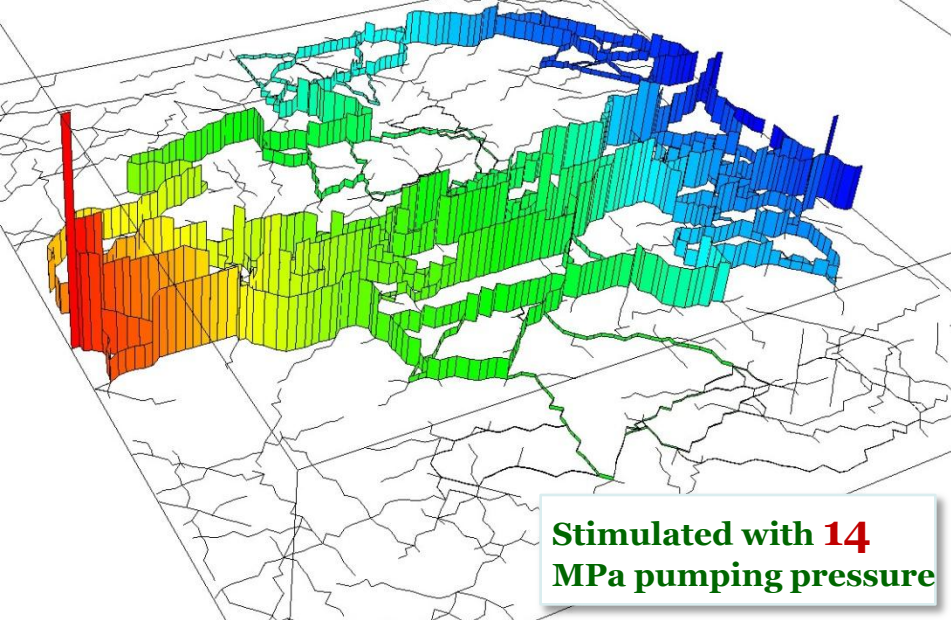
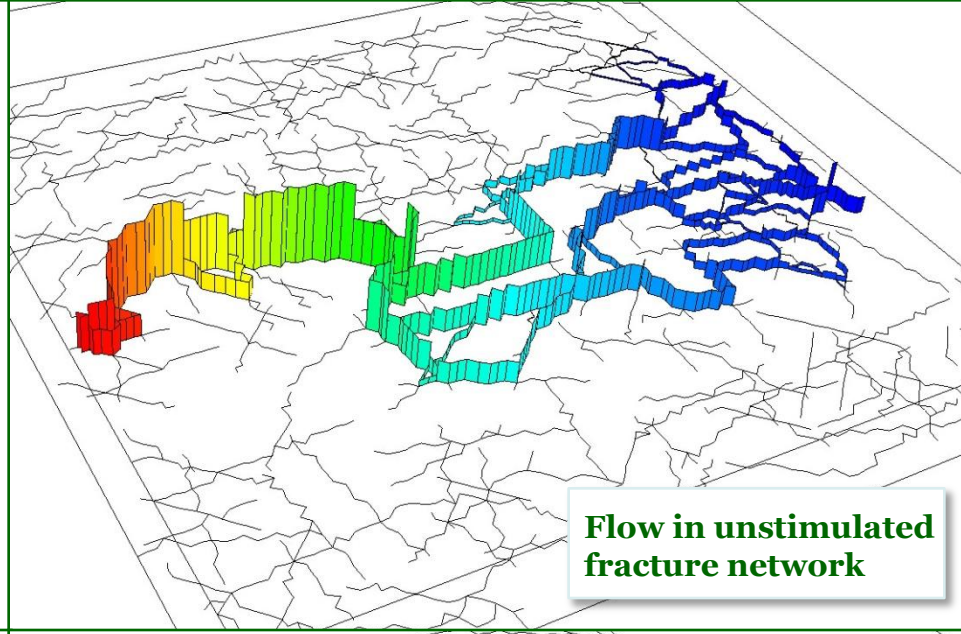
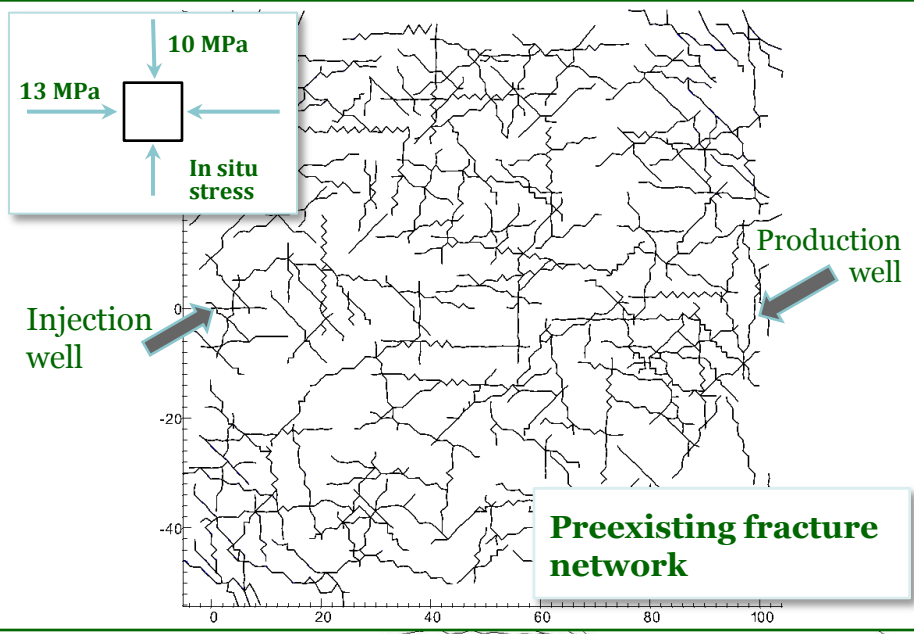


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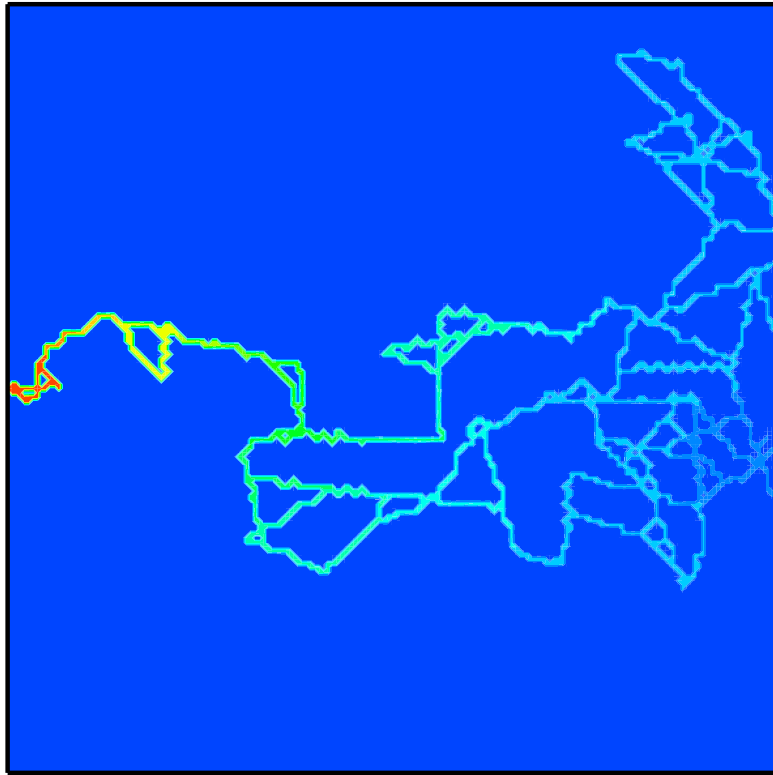


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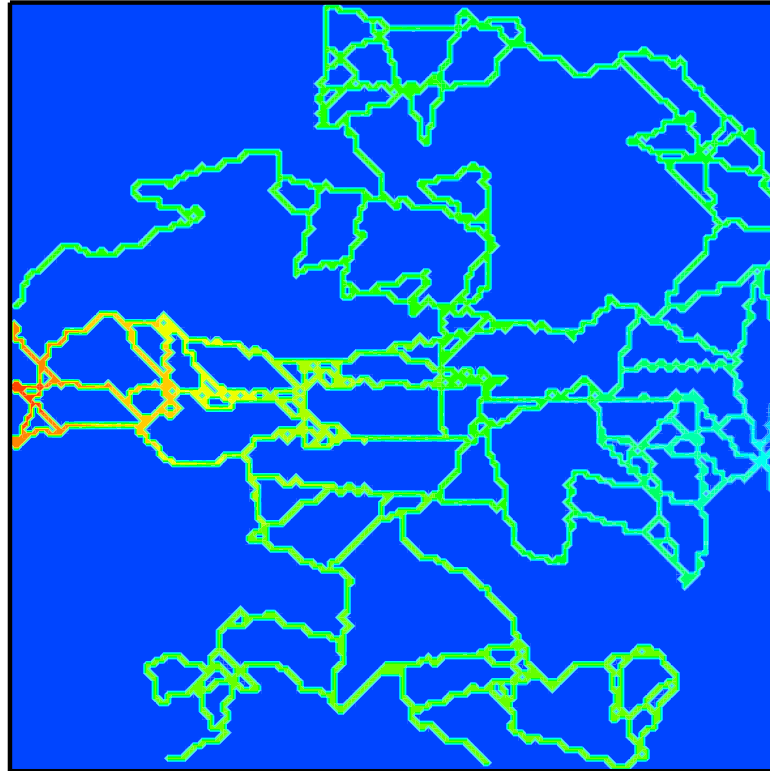




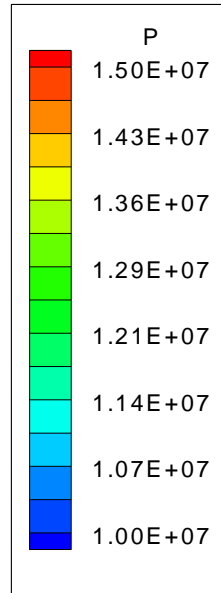
Application to more complex fracture networks



Before stimulation



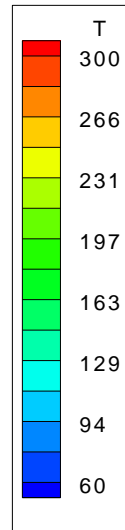
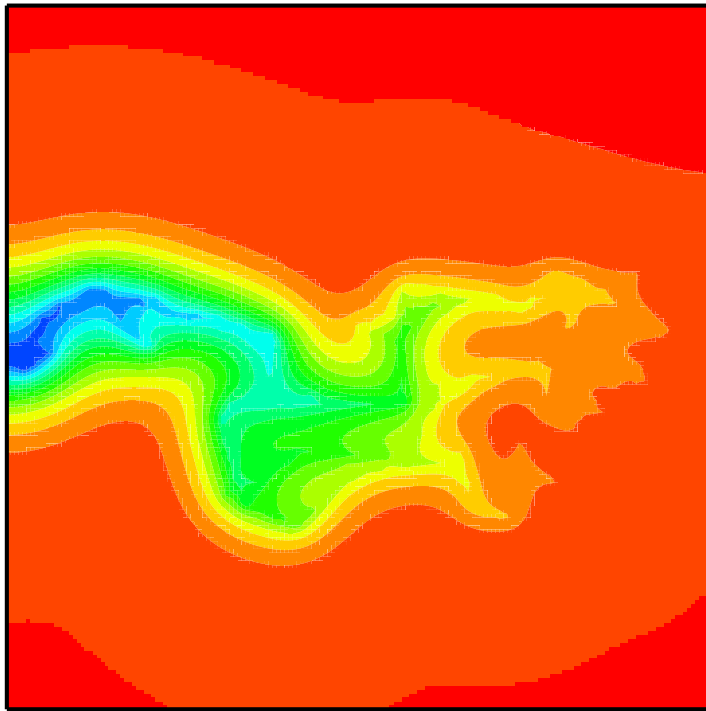
After stimulation





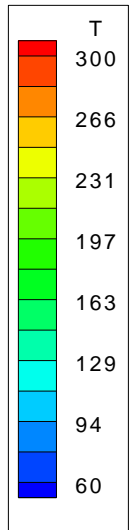
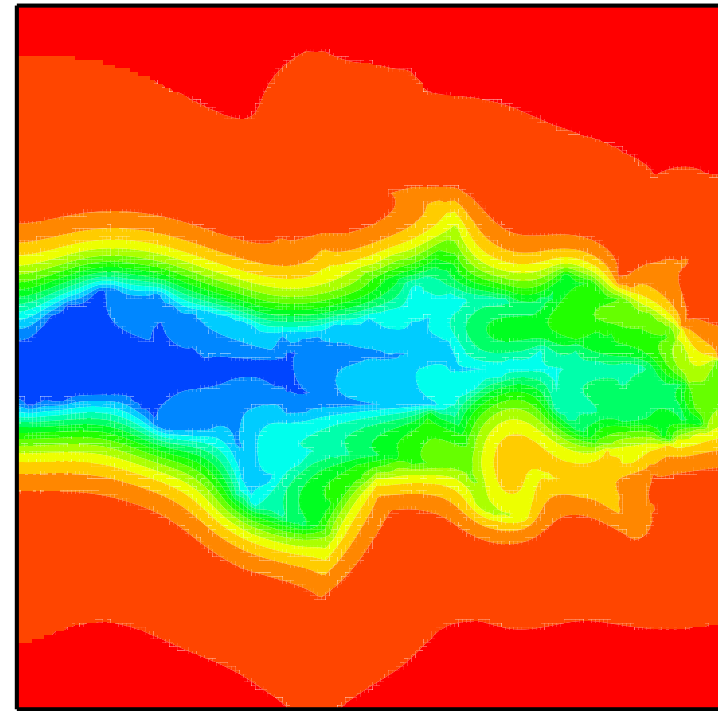
Application to more complex fracture networks

5 years



Before stimulation

5 years



After stimulation