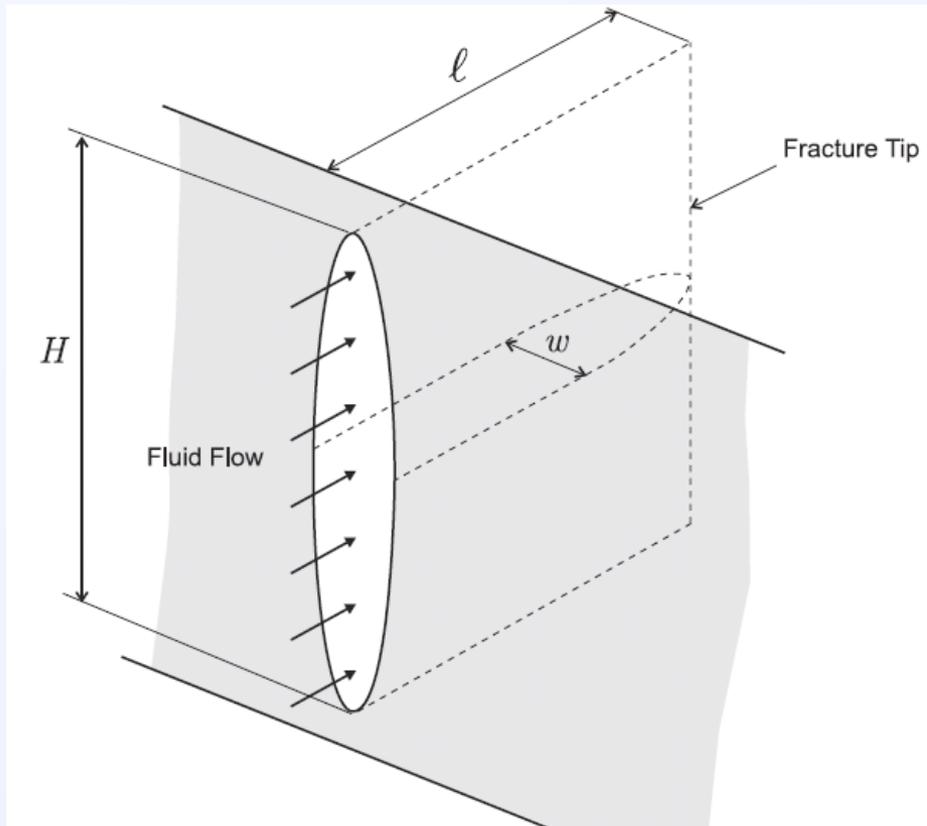


Investigation of **Stimulation-Response** Relationships for Complex Fracture Systems in Enhanced Geothermal Reservoirs

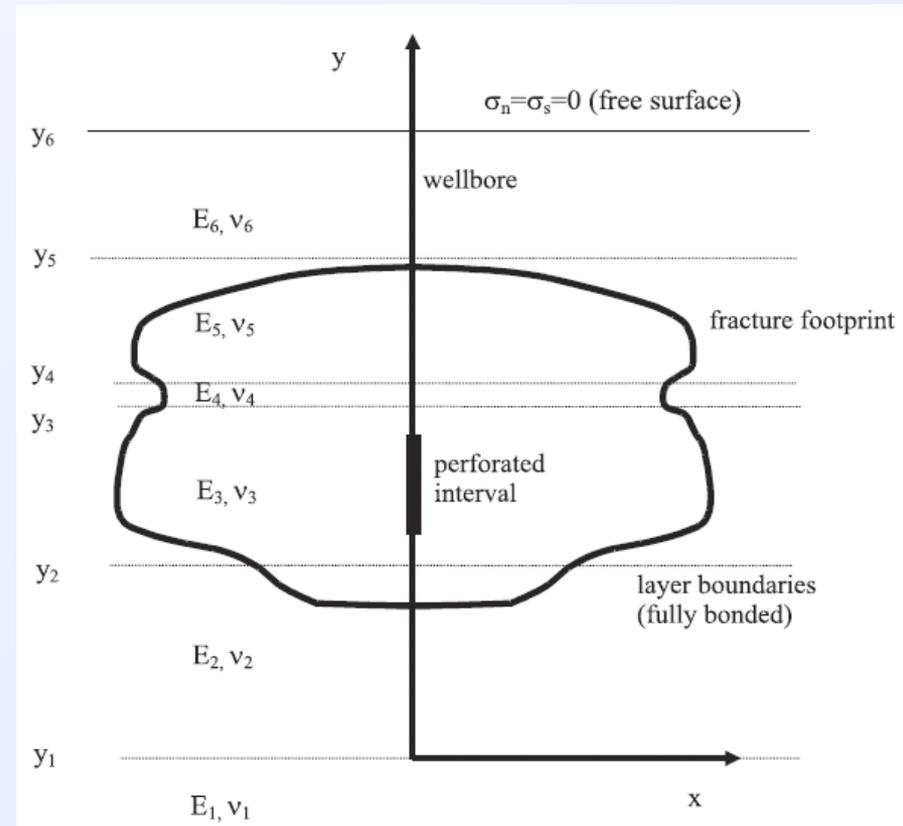
Pengcheng Fu, Scott M. Johnson, and Charles R. Carrigan



Conventional fracture models



PKN model

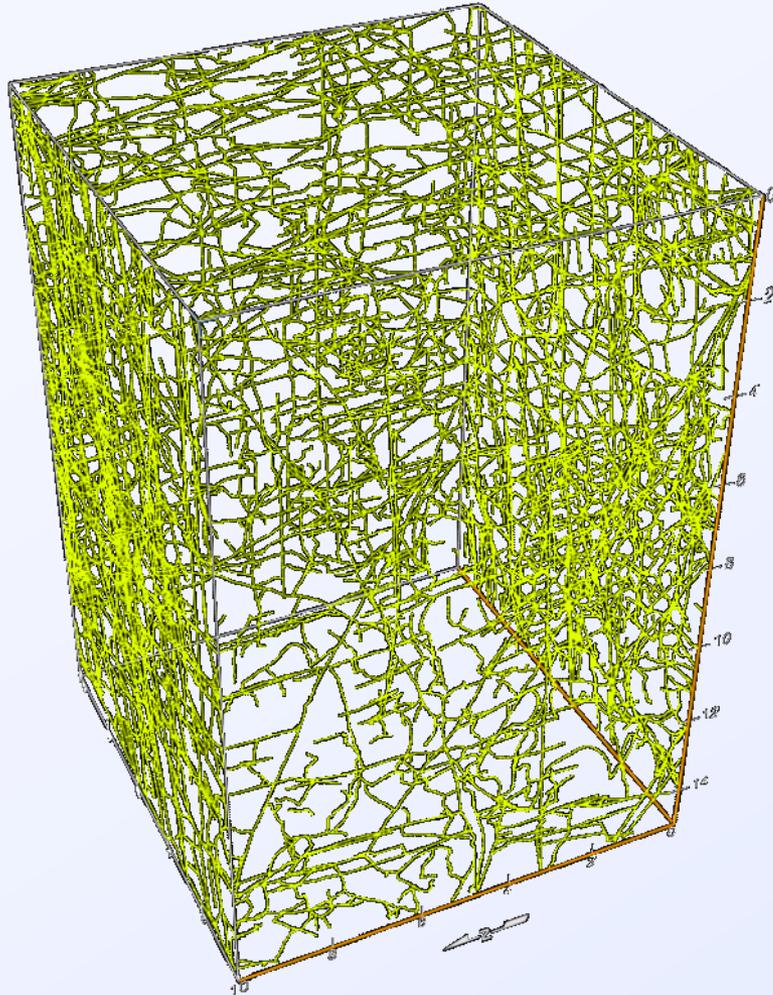


PL3D model

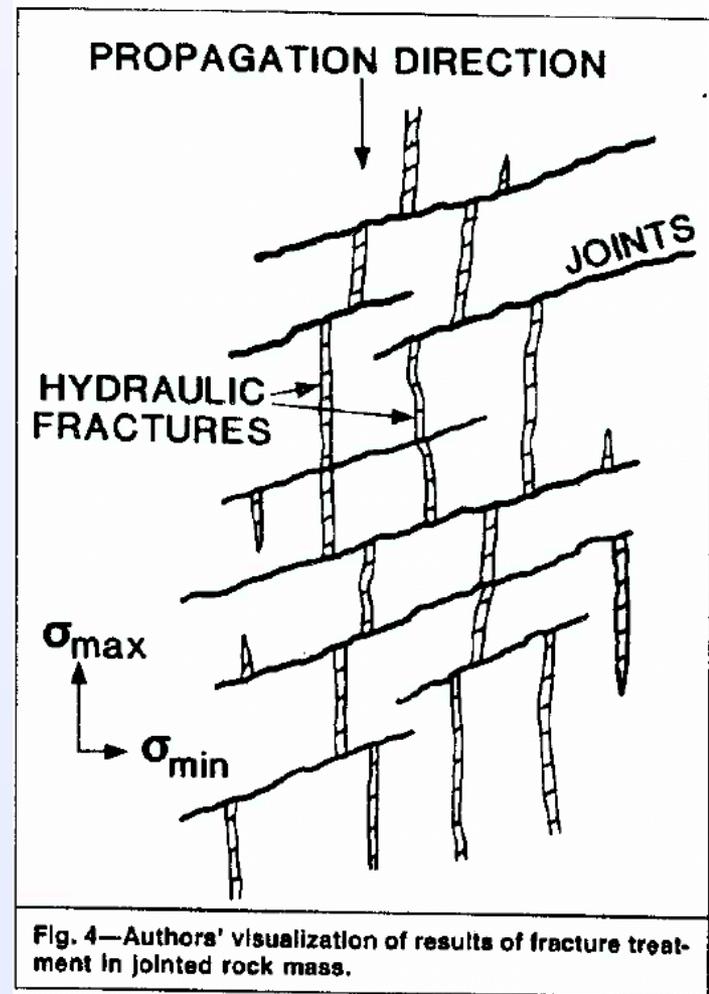
(Image credit: Adachi et al. 2000)



How real fracture system looks like



(Large Block Test, Yucca Mountain.
Wagoner, 2000)

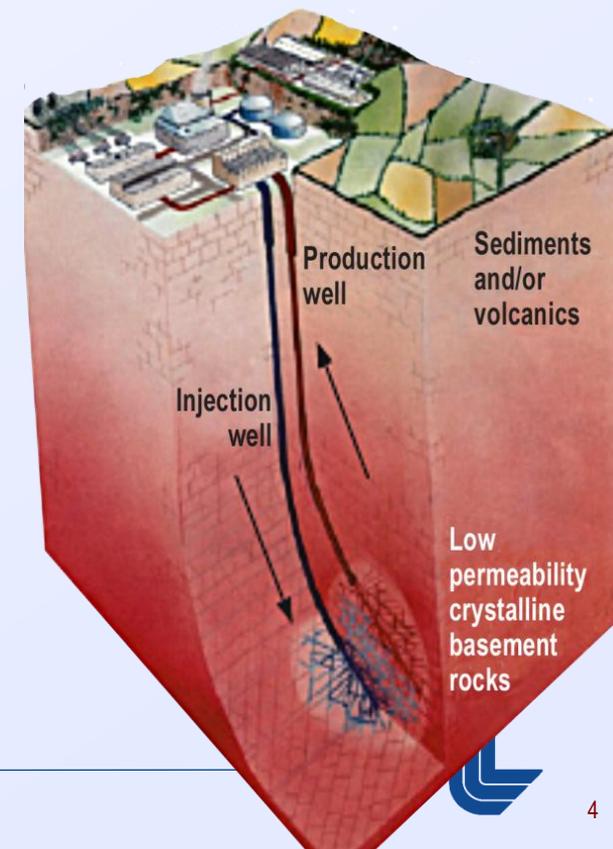


(Warpinski and Teufel, 1987)

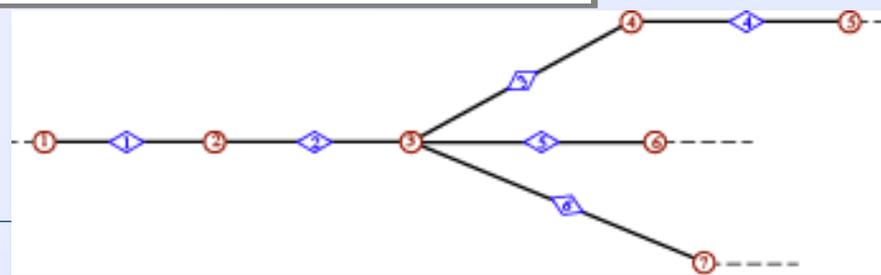
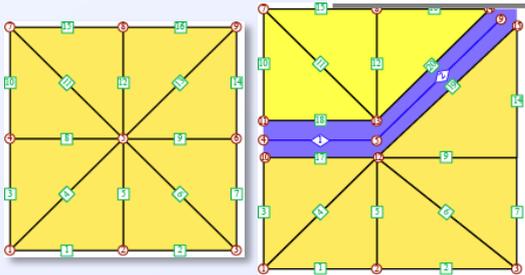
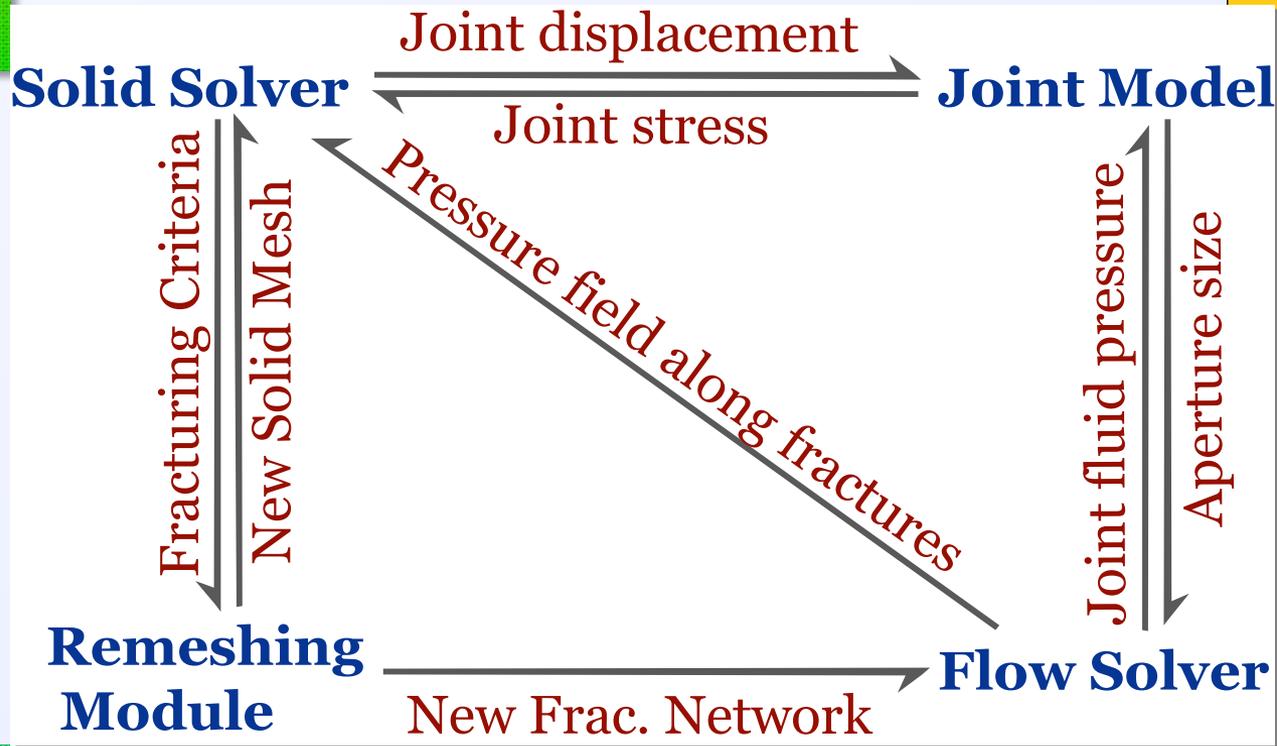
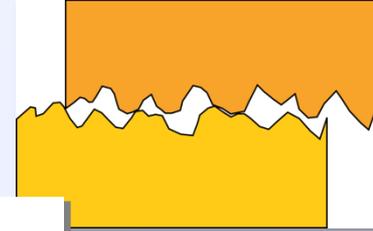
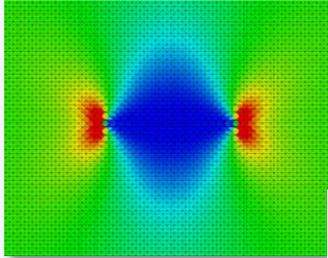


What do we need to simulate hydraulic stimulation of reservoir

- **Objective:**
 - Study the effectiveness of stimulation strategies through simulating fluid-fracture and fracture-fracture interactions.
- **Physical mechanisms need to be covered:**
 - Fluid flow due to pressure gradient;
 - Rock deformation;
 - Variation of aperture width; and
 - Rock fracturing.
- **Other variables:**
 - Natural fracture system;
 - *In situ* stress;
 - Stimulation parameters.



Modules and their coupling



Important Components

- Flow solver – Finite volume method

$$\frac{\partial q}{\partial l} + \frac{\partial w^h}{\partial t} = 0 \quad \kappa \frac{\partial P}{\partial l} = -q$$

$$\kappa_{ij} = \frac{w_{ij}^{h3}}{6\mu(L_i + L_j)}$$

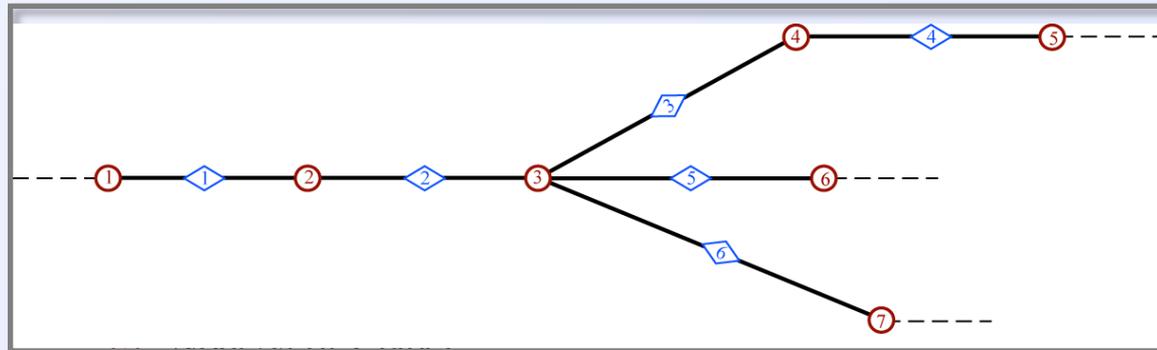
$$w_{ij}^{h3} = \frac{w_i^{h3} w_j^{h3} (L_i + L_j)}{w_i^{h3} L_j + w_j^{h3} L_i}$$

$$\dot{V}_{ij} = \kappa_{ij} (P_i - P_j)$$

$$P_i = \begin{cases} K \left(\frac{m_i}{V_i \rho_{ref}} - 1 \right) & \text{if } m_i / V_i \geq \rho_{ref} \\ P_{vap} & \text{if } m_i / V_i < \rho_{ref} \end{cases}$$

Two mechanisms:

- Flow in fractures due to pressure gradient.
- Mass conservation with varying total fracture volume.

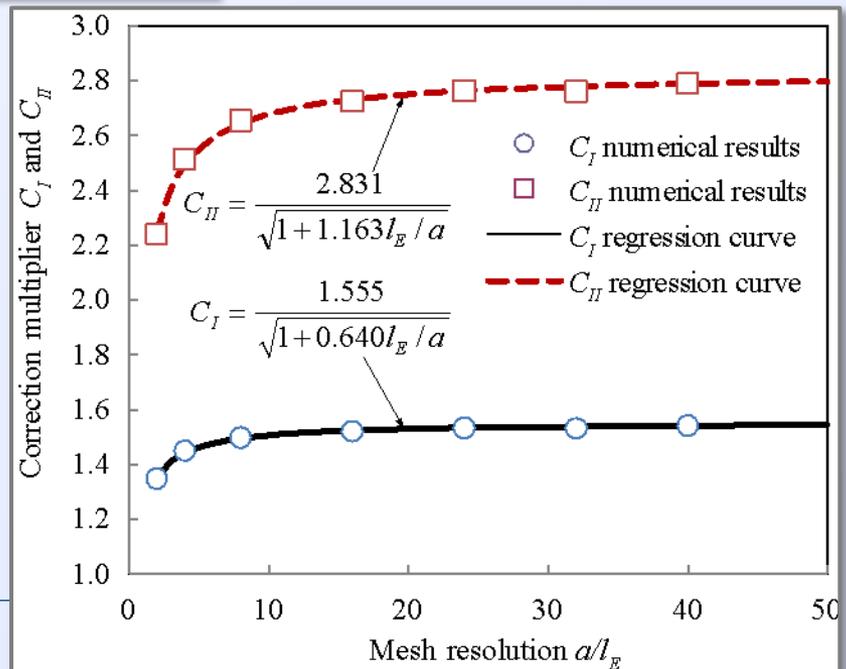
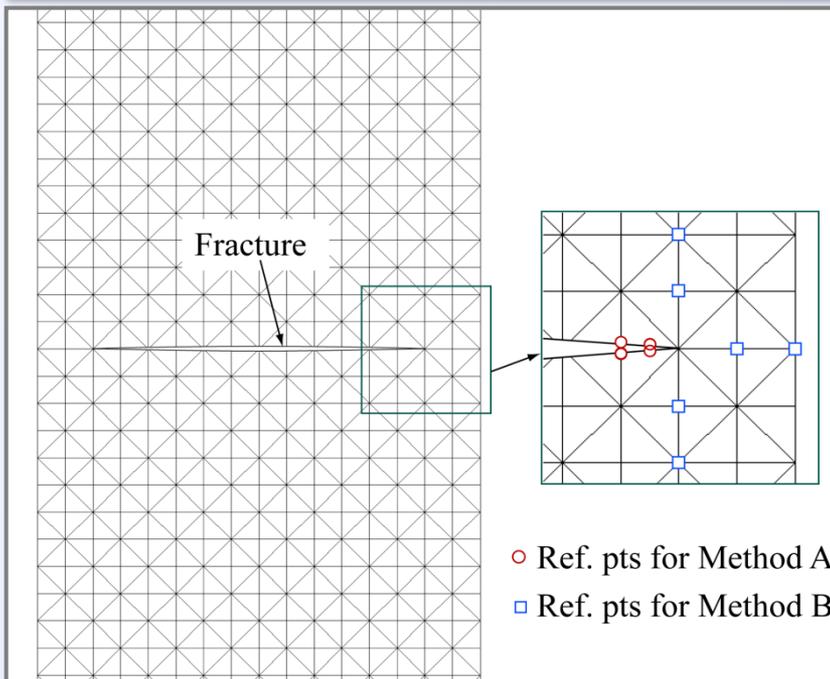


Important Components

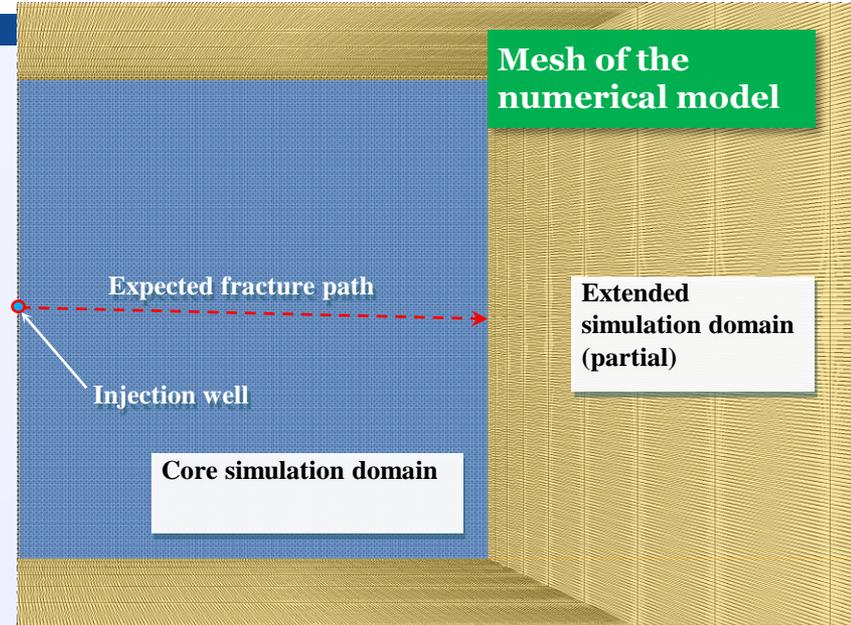
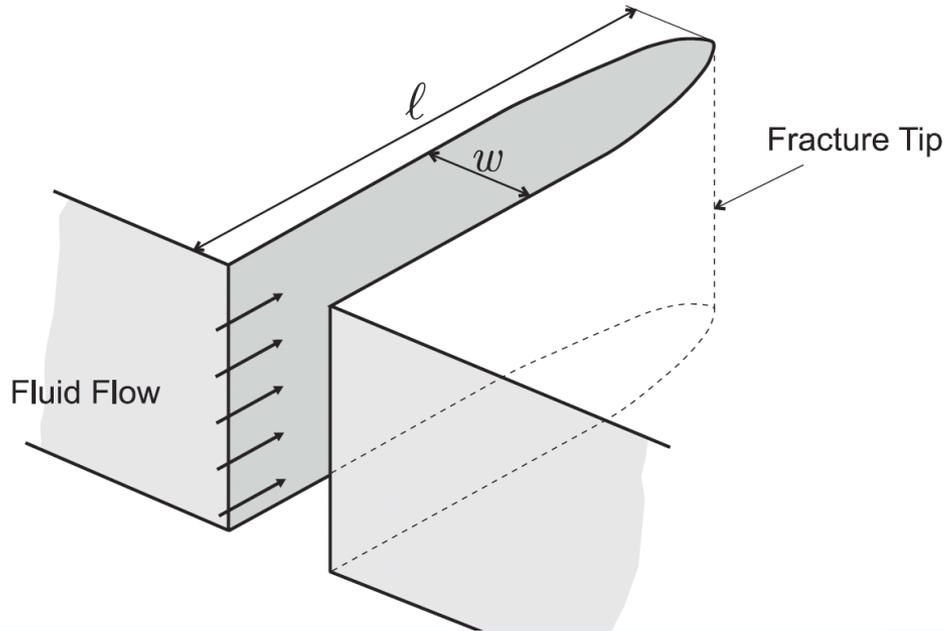
- Fracturing criterion (LEFM)
 - Generalized displacement correlation method.
 - Based on critical stress intensity function

$$K_I = C_I \frac{2u_\theta(l_E/2, \pi) - 2u_\theta(l_E/2, -\pi) - u_\theta(l_E, \pi) + u_\theta(l_E, -\pi)}{(2\sqrt{2} - 2)\sqrt{l_E} f_\theta^a(\pi)}$$

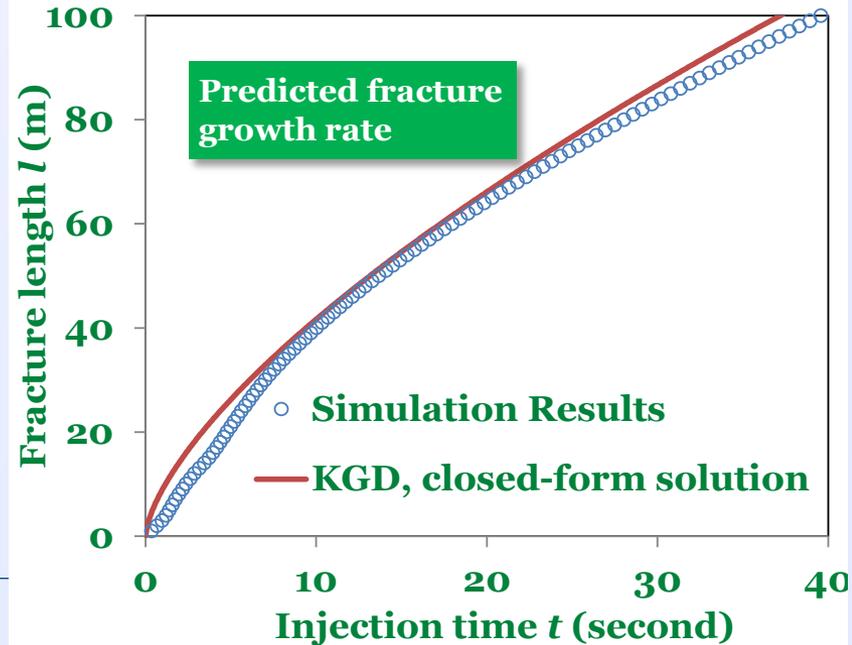
$$K_{II} = C_{II} \frac{2u_r(l_E/2, \pi) - 2u_r(l_E/2, -\pi) - u_r(l_E, \pi) + u_r(l_E, -\pi)}{(2\sqrt{2} - 2)\sqrt{l_E} f_r^b(\pi)}$$



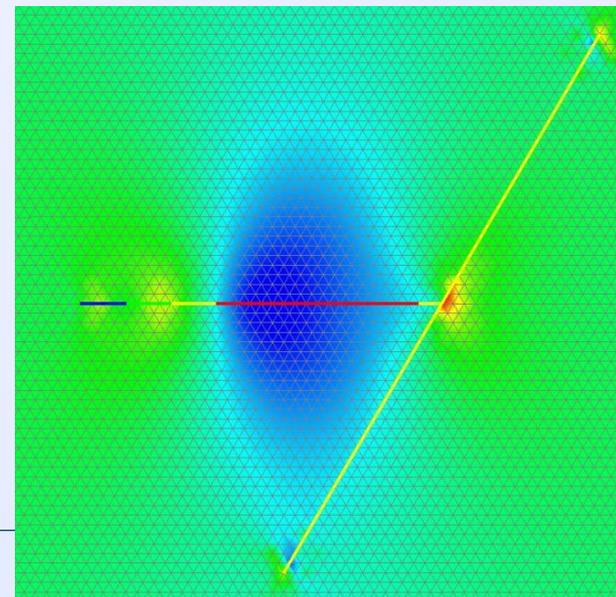
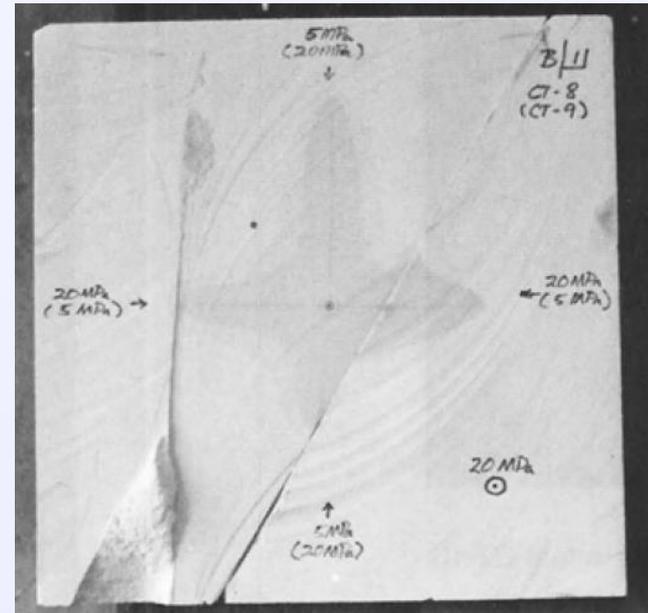
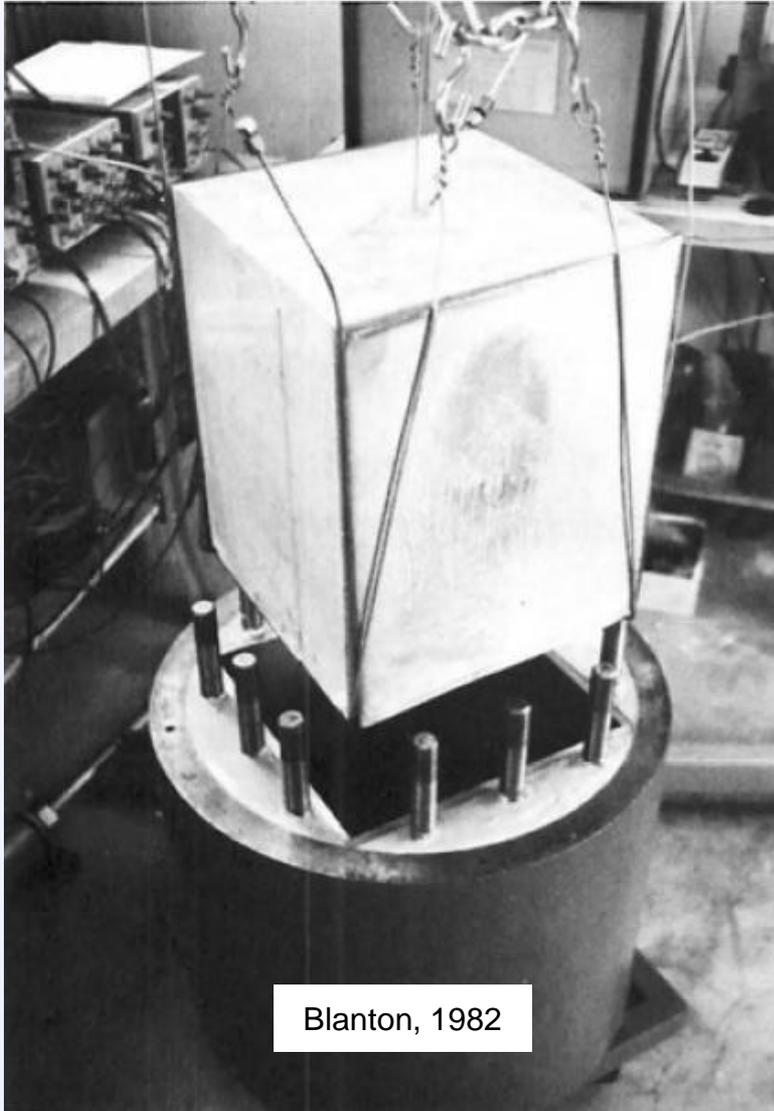
Model verification: classical KGD model



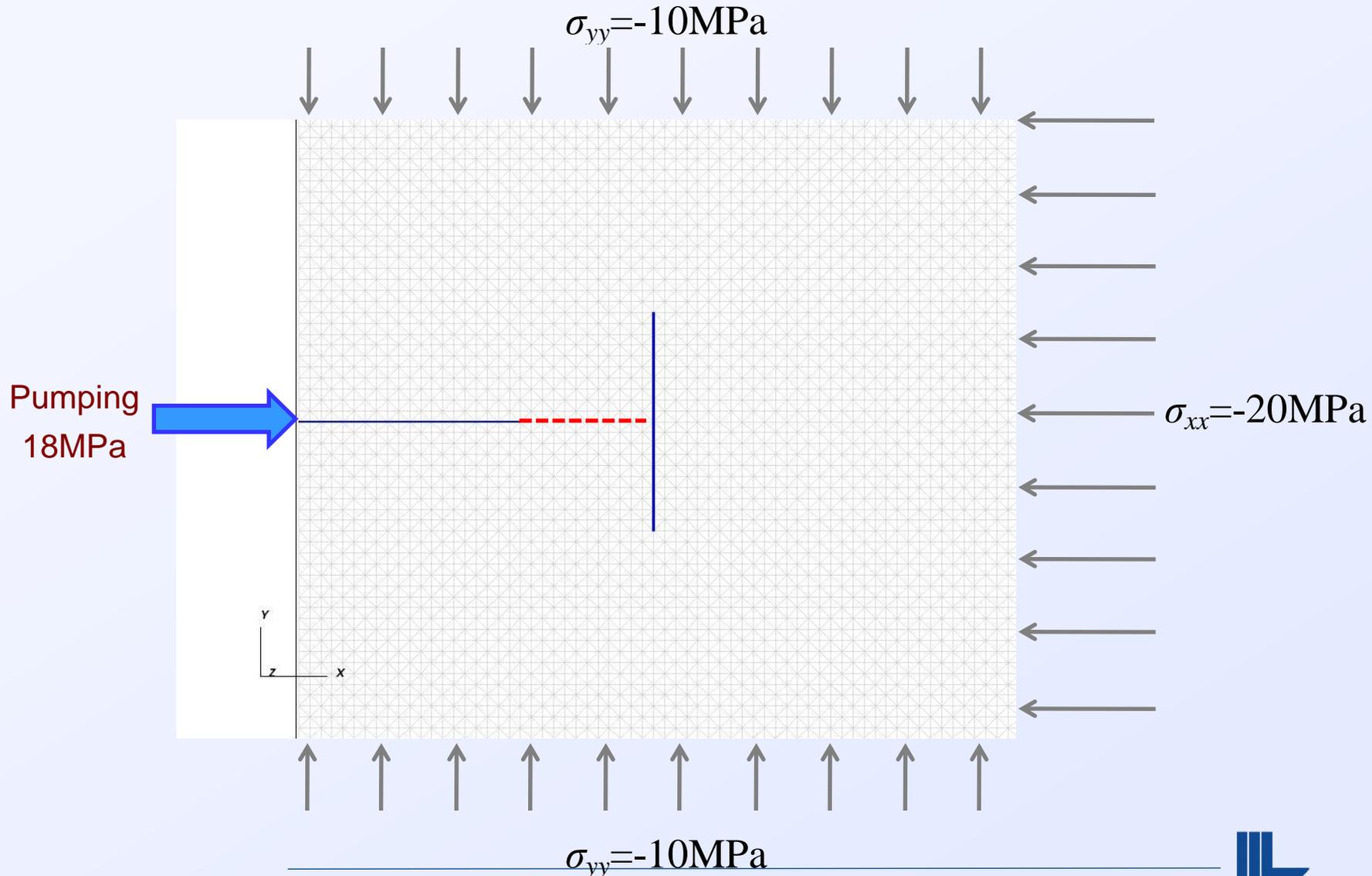
$$l(t) = 0.679 \left[\frac{Gq_0^3}{\mu(1-\nu)} \right]^{\frac{1}{6}} t^{\frac{2}{3}}$$



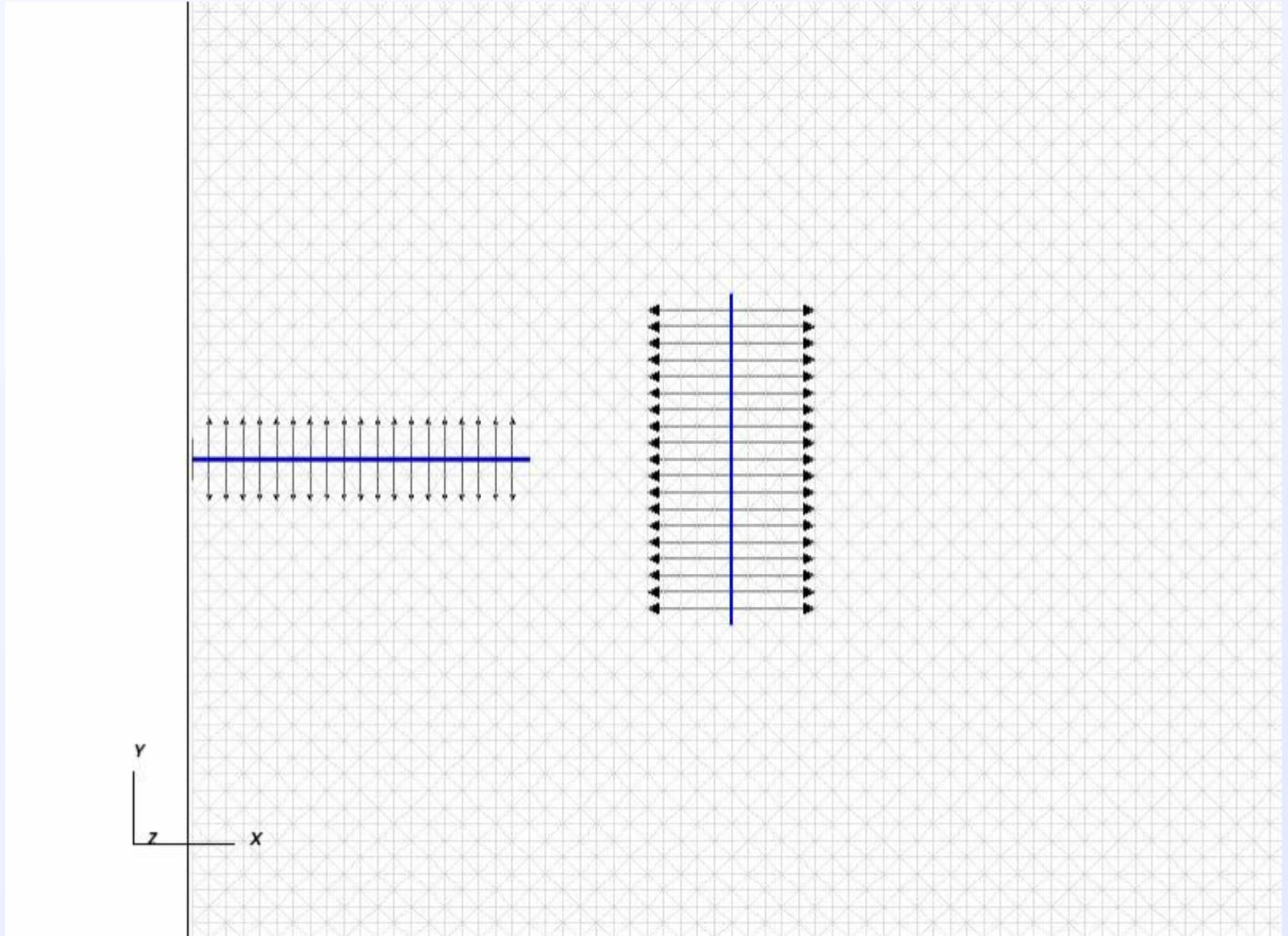
Model validation: lab test results



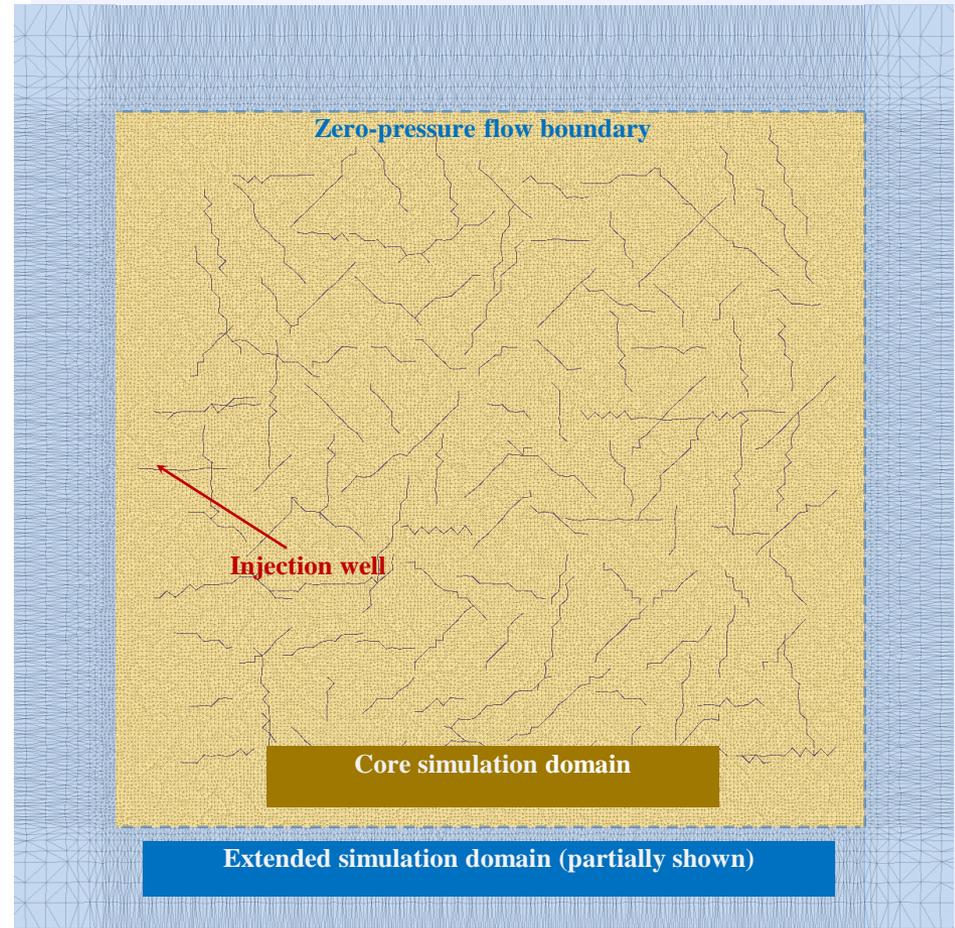
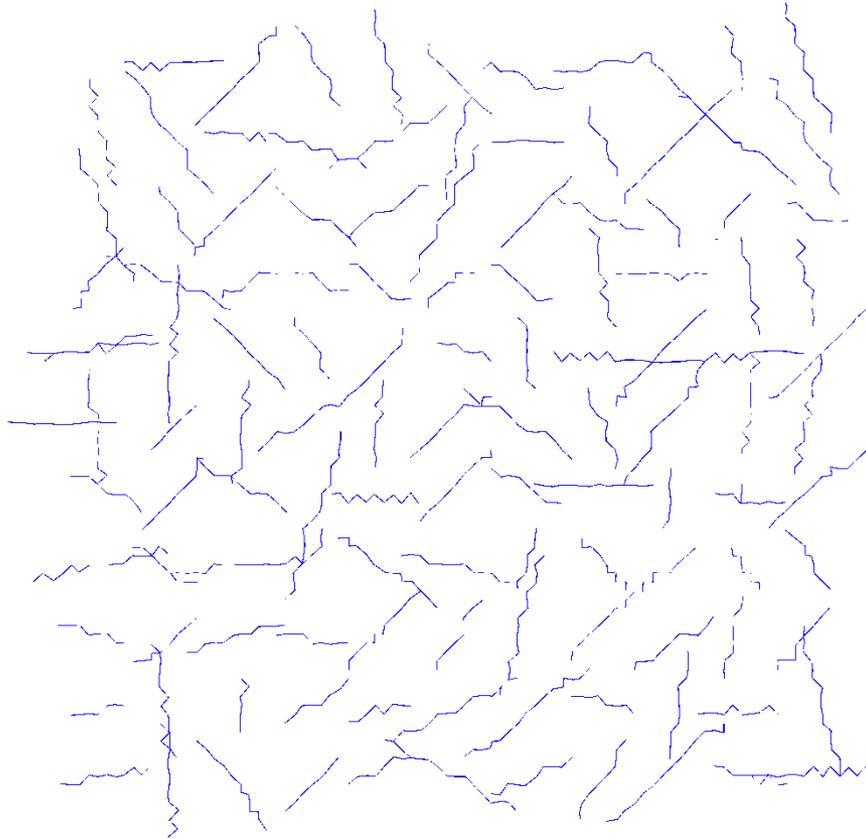
Interaction between propagating and existing fractures



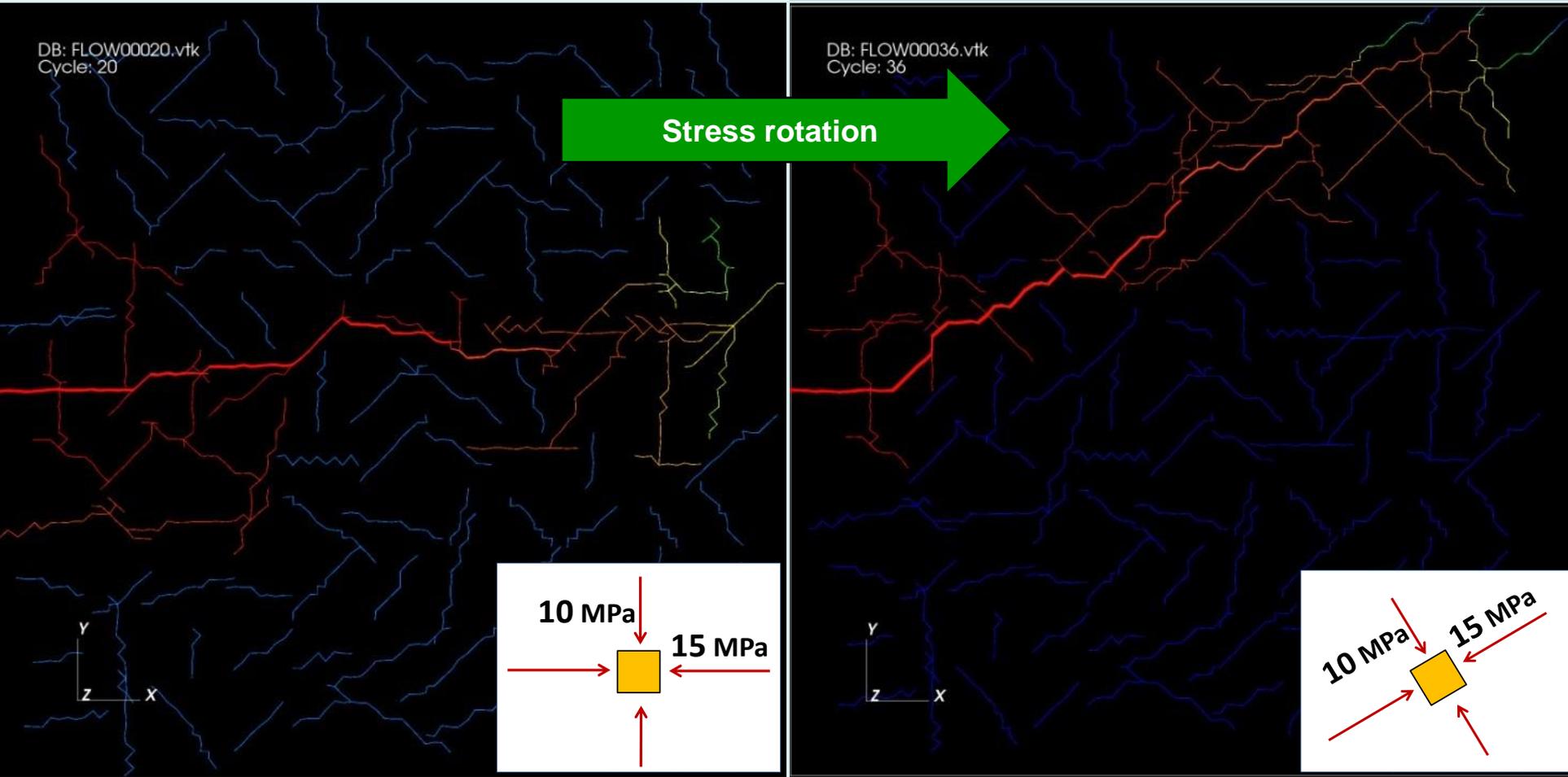
Interaction between propagating and existing Fractures



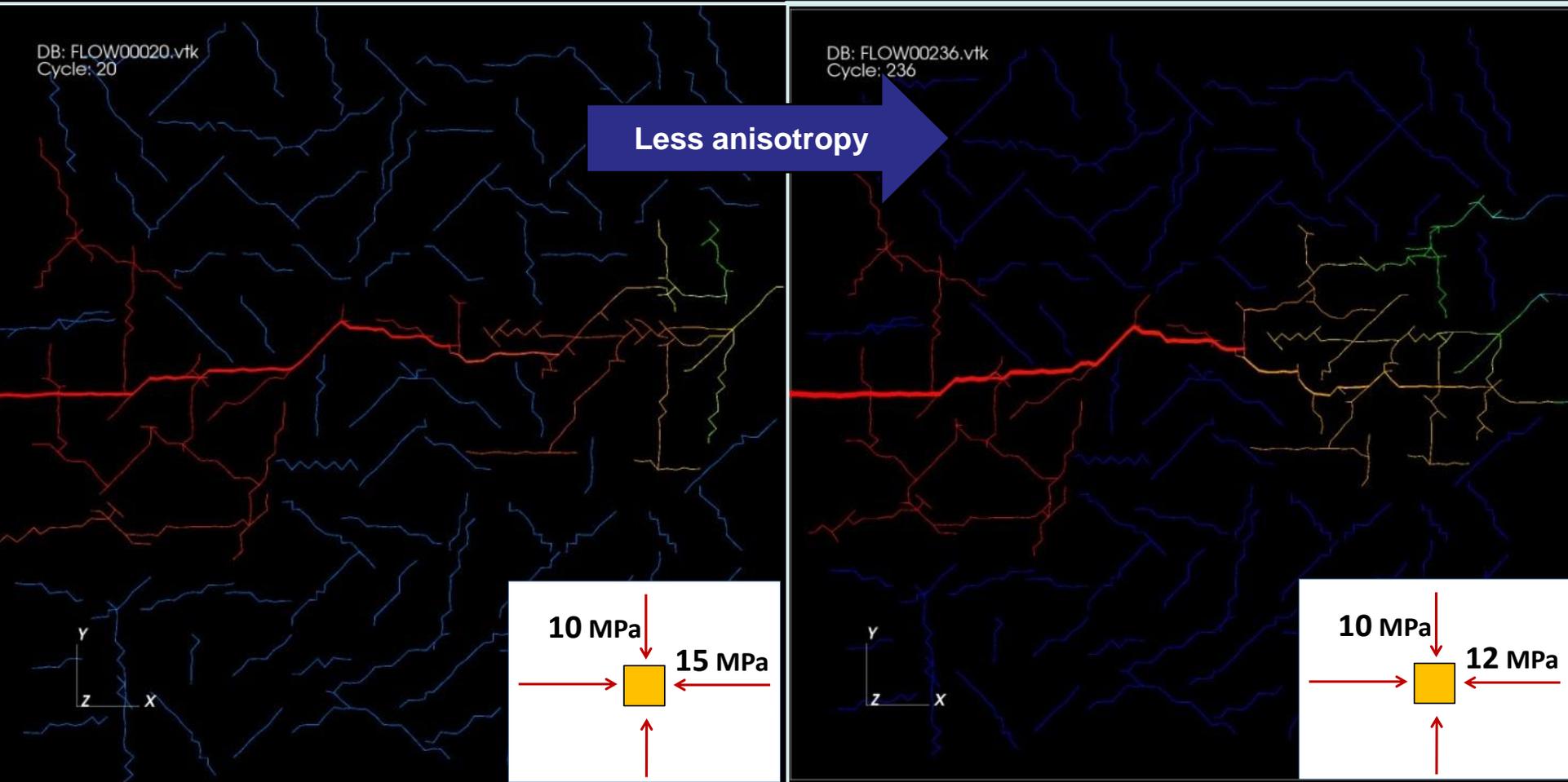
Application to more complex fracture networks



I: Effects of *in situ* stress: principal stress orientation & anisotropy



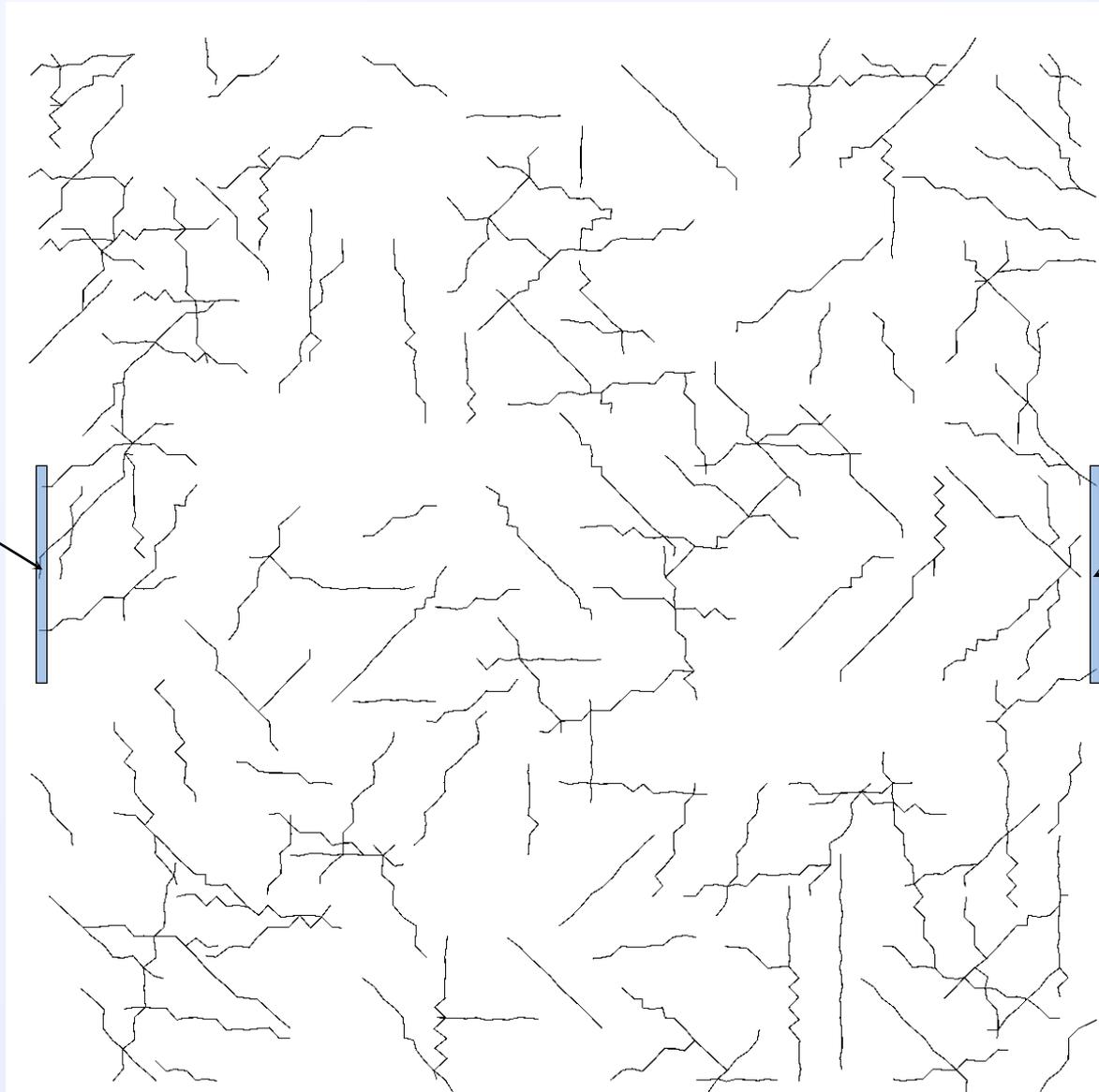
I: Effects of *in situ* stress: principal stress orientation & anisotropy





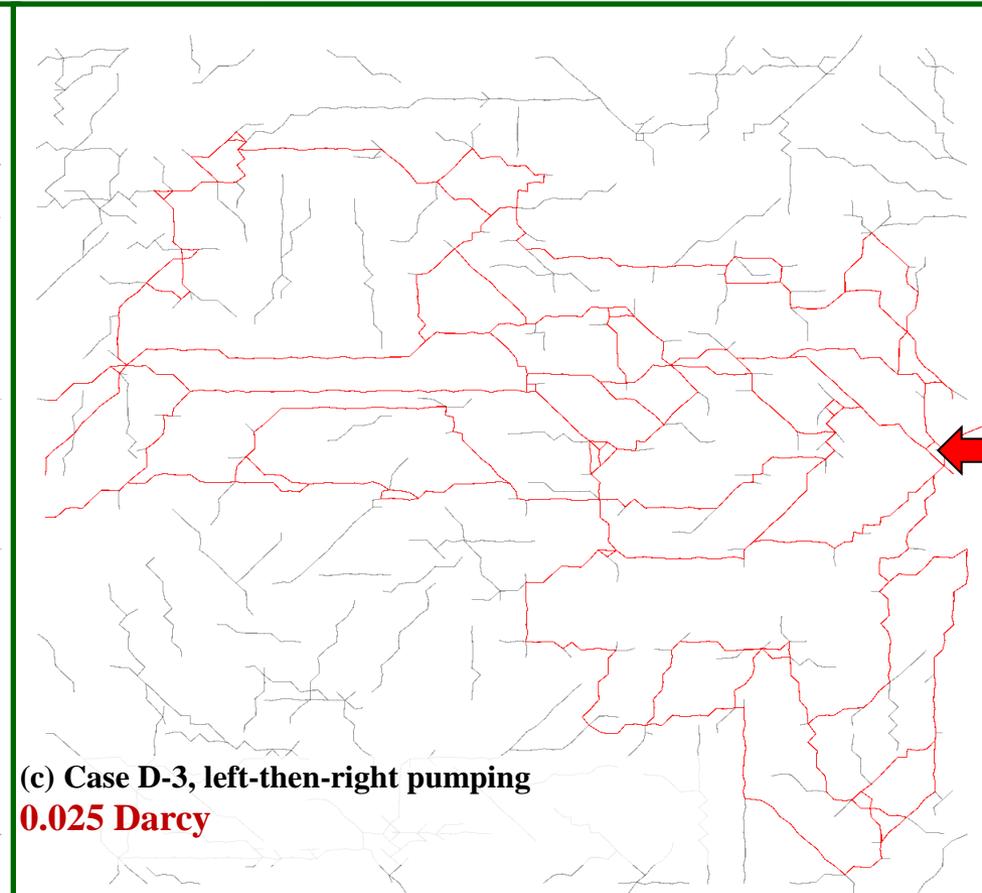
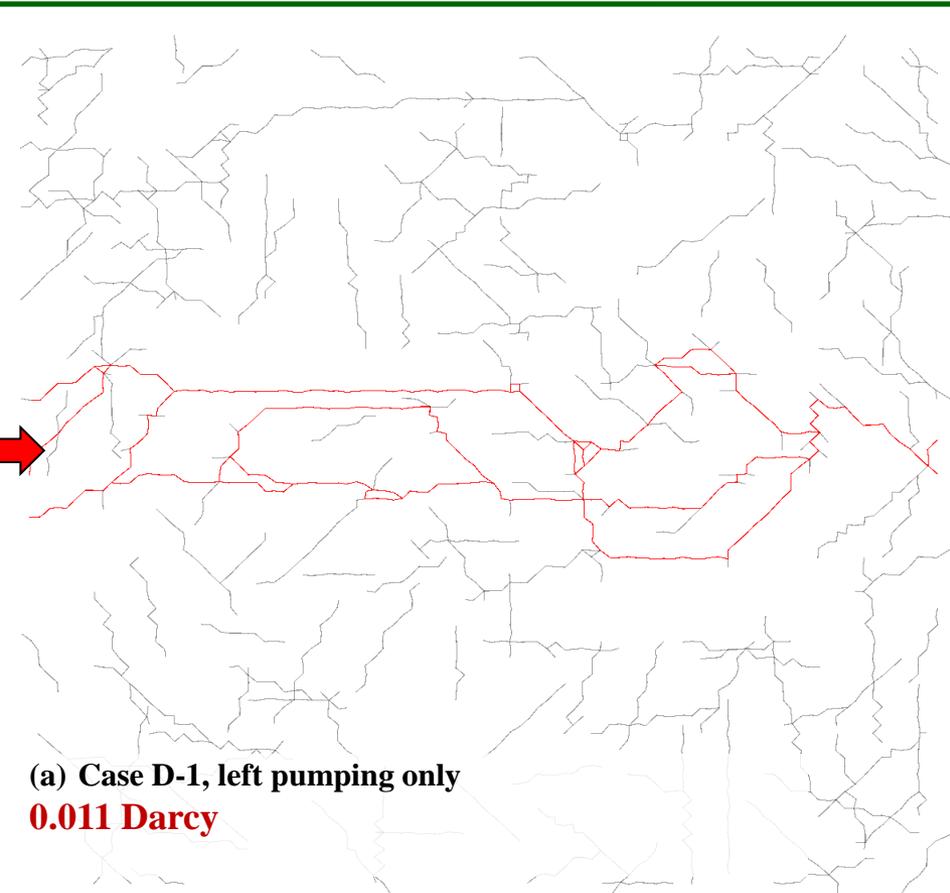
II: Multi-well stimulation

**Connected
to Well A**

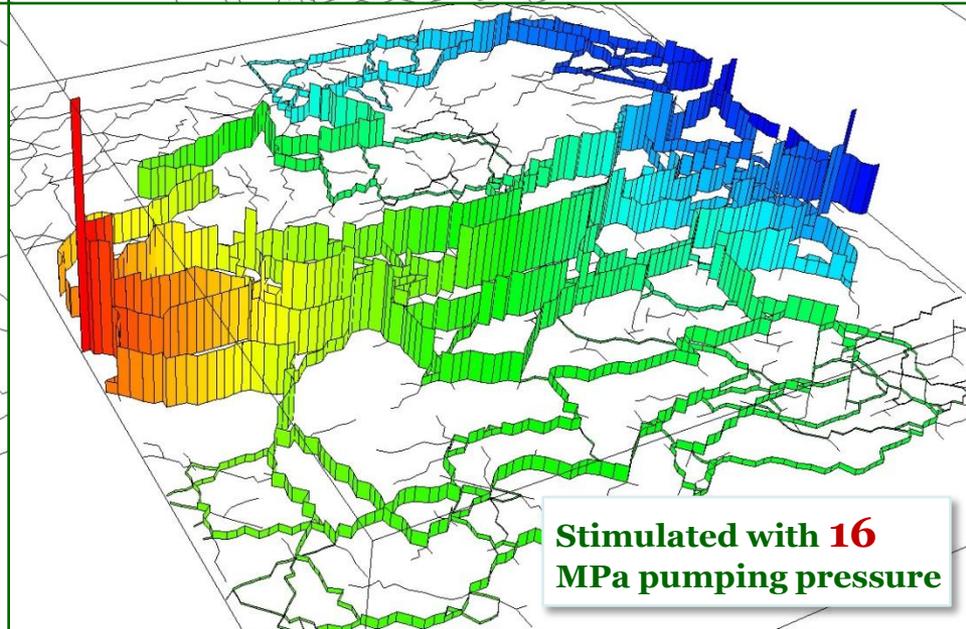
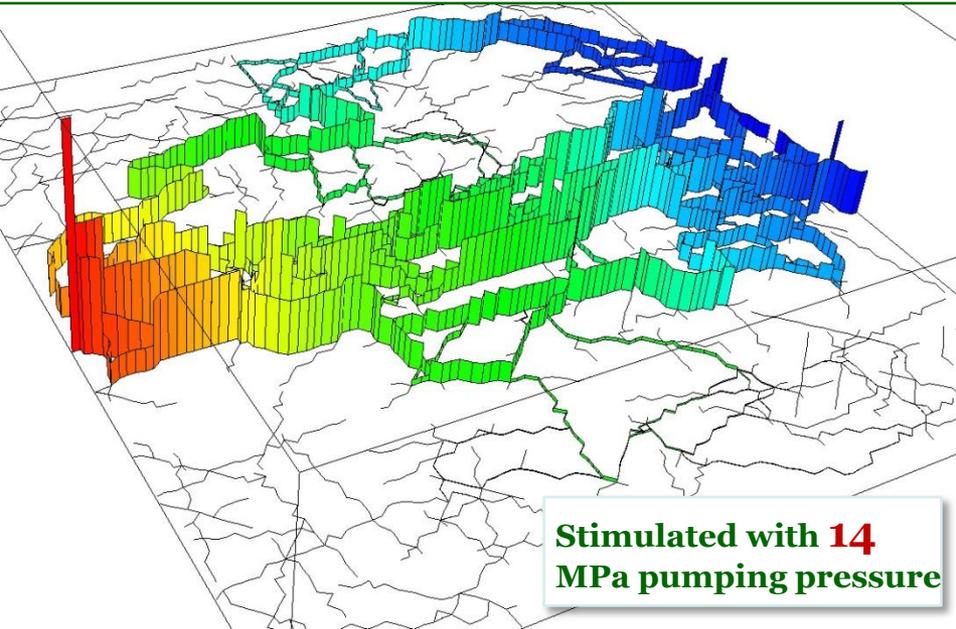
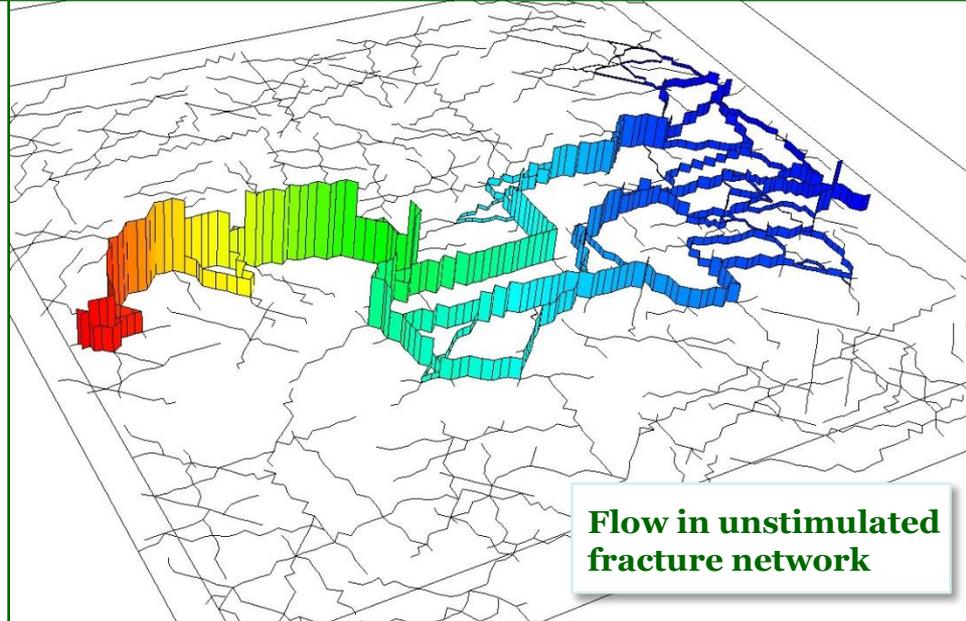
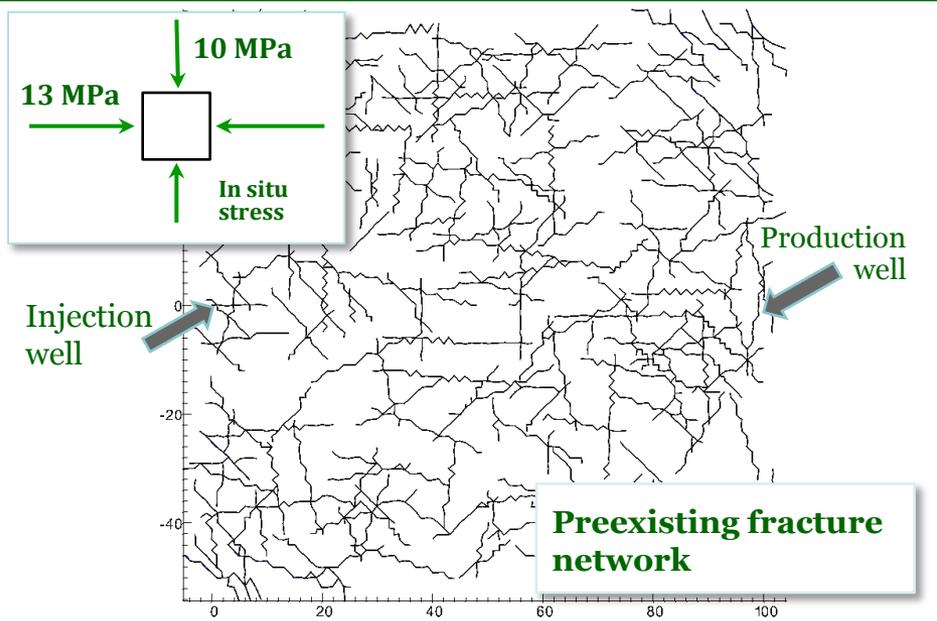


**Connected
to Well B**

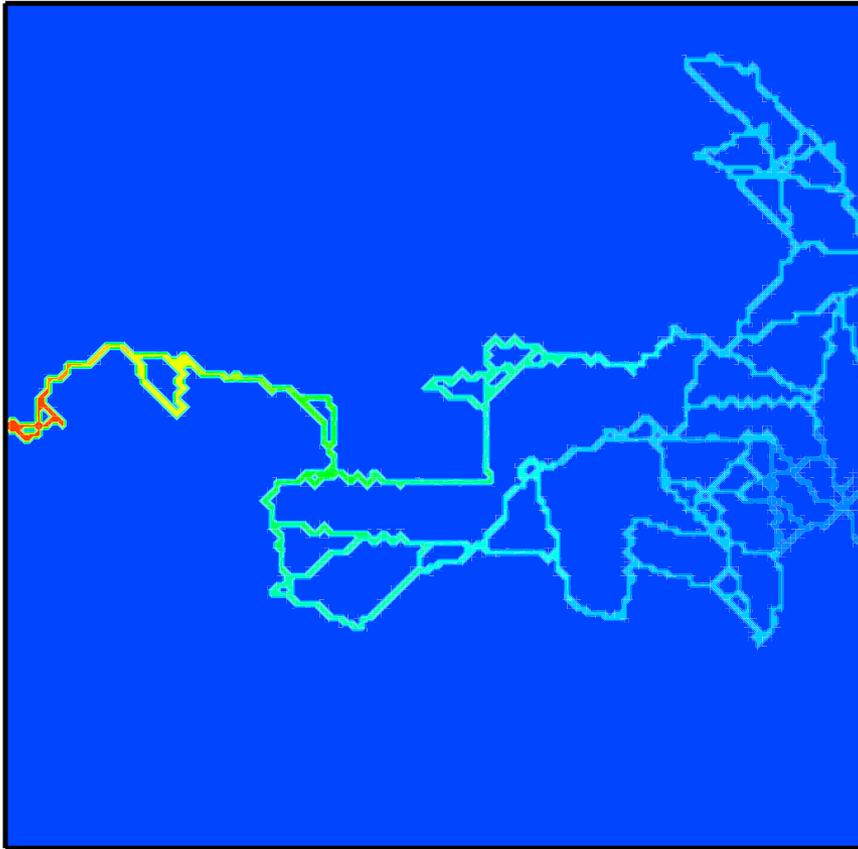




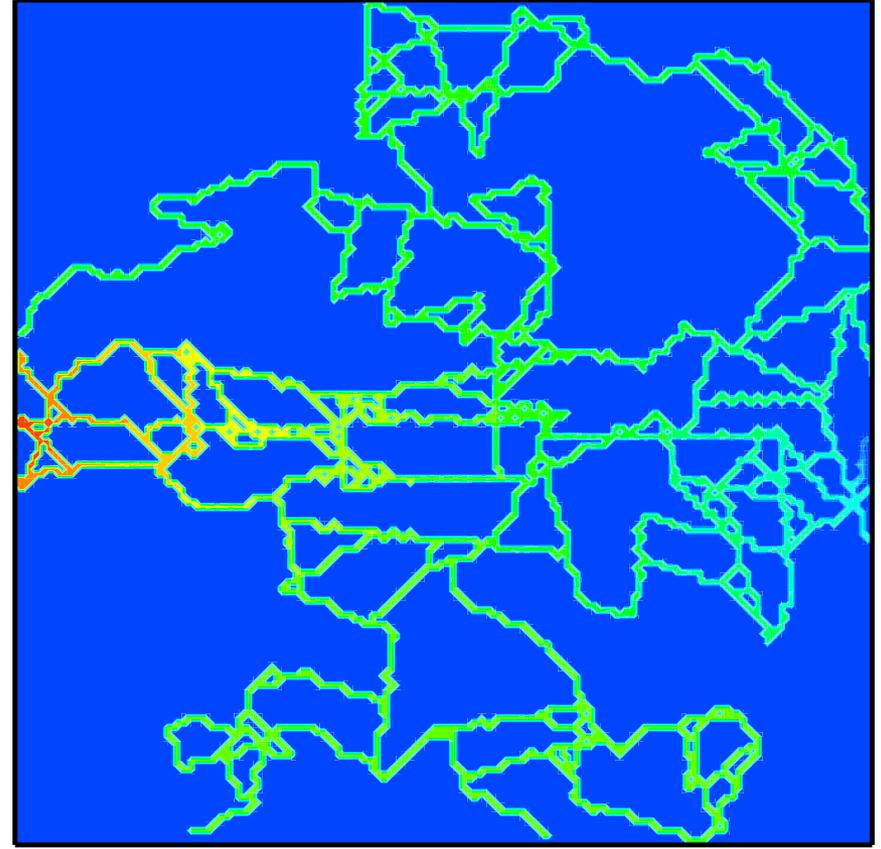
III: Effects of stimulation pressure



Thermal analysis based on the predicted fracture network.



Before stimulation



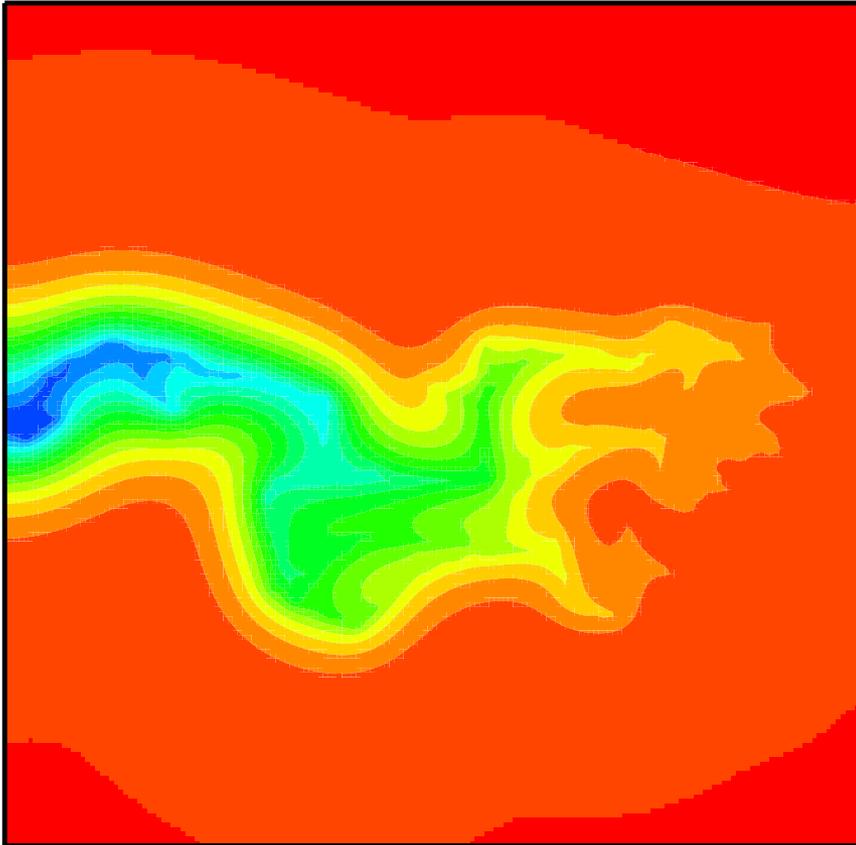
After stimulation

(Preliminary NUFT analysis results provided by Yue Hao at LLNL.)



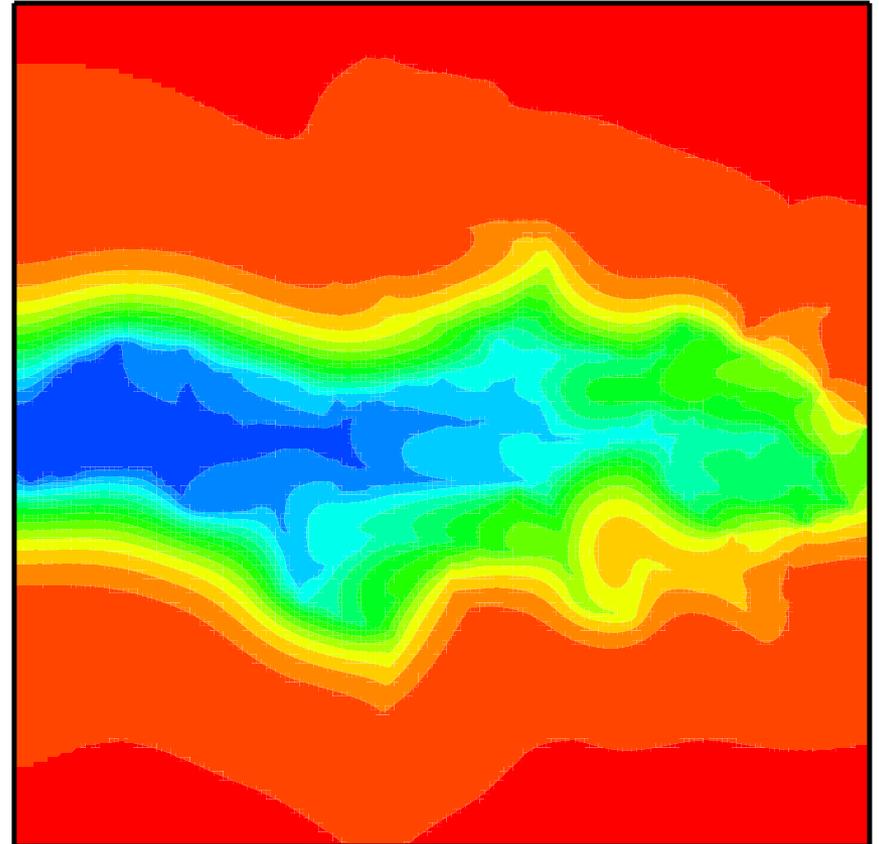
Thermal analysis based on the predicted fracture network.

5 years



Without stimulation

5 years



With stimulation

(Preliminary NUFT analysis results provided by Yue Hao at LLNL.)



Concluding Remarks

- Challenges:
 - The coupling of multiple modules.
 - High computational cost.
- Benefits:
 - Explicit simulation of fracture-fracture and fracture-fluid interaction.
 - Capable of handling complex fracture networks.
 - Simple and physically meaningful input parameters.
- Further development, enhancement, and validation
 - Methodology works; preliminary results are reasonable and inspiring.
 - **Collecting stimulation scenarios to investigate (poster on Tuesday).**



Acknowledgments

- This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344.



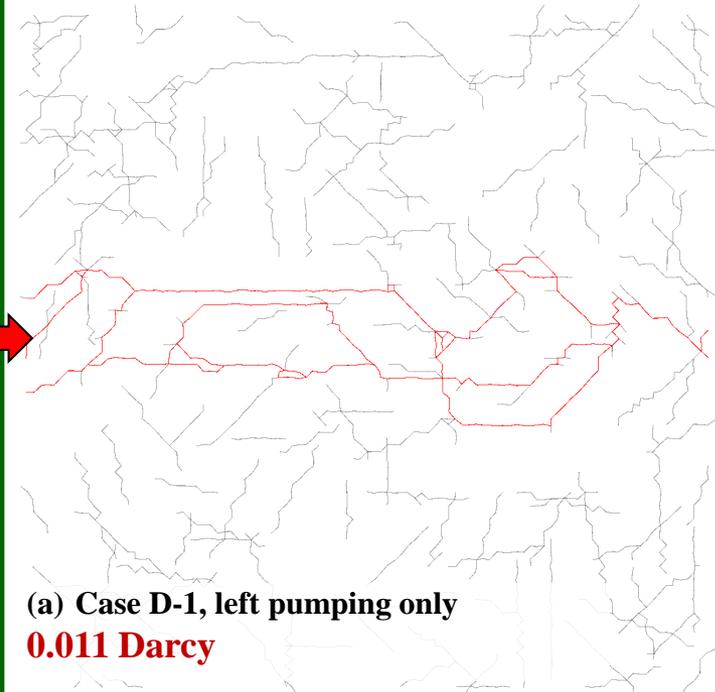
U.S. DEPARTMENT OF
ENERGY

GTP

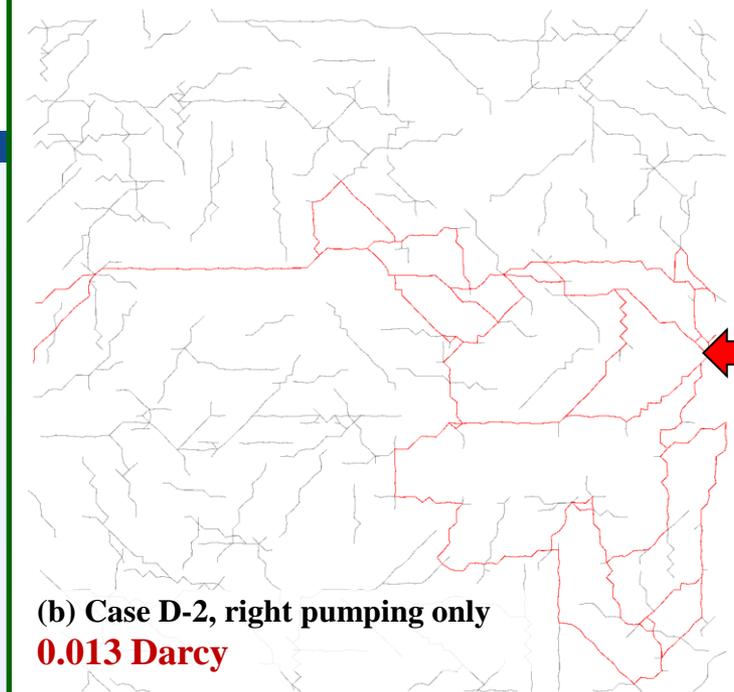
 **Lawrence Livermore
National Laboratory**

Release number: LLNL-PRES-489801

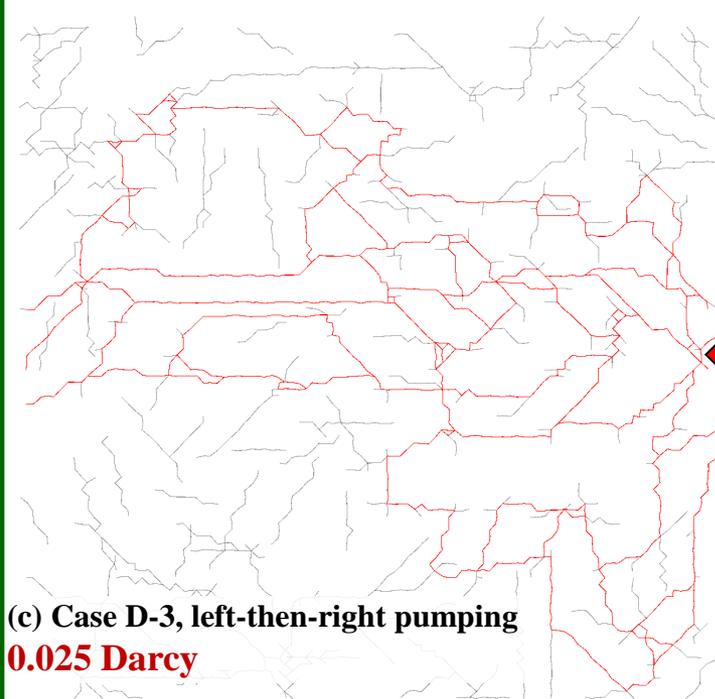




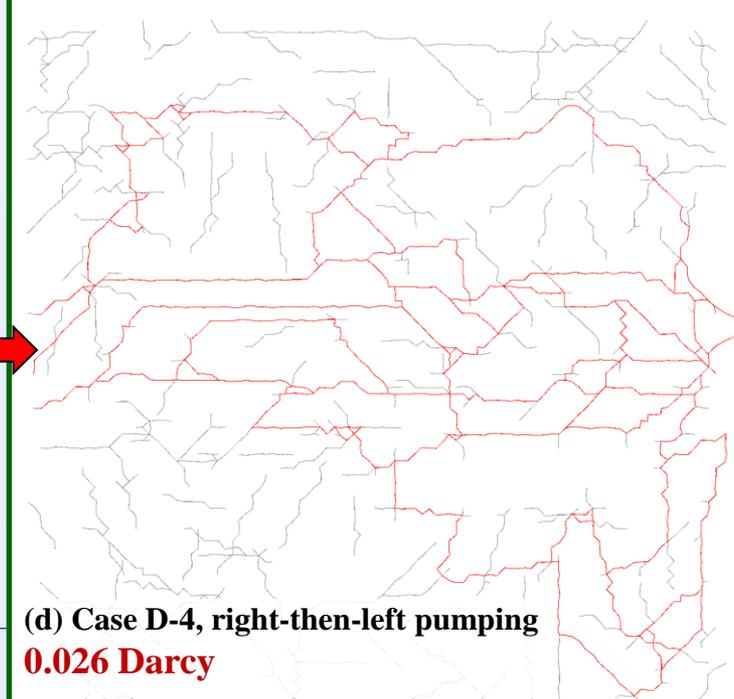
(a) Case D-1, left pumping only
0.011 Darcy



(b) Case D-2, right pumping only
0.013 Darcy

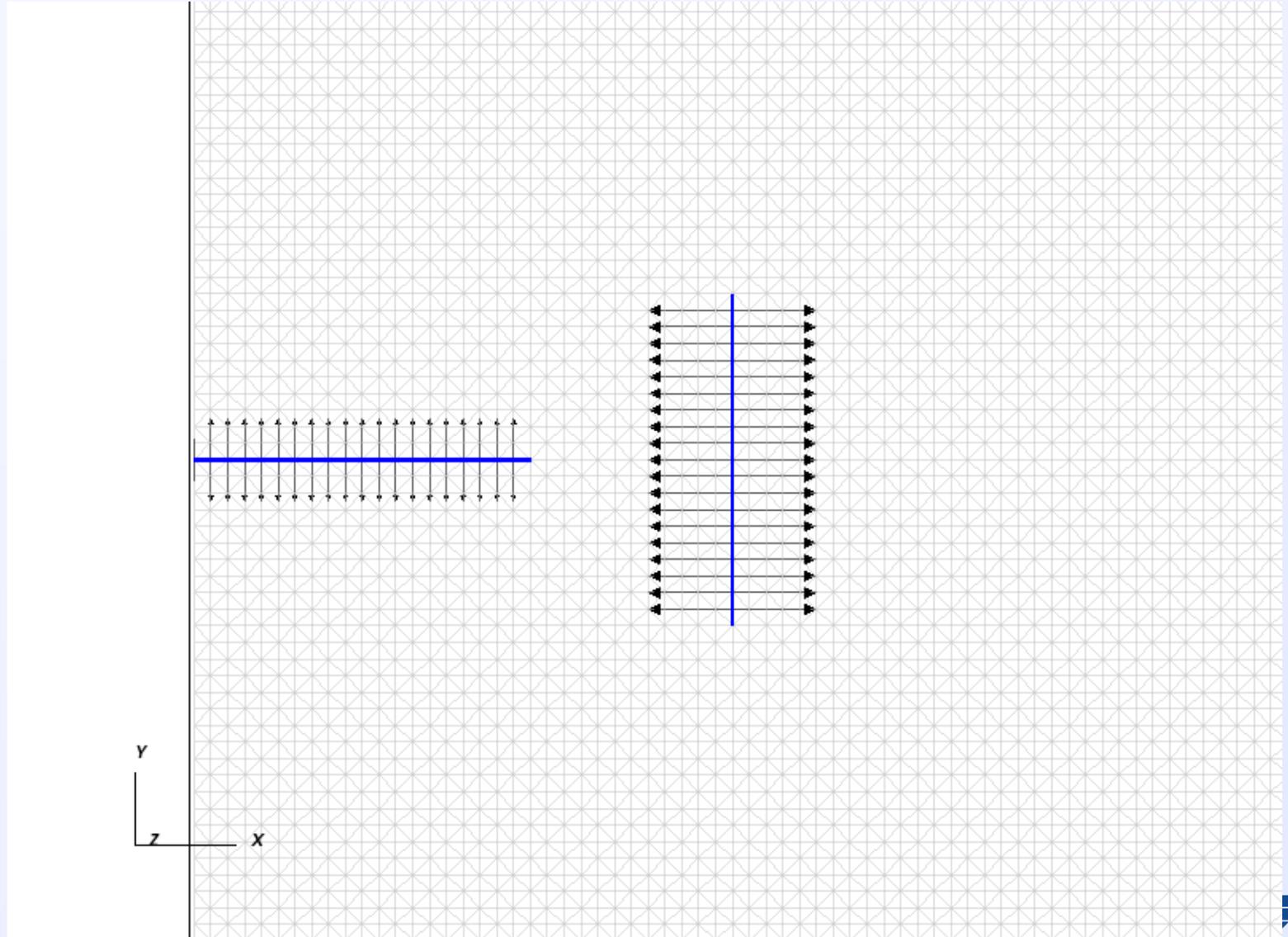


(c) Case D-3, left-then-right pumping
0.025 Darcy

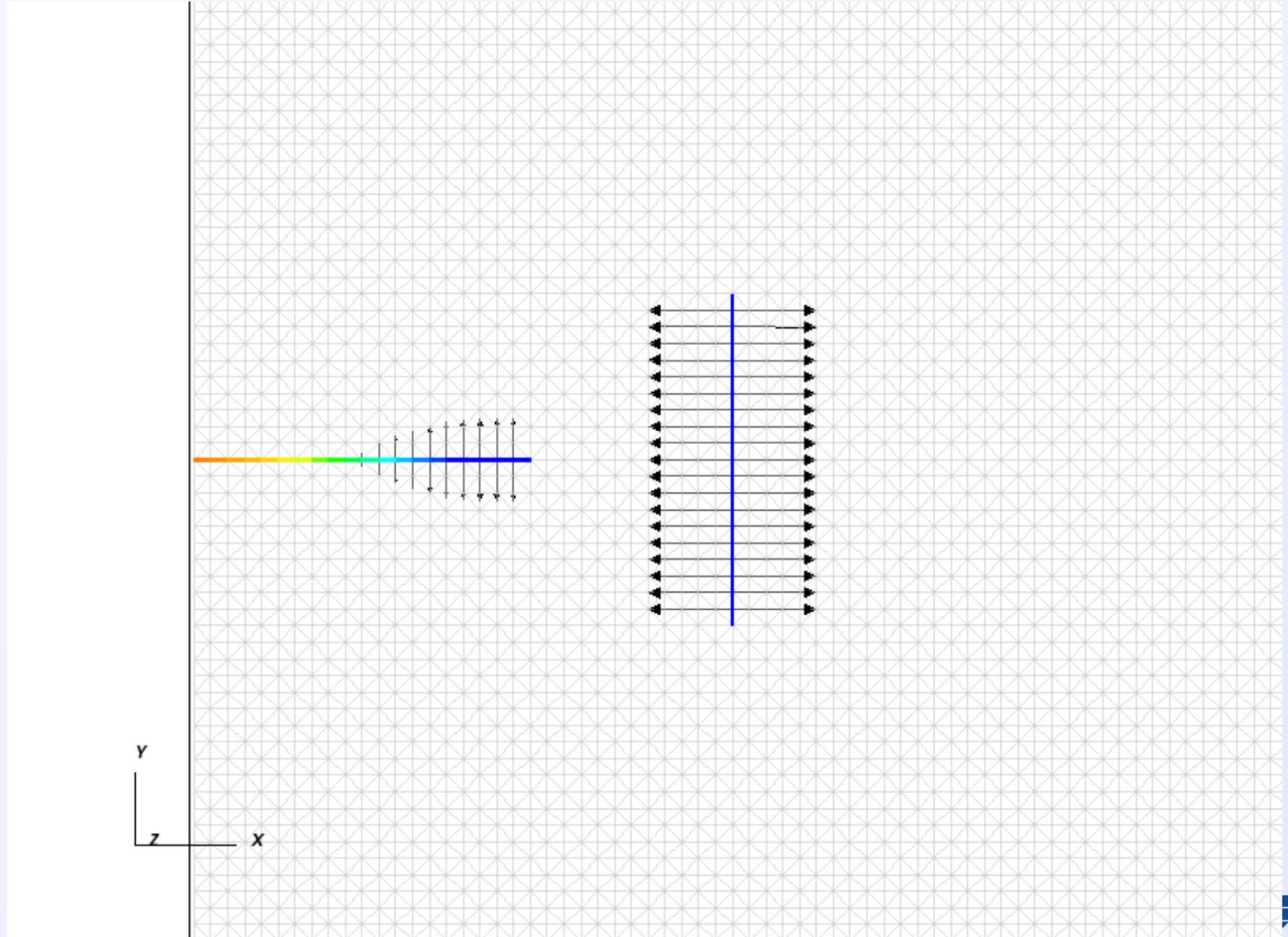


(d) Case D-4, right-then-left pumping
0.026 Darcy

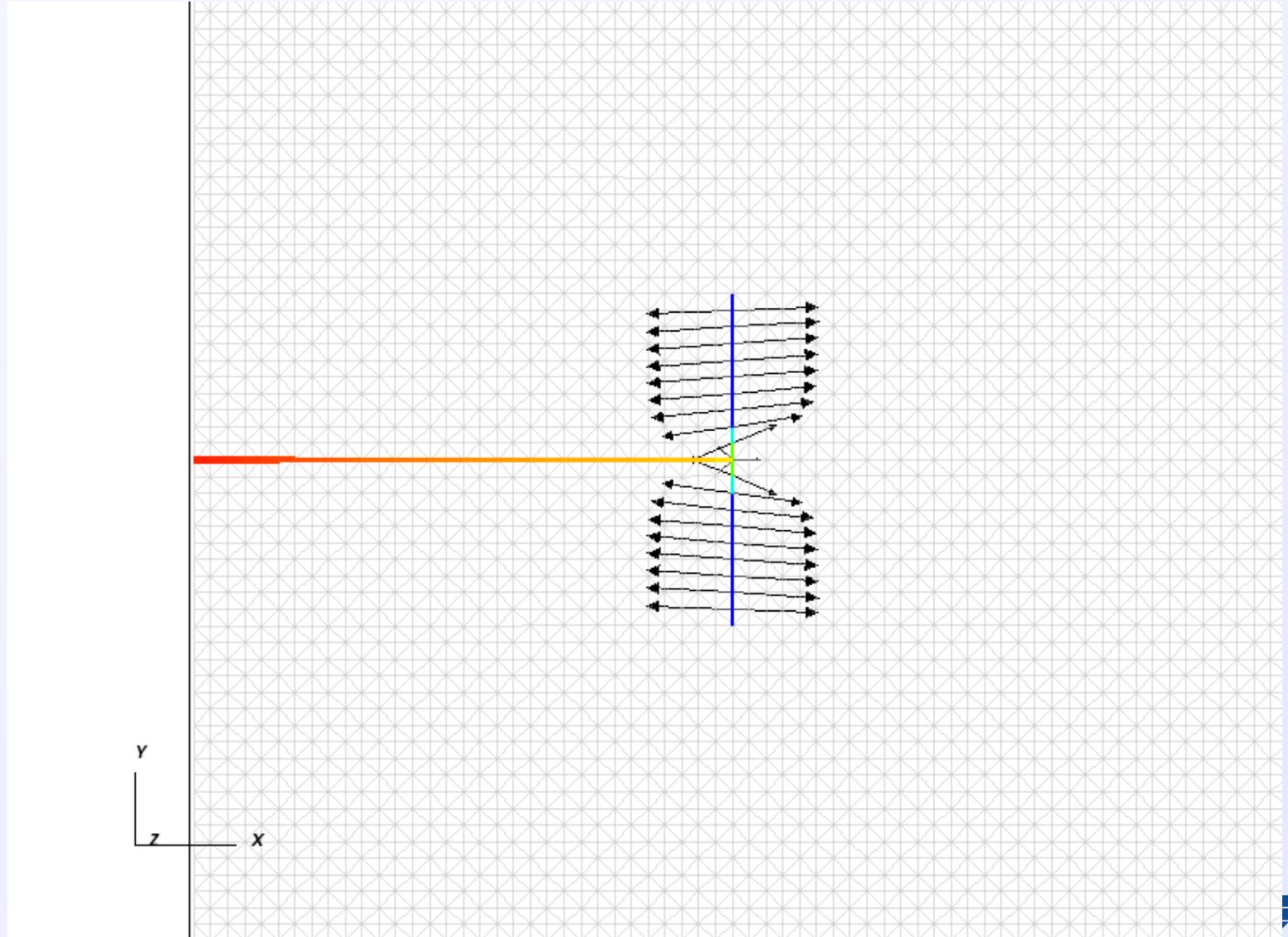
Interaction Between Propagating and Existing Fractures



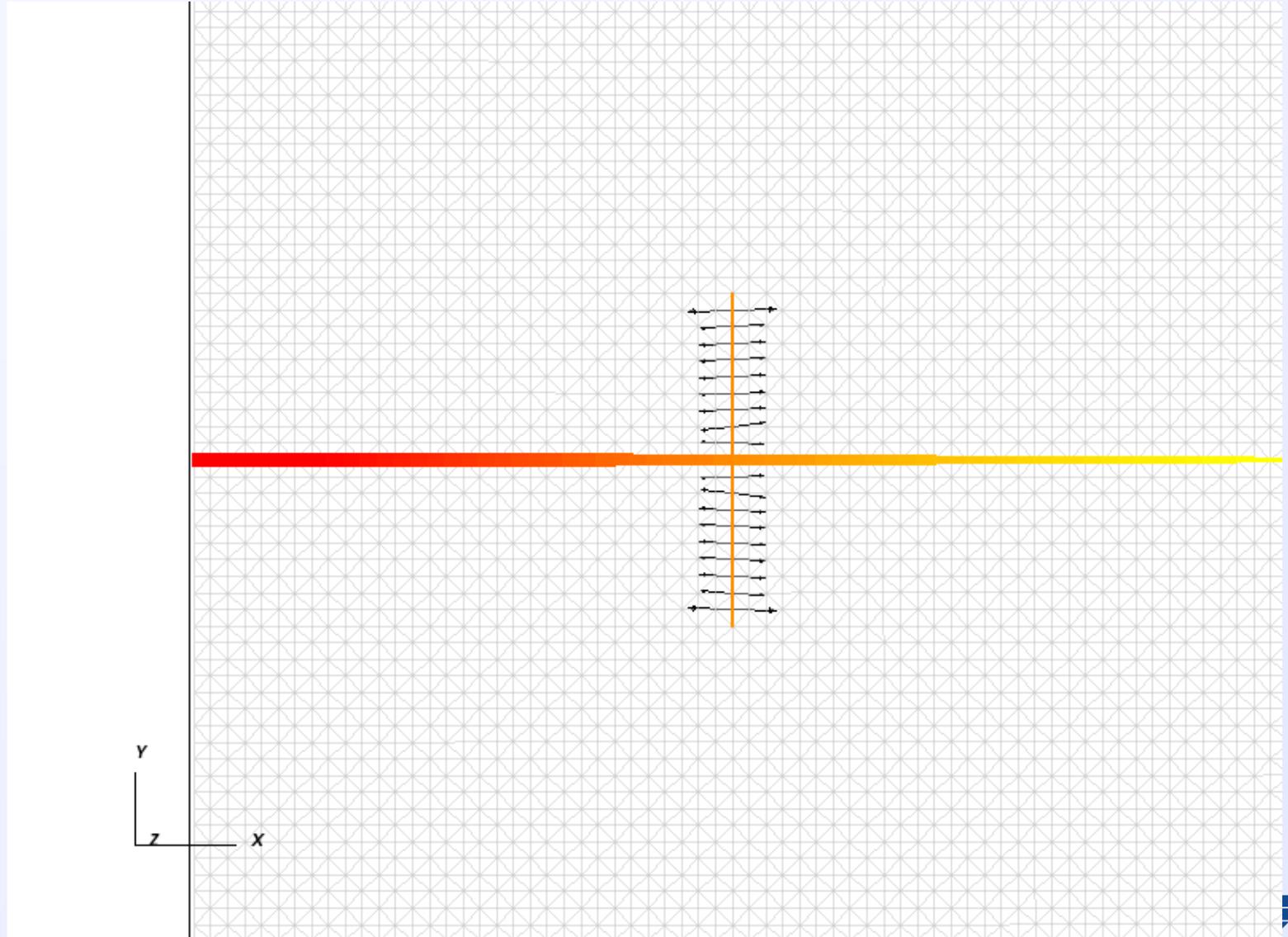
Interaction Between Propagating and Existing Fractures



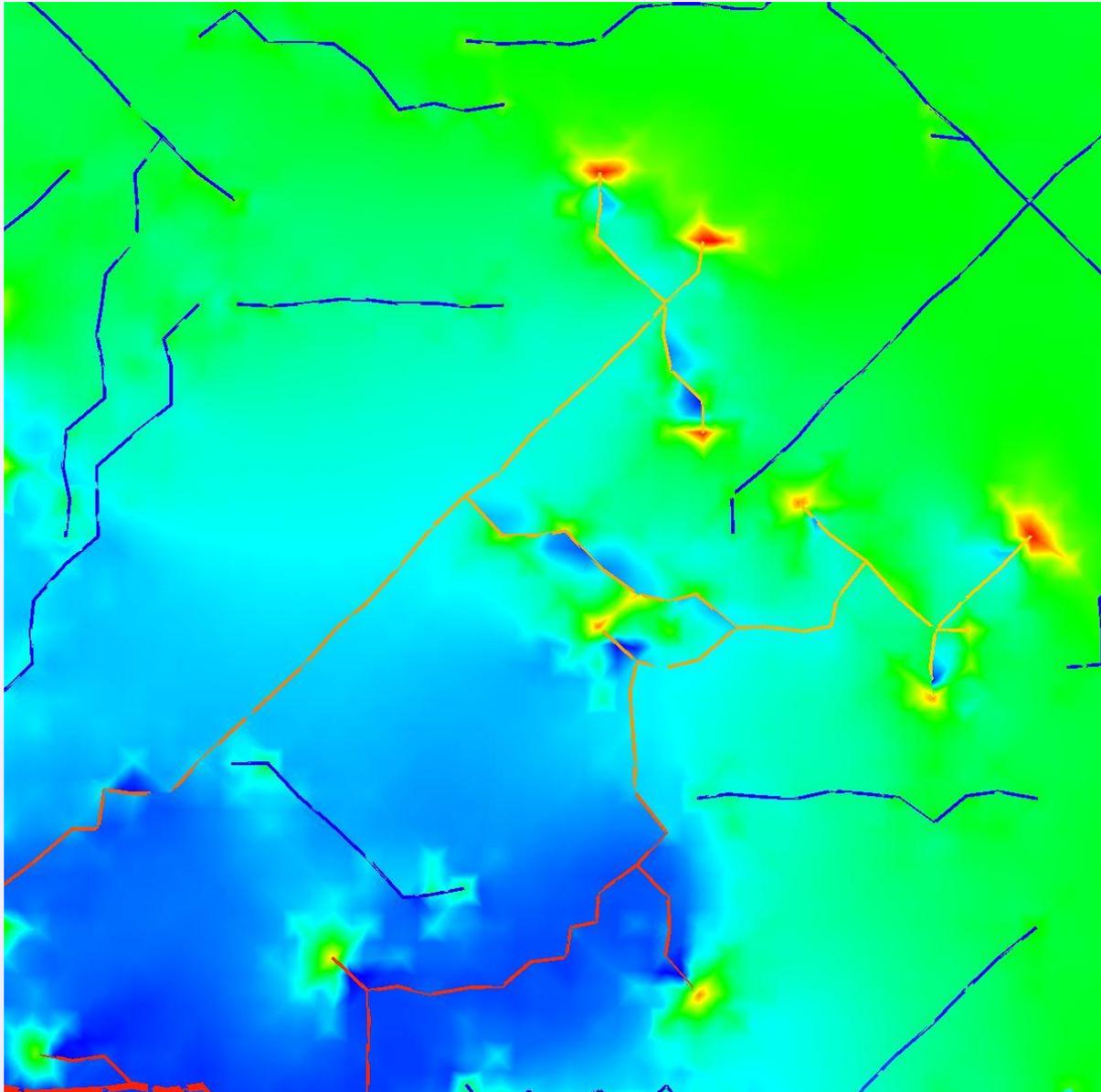
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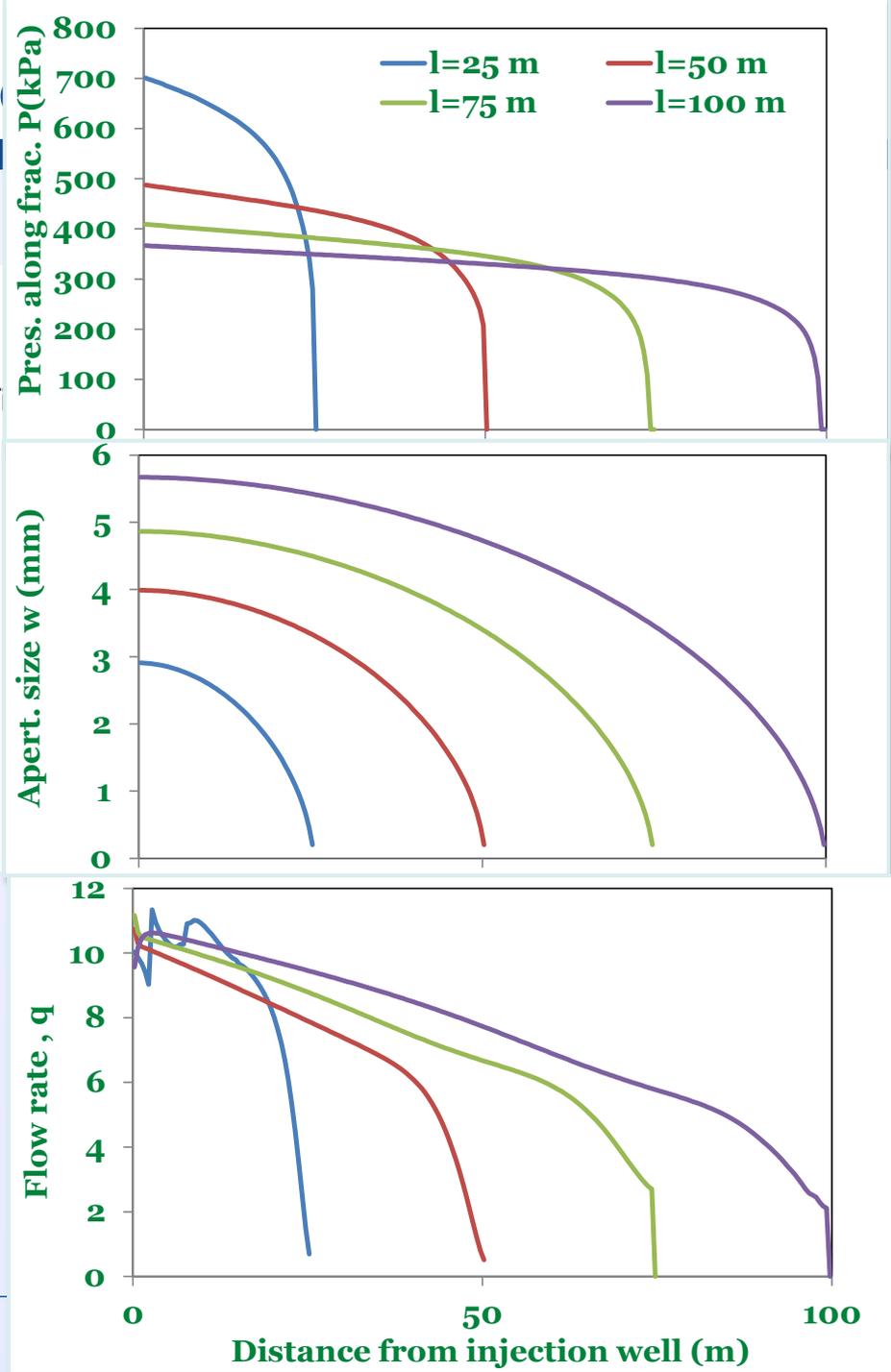
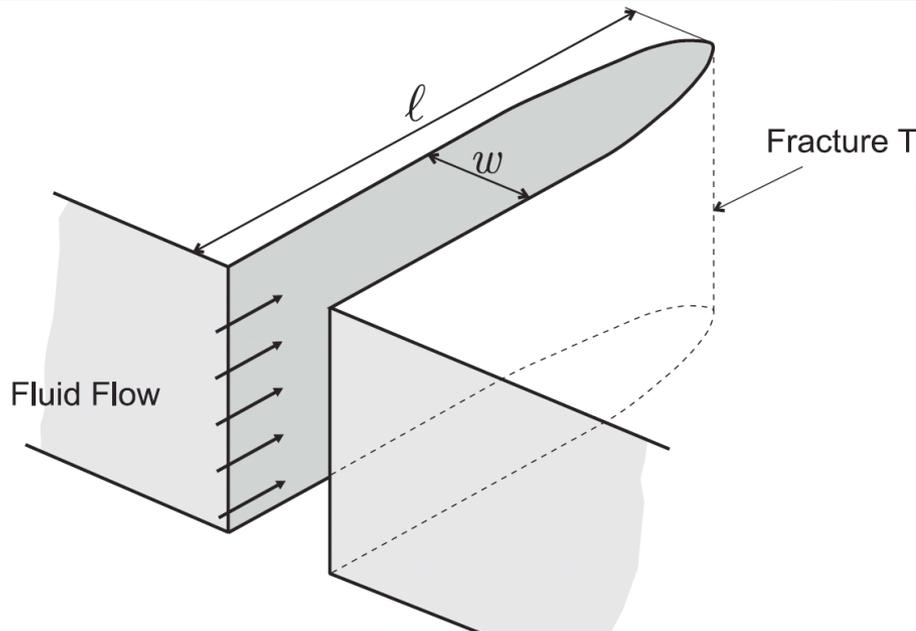
Interaction Between Propagating and Existing Fractures



Application to more complex fracture networks



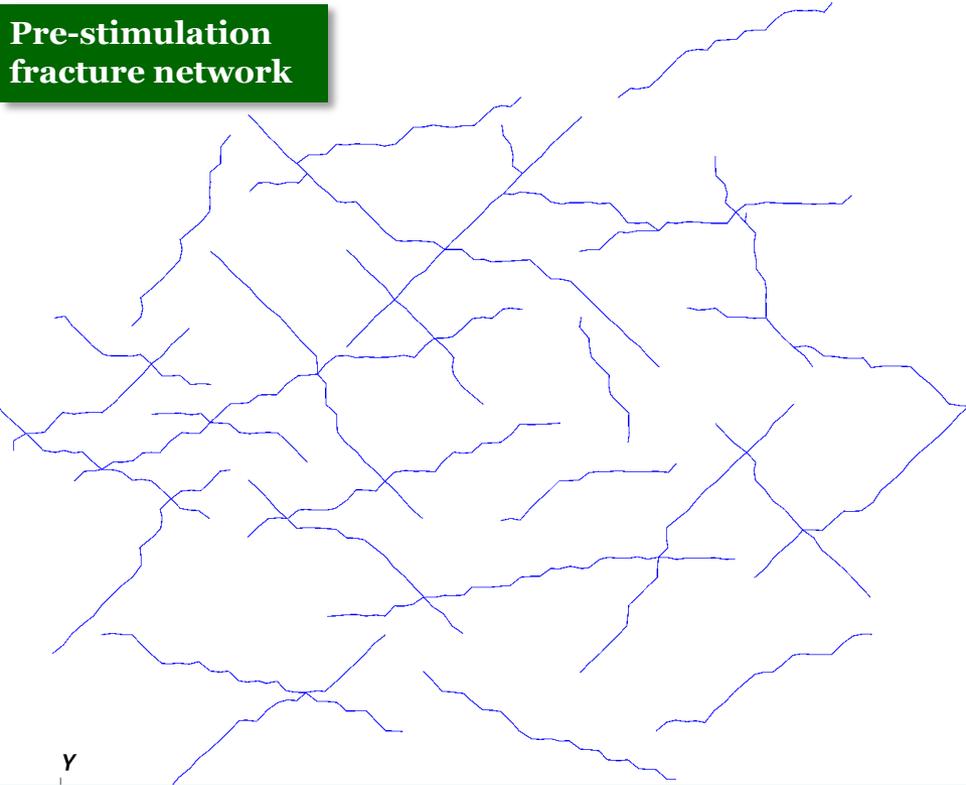
Model verification: classical KGD model



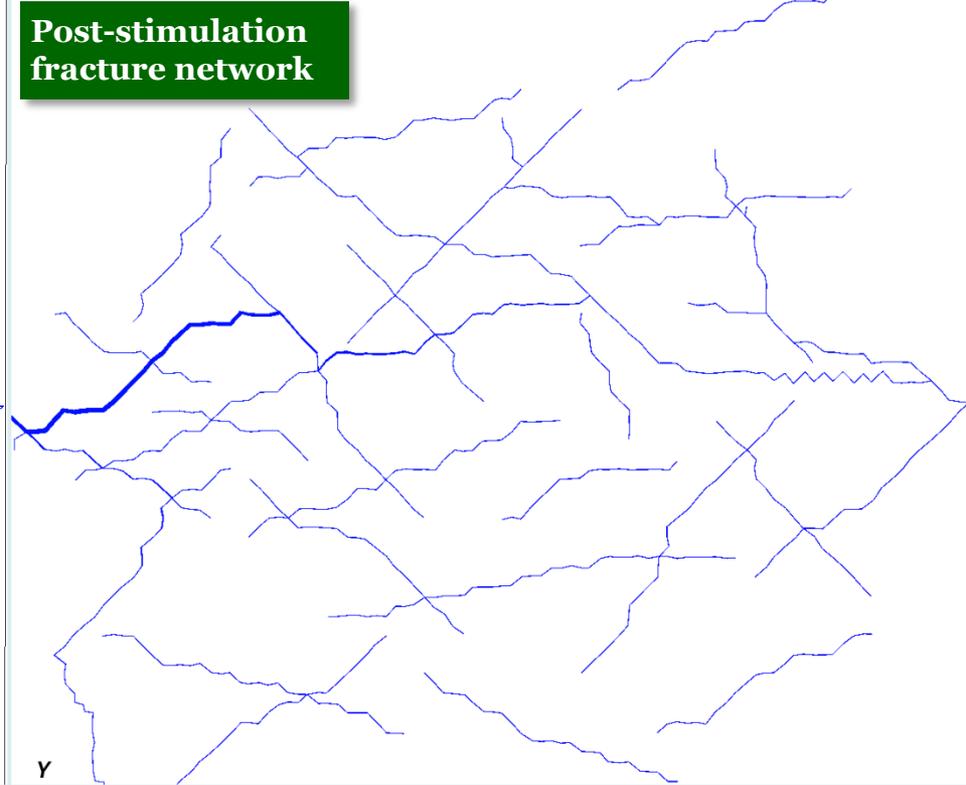
$$l(t) = 0.679 \left[\frac{Gq_0^3}{\mu(1-\nu)} \right]^{\frac{1}{6}} t^{\frac{2}{3}}$$

Application to more complex fracture networks

Pre-stimulation fracture network



Post-stimulation fracture network



Application to more complex fracture networks

