

# Foulger Consulting

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WEEKLY REPORT #8 TO ALTAROCK ENERGY INC.

PROCESSING OF INDUCED EARTHQUAKES ASSOCIATED WITH THE NEWBERRY EGS INJECTION STARTING SEPTEMBER 2014

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# Brief summary

During the last week we concentrated on studying the November swarm with a view to examining whether it had different characteristics from the September/October earthquake activity. This seems indeed to be the case:

- The swarm comprises two bursts, the first peaking in intensity about 16 November and the second peaking in intensity about 21 November.
- The earthquakes of the second burst are  $\sim 300$  m deeper than those of the first burst.
- Both the absolute locations of the 6 moment-tensor events studied from the November swarm and the relative locations of the November-only earthquakes suggest that a more northerly striking planar feature was activated (~ N15°W, compared with N60°W for the September/October planar feature).
- The depth range of the earthquakes spanned the zone that was aseismic during September/October, closing the "aseismic gap".
- Moment tensor calculations suggest that the P- and T-axes are orientated systematically differently, namely the T-axes plunge more steeply and trend more westerly, and the P-axes trend more northerly. This consistent with a different stress field and a rotated plane of failure.

During the forthcoming week we will work to increase the size of our relative-location and momenttensor data set for the November earthquakes in order to test these preliminary results.



### 1 Task 1 – Planning, conference calls, discussion of work, correspondence, followup

We continued to maintain contact with team members as before. The work continued to run smoothly.

#### 2 Task 2 – System Setup

No additional system setup was done during the last week.

#### 3 Task 3 – Quality control of prepicked MEQs for relocation and moment tensor calculation

We continued to derive moment tensors using the procedure described in our Weekly Report #1. We report here an additional 5 moment tensors from 16, 17 and 21 November. This brings the total number derived up to 70 (Appendix 1). We have provided the locations of these new moment tensors to Trenton Cladouhos of AltaRock electronically, by email attachment.

#### 4 Task 4 – Improved locations and relative locations

#### 4.1 Absolute locations–ISTI picks

We locate all the earthquakes hand-picked by ISTI as a routine matter, using our in-house location program *qloc*. In our report #7 of 19 November, we presented week-by-week maps of the earthquake locations which showed the development with time of the activity. Here we update the incomplete week shown in that report and add an additional week. Figure 1 shows maps of the earthquakes for November 14-20 and November 21-24 (incomplete week).



Figure 1: Earthquakes located using ISTI picks, and our in-house *qloc* location program for the weeks (left) November 14-20 and (right) November 21-24 (incomplete week).

Figure 2 shows the depths of all the earthquakes as a function of time (*qloc* locations, using ISTI picks). The November swarm comprises two bursts, the first peaking in intensity about 16 November and the second peaking in intensity about 21 November. The earthquakes of the second burst are significantly ( $\sim 300$  m) deeper than those of the first burst.



Figure 2: Estimated depths, with respect to sea level, of the earthquakes within the NMSA network as a function of time. These depths were obtained by using *qloc* to invert *P*- and *S*-phase arrival times measured by personnel of the ISTI Corporation on digital seismograms from the NMSA network.



### 4.2 Absolute locations–Foulger Consulting picks for moment-tensor derivation

We picked an additional 5 earthquakes for the purpose of moment-tensor derivation, bringing the total in hand to 70. Figure 3 shows a map of the 6 earthquakes that occurred in November, for which moment tensors have been derived. These locations are exceptionally accurate, being a by-product of the moment tensor deriviation process. The epicenters lie in a linear zone that trends more northerly than the entire earthquake set (see previous reports). This result agrees well with the results of relative locations of the November swarm as a whole (Section 4.4).

A map of all 70 moment-tensor-earthquake locations is shown in Figure 4.



Figure 3: High-quality estimated hypocenters of 6 microearthquakes that occurred in November. Moment tensors were derived for these events. The locations are computed using arrival times measured using advanced (and more time-consuming) methods in connection with the moment-tensor analysis. Well NWD 55-29 is shown in blue.





Figure 4: High quality estimated hypocenters of the entire 70-earthquake set for which moment tensors have been derived. Well NWD 55-29 is shown in blue.

## 4.3 Relative locations: the entire catalog

We continued with the relative location work, applying the method to the catalog of ISTI-picked events up to and including 21 November. This set contained 376 earthquakes. We relative located this catalog using the following input parameters:

- o minclust = 10;
- $\circ$  maxit = 25;
- $\circ$  maxsep = 0.20 km;
- $\circ$  *minlinks* = 18.

A higher threshold of minlilnks = 18 could be used because of the larger size of the catalog. 25 earthquakes passed the thresholds and were located.

The results are shown in Figure 5 and Figure 6.



Figure 5: Map of relative locations of 25 earthquakes that occurred in the time period 26 September - 21 November, 2014. Runtime parameters used were *minclust* = 10, maxit = 25, maxsep = 0.20 km, minlinks = 18.



Figure 6: Same as Figure 5 except looking along the strike of the epicentral trend, to the NW.

The northwesterly trending epicentral zone continues to be apparent.

# 4.4 Relative locations: The November swarm

Relative locations were calculated for the November swarm only, using earthquakes that occurred in the period 15 - 21 November. This subset of the data comprised 78 earthquakes. The following input parameters were used. These yielded the best balance between selecting out the highest-quality locations, whilst not reducing the number of earthquakes to a very small number:

- $\circ$  *minclust* = 10;
- $\circ$  maxit = 25;
- $\circ$  maxsep = 0.20 km;
- $\circ$  *minlinks* = 14.



Interestingly, these earthquakes delineate a sub-vertical, planar feature, but in contrast to the September/October earthquakes, the strike of the November feature is more northerly. It strikes just slightly west of north (Figure 7). This seems to be consistent with an apparent change in the orientation of the P-, and T-axes detected in new moment tensors derived (see Section 5).

The depth range of the November earthquakes includes the layer that was aseismic in September/October, separating those earthquakes into two clusters. This is consistent with the depth distribution of the entire catalog no longer showing a division into two clusters (Figure 6).



Figure 7: Map of relative locations of 17 earthquakes that occurred in the time period 15 - 21 November, 2014. Runtime parameters used were *minclust* = 10, *maxit* = 25, *maxsep* = 0.20 km, *minlinks* = 14.



Figure 8: Same as Figure 7 except looking along the strike of the epicentral trend, to the NNW.

# 5 Task 5 Moment tensors

We continued to derive moment tensors and report here an additional 5. We focused on the earthquake sequence that occurred in mid-November, and report mechanisms for events from 16, 17 and 21 November.

The entire list of earthquakes processed to date is given in Appendix 1. The numerical results of the entire moment-tensor catalog, including the 5 new results are given in Appendix 2. Graphical results for the additional 5 events are given in Appendix 3. We have provided the decomposition data of these new moment tensors to Trenton Cladouhos of AltaRock electronically, by email attachment.

The source types for the 6 moment tensors we have now derived for the November sequence are shown in Figure 9. The distribution lies along the +Dipole to -Dipole range, but does not occupy the full range. Mechanisms range from strongly implosive (-Dipole) to mildly explosive. This suggests that



these earthquakes were dominantly volume-decreasing. The dataset is small, and it will be interesting to see if this is confirmed when more mechansims from this sequence are derived.



Figure 9: Source-type plot showing the 6 earthquakes from November for which moment tensors have been derived to date.

Figure 10 shows plots of the P-, T- and I-axes, approximately corresponding to the directions of  $\sigma_1$ ,  $\sigma_3$  and  $\sigma_2$ . The plot on the left is of the 65 events from September and October, reported in our Weekly Report #7 of 19 November. The plot on the right is of the 6 events from the November swarm.

The number of events is small, but there appears to be a significant difference in the orientation of the P-, T- and I-axes compared with the events of September and October. The T-axes dip more steeply and are somewhat more westerly oriented. The P-axes are distributed around the north direction, and do not preferentially trend NE as was the tendency in the earlier earthquakes.



Figure 10: Plots of pressure ( $P \sim \sigma_1$ ) and tension ( $T \sim \sigma_3$ ) and intermediate ( $I \sim \sigma_2$ ) axes. Left: the 65 earthquakes that occurred in September and October; Right: the 6 earthquakes that occurred 16, 17 and 21 November.

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During the forthcoming week we will work to increase the size of our relative-location and momenttensor data set for the November earthquakes in order to test these preliminary results.



Appendix	1: 7	The	70	earthquakes	for	which	moment	tensors	have	been	obtained	to	date.	Locations
given belo	w ai	re fro	om	the webpage	http	://fract	ure.lbl.go	v/Newb	erry/lo	ocatio	ns.txt.			



0.7.0	1.0	-		_		40 505	101 01000	0 (= 0	1
278	10	5	4	7	30.446	43.725	-121.31322	0.659	1.696
278	10	5	15	55	21.373	43.73483	-121.30918	0.702	0.695
278	10	5	16	7	32.904	43.7253	-121.30967	1.205	0.819
278	10	5	23	22	16.638	43.72368	-121.3116	1.055	0.931
279	10	6	4	2	55.851	43.72307	-121.30835	0.835	0.637
279	10	6	6	13	48.787	43.72425	-121.3097	0.638	0.604
280	10	7	6	12	8.757	43.72372	-121.31015	0.564	0.791
280	10	7	7	26	23.29	43.71807	-121.31032	0.962	0.574
280	10	7	10	47	21.079	43.72403	-121.3095	1.136	0.822
281	10	8	7	5	6.107	43.72662	-121.3048	0.864	0.541
281	10	8	19	8	20.701	43.71945	-121.31087	1.267	0.523
281	10	8	21	16	58.206	43.73442	-121.31173	1.703	0.522
282	10	9	6	24	33.517	43.72232	-121.31203	0.735	0.769
282	10	9	10	16	9.958	43.7172	-121.31332	1.378	0.722
284	10	11	3	29	5.813	43.72417	-121.31338	0.409	0.852
284	10	11	10	53	26.568	43.72493	-121.30897	1.292	0.824
285	10	12	10	12	29.727	43.7257	-121.3135	0.783	0.863
285	10	12	16	37	43.42	43.72515	-121.3151	0.49	1.482
285	10	12	16	47	1.174	43.7297	-121.3126	1.07	0.681
285	10	12	18	33	4.878	43.72363	-121.30787	0.359	0.743
285	10	12	21	10	18.995	43.72783	-121.31002	0.653	0.792
286	10	13	0	57	6.873	43.72382	-121.3175	0.242	1.197
286	10	13	4	12	29.232	43.72657	-121.30698	0.882	1.179
286	10	13	10	22	29.146	43.7302	-121.3153	0.831	0.907
287	10	14	5	46	14.161	43.71765	-121.31087	0.161	0.904
288	10	15	15	3	44.691	43.72658	-121.30768	0.897	0.781
288	10	15	15	37	26.034	43.72713	-121.30915	0.934	0.883
289	10	16	16	53	27.596	43.72378	-121.31295	-0.186	0.736
291	10	18	23	57	3.867	43.72965	-121.31732	0.116	0.781
292	10	19	9	7	50.375	43.73525	-121.3113	0.837	0.776
296	10	23	21	2	22.32	43.7257	-121.30855	0.819	0.6
320	11	16	16	44	39.436	43.72772	-121.31492	1	1.099
320	11	16	18	52	9.671	43.72657	-121.31147	0.868	0.864
321	11	17	3	34	37.593	43.7274	-121.31807	0.203	1.088
321	11	17	4	41	53.061	43.7249	-121.31087	0.708	2.229
321	11	17	23	31	42.368	43.72523	-121.3094	-0.399	1.12
325	11	21	9	57	35.294	43.72682	-121.31657	0.475	1.219
-	-	-	-					· ·	

Appendix 2:	Numerical mor	ment tensor	results	for the	70 MEQs	studied	to date.	N=North,	E=East,
D=Down.									

NN	NE	EE	ND	ED	DD	Yea r	M o	Da V	H r	mi n	Sec	Quality
								•				
1.578e-01	3.466e-02	6.671e-02	2.482e-01	6.317e-02	8.338e-02	201	1	01	1	53	05.23	excellen +
2.172e-01	-3.673e-	-6.417e-	2.346e-01	7.204e-02	3.184e-02	201	1	01	1	05	16.54	excellen
8.713e-02	02 1.262e-01	-4.193e-	1.814e-01	8.429e-02	8.722e-02	4 201	0	04	9 1	51	12.00	excellen
-1.029e-	1.325e-01	-1.185e-	1.480e-01	5.508e-02	1.074e-01	4 201	0	04	8 1	32	52.76	excellen
-1.165e-	1.705e-01	-1.989e-	1.394e-01	-2.430e-	1.639e-02	4 201	0	02	0	07	04.16	excellen
01 2.406e-01	-7.298e-	-9.789e-	1.731e-01	02 4.297e-02	8.349e-02	4 201	0	02	1	01	42.38	excellen
-1.461e-	02 9.643e-02	-3.978e-	2.595e-02	1.691e-01	-4.693e-	4 201	1	02	0	47	52.94	excellen
02 6.066e-03	-2.231e-	01 -9.157e-	1.941e-01	3.367e-02	-6.184e-	4 201	0	03	6 0	06	22.76	excellen
-5.772e-	-1.655e-	-1.427e-	1.464e-01	7.811e-02	-1.952e-	4 201	0	03	6 1	54	53.93	t fair
02 2.004e-01	01 -1.410e-	01 -1.461e-	1.400e-01	-8.713e-	02 7.412e-02	4 201	0	01	8	03	16.94	good
5.304e-02	01 6.783e-02	-1.175e-	1.615e-01	03 7.508e-02	2.206e-01	4 201	0	05	2	07	20	excellen
-1.777e-	-1.053e-	-1.512e-	7.111e-02	1.063e-01	1.057e-01	4 201	0	01	4	03	14.49	excellen
01 -2.667e-	01 1.320e-01	01 -6.399e-	6.063e-02	1.031e-01	7.787e-02	4 201	0	30	1 2	30	43.50	t excellen
01 -1.871e-	8.995e-02	02 -9.473e-	-1.446e-	-2.491e-	1.992e-01	4 201	9	05	1 2	22	3 16.49	t good
01 1.684e-01	-3.350e-	02 -9.826e-	01 2.952e-01	02 3.542e-02	9.350e-02	4 201	0 1	04	3 0	29	9 08.25	fair
2.449e-01	02 -8.111e-	03 -1.972e-	1.741e-01	1.624e-02	1.507e-02	4 201	0 1	03	5 1	27	8 57.66	good
-2.209e-	02 -8.132e-	01 -2.190e-	-1.520e-	3.521e-02	2.201e-01	4 201	0 1	01	5 1	56	1 11.34	good
01 1.477e-01	02 -1.175e-	02 -1.492e-	01 1.577e-01	-3.130e-	9.546e-02	4 201	0 1	01	6 0	08	3 57.99	excellen
-3.263e-	01 2.220e-01	01 -3.373e-	1.644e-02	02 7.162e-02	9.879e-03	4 201	0 1	01	8 1	50	8 55.10	t excellen
02 -1.038e-	1.463e-01	01 -2.541e-	1.246e-01	-1.332e-	7.335e-02	4 201	0 1	01	0	01	7 54.95	t excellen
01 2.306e-03	-1.802e-	01 -9.214e-	2.203e-01	02 -4.354e-	9.593e-02	4 201	0 1	02	5 1	54	0 03.15	t good
1.619e-01	01 4.200e-02	02 -2.041e-	2.158e-01	03 -2.044e-	7.759e-02	4 201	0 1	02	8 0	39	2 02.99	excellen
-6.570e-	-1.851e-	01 -1.140e-	1.691e-01	02 4.183e-02	2.826e-02	4 201	0 1	02	6 1	39	8 24.31	t good
02 1.420e-01	01 -1.373e-	01 -1.638e-	1.721e-01	1.076e-02	5.384e-02	4 201	0 1	02	2 2	37	7 06.04	good
-1.365e-	01 -1.837e-	01 -5.911e-	1.611e-01	-1.124e-	9.224e-02	4 201	0 1	05	0 0	06	3 16.96	excellen
01 2.866e-01	01 -3.707e-	02 -1.787e-	9.263e-02	02 1.263e-01	2.268e-02	4 201	0 1	05	2 1	07	7 32.77	t excellen
-2.286e-	02 1.607e-01	01 -7.209e-	-9.281e-	8.007e-02	-3.216e-	4 201	0 1	05	6 1	55	7 21.00	t good
01 -1.352e-	-1.174e-	02 -4.098e-	02 1.996e-01	-5.345e-	02 8.302e-02	4 201	0 1	12	5 1	12	7 29	good
01 -2.211e-	01 1.542e-01	02 4.959e-02	9.042e-02	02 8.191e-02	7.603e-02	4 201	0 1	12	0 2	10	23.31	good
01 -4.882e-	-1.017e-	5.620e-02	5.965e-02	-1.844e-	1.292e-01	4 201	0 1	12	1 1	37	1 43.28	excellen
01 -5.873e-	01 -1.252e-	-2.804e-	6.116e-02	03 1.409e-01	6.331e-03	4 201	0 1	13	6 0	57	7 06.71	t good
02 2.607e-02	01 -1.181e-	01 -2.888e-	8.025e-02	1.234e-01	4.154e-02	4 201	0 1	13	0 0	12	7 29.12	excellen
-1.162e-	01 -1.387e-	01 -1.174e-	1.514e-01	5.536e-02	7.558e-02	4 201	0 1	13	4 1	22	6 29.08	t excellen
01 -1.128e-	01 -2.729e-	01 -2.406e-	5.661e-02	5.175e-02	3.753e-01	4 201	0 1	14	0 0	46	4 13.91	t excellen
01 -5.101e-	02 -1.756e-	01 -8.505e-	1.953e-01	1.276e-03	1.195e-01	4 201	0 1	15	5 1	37	4 25.94	t excellen
02 -1.267e-	01 -1.699e-	02 3.343e-02	1.566e-01	-5.422e-	7.857e-02	4 201	0 1	15	5 1	03	5 44.60	t excellen
01	01			02		4	0		5		2	t



6.492e-02	-9.495e-	-2.842e-	6.736e-02	1.452e-01	-3.577e-	201	0	30	0	23	48.62	good
-1.426e-	02 -1.356e-	01 3.347e-03	1.557e-01	-5.829e-	02 1.550e-01	4 201	9	11	9	29	05.66	good
01 3.707e-03	01 3.866e-02	-3.573e-	5.614e-02	02 2.090e-01	2.164e-02	4 201	0	11	3	53	26.50	good
4.380e-02	2.443e-01	01 -1.804e-	4.365e-02	9.993e-02	-2.176e-	4 201	0 1	07	0 1	47	2 20.91	good
2.443e-02	7.095e-02	01 -2.428e-	-8.639e-	-1.620e-	05 3.127e-01	4 201	0 1	09	0 0	24	6 33.41	excellen
-4.203e-	-1.463e-	02 -3.196e-	02 -5.380e-	01 1.433e-01	5.826e-02	4 201	0 1	18	6 2	57	8 03.69	t good
02 -1.860e-	01 8.584e-02	01 -2.758e-	04 1.397e-01	-1.349e-	6.014e-02	4 201	0 1	19	3 0	07	5 50.32	good
01 2.027e-01	-2.424e-	01 -3.047e-	1.709e-01	02 -4.330e-	1.575e-02	4 201	0 1	12	9 1	33	5 04.69	moderate
1 3190 01	02	01	3 1200 02	02	1 9080 02	4	0	07	8	12	3	good
1.3198-01	1.004e-01	-3.8740-	1 172- 01	9.8940-02	1.9080-02	4	0	107	6	12	3	good
-4.011e- 01	-1.326e- 01	-3.893e- 03	1.173e-01	1.595e-02	6.345e-02	201 4	1 0	16	1 6	53	27.37	good
7.443e-02	8.687e-02	-6.603e- 02	-1.453e- 01	-9.859e- 02	1.981e-01	201 4	1 0	09	1 0	16	09.94 5	moderate
1.913e-01	-1.220e- 01	-8.473e- 02	1.936e-01	2.385e-02	4.506e-02	201 4	0 9	29	0 9	57	54.15 8	excellen t
4.999e-02	-1.926e-	-1.244e-	1.754e-01	2.482e-02	3.990e-02	201	0	29	1	03	37.66	excellen +
4.020e-02	-1.230e-	-2.565e-	1.610e-01	1.968e-02	9.601e-02	201	1	12	1	47	01.13	excellen
-2.448e-	-1.879e-	-1.233e-	1.689e-01	9.679e-03	1.193e-01	201	1	05	0	14	37.16	excellen
02 -8.061e-	01 -9.300e-	01 -2.670e-	6.013e-02	1.629e-01	-2.038e-	4 201	0 1	06	2 0	02	8 55.78	t good
02 -2.166e-	02 -2.314e-	01 4.005e-02	5.036e-02	7.205e-02	02 3.578e-02	4 201	0 1	02	4 1	12	9 35.31	weak
01 -3.561e-	01 1.589e-01	1.186e-01	5.145e-02	2.877e-02	4.702e-02	4 201	0 1	06	6 0	13	5 48.62	excellen
01 -1.403e-	-2.150e-	-6.153e-	2.265e-01	1.118e-03	3.928e-02	4 201	0 1	23	6 2	02	6 22,25	t good
02	01	02	1 8900 01	7 1420	1 6420 02	4	0	04	1	20	2	modorato
01	-1.800e-	4.0510-02	1.0900-01	02	1.042e=02	4	0	04	1	29	47.55	INOUETALE
2.446e-01	-1.186e- 01	-1.136e- 01	1.673e-01	-1.161e- 02	4.689e-02	201 4	1 0	07	0 7	26	23.18 0	good
1.281e-01	1.267e-01	-6.919e- 02	8.793e-02	1.446e-01	-8.415e- 02	201 4	1 0	01	2 2	13	54.15 1	good
3.027e-02	-1.918e- 01	-9.497e- 02	1.993e-01	1.073e-02	7.111e-02	201 4	1 0	01	2 0	47	39.52 1	excellen t
3.771e-01	-1.266e-	-1.422e-	1.286e-01	8.113e-02	3.587e-02	201	1	02	0 7	22	03.57	good
5.178e-02	-1.721e-	-2.476e-	2.088e-01	-2.967e-	1.023e-01	201	1	02	0	04	08.64	good
2.550e-02	1.506e-01	-2.807e-	1.688e-02	1.792e-01	-4.140e-	201	1	08	0	05	05.94	weak
-7.821e-	2.190e-01	01 -2.873e-	2.798e-02	1.012e-01	04 -8.510e-	4 201	0 1	08	1	08	1 20.61	excellen
03 -1.751e-	-2.003e-	01 -6.441e-	1.282e-01	-1.701e-	03 6.958e-02	4 201	0 1	08	9 2	16	9 58.20	t good
01 -2.488e-	01 -8.809e-	02 -1.116e-	3.179e-02	02 -3.713e-	3.255e-01	4 201	0 1	17	1 0	41	0 52.96	excellen
01 -1.087e-	02 -7.561e-	01 2.844e-01	6.334e-02	02 1.557e-01	1.754e-02	4 201	1 1	17	4 2	31	2 42.14	t
01	02	4 5590	1 2900 01	5 9520	5 2620	4	1	17	3	24	2	good
01	1.2700-01	-4.5586-	1.3090-01	02	-5.202e-	4	1	17	3		2	good
-1.488e- 01	8./62e-02	2.022e-01	/.869e-02	-1.506e- 01	1.524e-02	201	1 1	16	1 6	44	39.13 8	excellen t
-2.700e- 01	1.514e-01	-2.262e- 02	7.176e-02	8.808e-02	8.496e-02	201 4	1 1	16	1 8	52	09.58 8	moderate
-3.774e- 01	1.336e-01	-1.288e- 01	7.077e-02	-2.171e- 02	4.149e-02	201 4	1 1	21	0 9	57	35.09 6	good



Appendix 3: The additional 5 moment tensors derived over the reporting week.



2014 Nov 17 23:31 42.142 UTC 43:43:5282 N       12113 Bepth: 0.532       50he       North       Est       Dom       Do																		
2014 Nov 17 23:31:42.124 UTC       Solve       Not the East Down       Down         14: 43:725 L2 N       121:18.6192 W       Solve       Not the East Down       Cast Part Stee 02       Cast Part Stee	2014 Nov 17 23 3142,124 UTC       North       Start       North       East       Down         114 43,753 22 N       121.18.6192 W       501/e																	
Lit. 43,7255       Loin - 121,31       Deptr. 0.32       Solve         43,7255       Loin - 121,31       Deptr. 0.32       Solve       Note - 10,56e-01       1,56e-01       1,56e-0	Lit: 43/235 Loir: 121:13 Deptr: 0.352       Solve         Solve       Solve       Norm - 102:04-00 13:58-02         Solve       Solve       Norm - 102:04-02 13:58-02         Solve       Solve       Solve         Solve       Solve       Solve       Solve         Solve       Solve       Solve       Solve       Solve         Solve       Solve       Solve       Solve       Solve         Solve       Solve       Solve       Solve       Solve       Solve         Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve         Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       Solve       S	20	14 Nov 1	7 23:31:4	2.142	UTC								North East	Down	+V		
43:43:522 K 1       12118:6192 W         1       1       1       108:00       1.58:00       17:58:00       1.58:00       17:50:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       17:00:00       1.58:00       11:00:00       1.58:00       11:00:00       1.58:00       11:00:00       1.58:00       11:00:00       1.58:00       1.5	43/33/28/N       12118/519/W         1 <td>La</td> <td>: 43.725</td> <td>5 Lon:</td> <td>-121.</td> <td>31 D</td> <td>epth:</td> <td>0.532</td> <td></td> <td></td> <td></td> <td>Solve</td> <td></td> <td colspan="5">Fast _756e_02 2 84e_01 1 56e_01</td>	La	: 43.725	5 Lon:	-121.	31 D	epth:	0.532				Solve		Fast _756e_02 2 84e_01 1 56e_01				
Name	1       Nor       Az       10       10       Az       10       12       10       Az <t< td=""><td></td><td>43:43.</td><td>5282 N</td><td>121</td><td>:18.61</td><td>192 W</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td>Down 633e=02 156e=0</td><td>1 1 75e=02</td><td>+Crac +Dipol</td></t<>		43:43.	5282 N	121	:18.61	192 W		_					Down 633e=02 156e=0	1 1 75e=02	+Crac +Dipol		
Sta       Dist       Lan       Max       Resid       Point       Tends       Zero       Sta       Dist       Lan       Point       Constraint       Point       Constraint       Point       Constraint       Point       Constraint       Point       Constraint       Point       Point </td <td>Sta       Dist       Ac       Total       Made       Note       Note</td> <td></td> <td>00000 00000 0000000</td> <td></td> <td>+CLV</td>	Sta       Dist       Ac       Total       Made       Note													00000 00000 0000000		+CLV		
Image         Opt         Art         Image         Control         Arrow         Free           1         NM03         306         12         008         14         118         14         118         14	I       NN03       0.5t       1       1       Rest       Rest       Number 1       Rest       Rest <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Scalar M0 = 2.837e-01</td><td></td><td>Dipole</td></th<>													Scalar M0 = 2.837e-01		Dipole		
1       NM00       306       12       000       HP       P       0.011       I       I       1.1       1.2       1.1	I       Nu00       3.06       12       Nu00       1.06       H       P       0.011       I       I       1.06       2.164+01       2.464+01		Sta	Dist	Az	1	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq	T = -0.368 k = 0.179				
2       NM03       3.06       12       108       EHT       5H       0.002 $\vec{u}$ $\vec{u}$ 2.112+02       1.42e-01 $\vec{u}$	2       NM03       308       92       100       HT       SH       0.002       Ø       P       Ø	1	NM03	3.06	12	108	EHU	Р	0.011	<b>I</b> -		✓ -1.61e+01	2.46e+01	Total Penalty - 0.166		-1		
B       NM06       0.83       97       154       EHU       P       0.001       Ø       Ø       Ø       0.22       1.38e401         A       NM06       0.83       97       154       EHU       P       0.001       Ø       -       0.22       Ø       1.38e401         S       NM22       0.11       104       176       EHT       SH       0.016       Ø       +       Ø       1.38e401       1.58e401         NM42       3.76       42       102       EHT       SH       0.016       Ø       ·       Ø       9.66402       1.58e401         NM42       3.76       42       102       EHT       SH       0.128       Ø       Ø       3.278e401       1.58e401         10       NM07       3.13       338       105       EHT       SH       0.028       ·       Ø       3.272e402       2.8e401         1       NM08       1.99       286       1.22       EHT       SH       0.028       ·       Ø       5.36e-01       1.64e401         1       NM08       1.99       286       1.22       PHU       P       0.028       Ø       S.36e-01       1.64e401       <	3       NN06       0.88       97       154       EHU       P       0.017       √       √       √       √       2.12e-02       1.38e-01	2	NM03	3.06	12	108	EHT	SH	0.082	- N		-2.11e+02	1.42e+01	fotal fenancy = 01200				
a       NM06       0.83       97       154       EHR       SV       0.098       Ø +       0.020       Ø 3.38+03       185e+01         5       NM22       0.11       104       176       EHU       P       0.028       Ø +       Ø 3.38+03       185e+01         7       NM42       3.76       42       102       EHU       P       0.028       Ø +       Ø -       Ø - 120e+02       1.15e+01         10       NN07       3.76       42       102       EHT       SN       0.101       Ø +       Ø - 120e+02       1.15e+01         10       NN07       3.13       338       105       EHU       P       0.015       Ø -       Ø - 327e+01       161e+01         11       NN07       3.13       338       105       EHT       SN       0.042       Ø -       Ø - 220e+02       226e+01         12       NN07       1.98       284       122       EHX       N       0.028       Ø -       Ø - 820e+02       226e+01         14       NN06       1.98       284       122       EHX       SN       0.028       Ø - 1.14e+03       110e+01         1       NM42       Ø PSV       0.027	Image: Note ()       0.83       07       154       EHR       SV       0.008       Ø       0.020       Ø       3.38e+03       185e+01         Image: Note ()       11       14       176       EHU       P       0.028       Ø       Ø       1.20e+01       1.51e+01         Image: Note ()       104       176       EHU       P       0.028       Ø       Ø       1.20e+01       1.51e+01         Image: Note ()       1.376       42       102       EHU       P       0.028       Ø       Ø       1.31e+01       179e+01         Image: Note ()       Note ()       A       0.15       Ø       Ø       1.31e+01       179e+01       Image: Note ()       Image: Note ()       Note ()       Image: Note ()       I	3	NM06	0.83	97	154	EHU	Р	0.017	<b>v</b> -		-2.12e+02	1.38e+01		POI ARITIES			
S       NM22       0.11       104       77       EHU       P       0.024       Ø       M 402       3.16       M1       106       176       EHU       S       0.016       Ø       1.28e+01       1.51e+01         7       NM42       3.76       42       102       EHI       SV       0.107       Ø       9.16e+02       2.07e+01       1.51e+01       I.51e+01	S       NM22       0.11       104       176       EHU       P       -0024       Ø       I       346e+02       128e+01         NM22       0.11       104       176       EHU       P       -0024       Ø       I       1218e+01       1518e+01         NM42       376       42       102       EHR       SV       0.012       Ø       I       1218e+01       1738e+01       1538e+01       154e+01       184e+01       1738e+01       1738e+01       1738e+01       1538e+01       154e+01       1738e+01       154e+01       1738e+01       154e+01       1738e+01       154e+01       1738e+01       154e+01       1738e+01       154e+01       154e+01       1738e+01       154e+01       154	4	NM06	0.83	97	154	EHR	SV	0.098	<b>√</b> +	0.020	✓ 3.33e+03	1.85e+01		TOLANITILS			
6       NM22       0.11       104       176       EHT       SH       0.016       I       V       2.13e+03       1.51e+01         7       NM42       3.76       42       102       EHT       SH       0.016       I       V       1.20e+02       1.15e+01         8       NM42       3.76       42       102       EHT       SH       0.115       I       V	6       NM22       0.11       104       176       EHT       SH       0.016       Image: Constraint of the section of the sectin of the section of the section of the section	5	NM22	0.11	104	176	EHU	Р	-0.024	<b>√</b> +		✓ 3.46e+02	1.29e+01					
7       NM42       3.76       42       102       EHU       P       -0.023       Image: constraint of the second consecond constraint of the sec	7       NM42       3.76       42       102       EHU       P       -0.023       -       -       -       1.15e+01         8       NM42       3.76       42       102       EHU       SV       0.107       -       -       9.16e+02       2.07e+01         9       NM42       3.76       42       102       EHU       SV       0.107       -       -       9.16e+02       2.07e+01         10       NNO7       3.13       338       105       EHU       P       0.015       -       -       2.27e+01       1.15e+01         11       NNO7       3.13       338       105       EHI       SV       0.001       +       0.356+01       1.86e+01         14       NN09       1.99       296       122       EHZ       S0       0.028       +       0       8.56+01       1.16e+01       1.10e+01         1       NM06       P.SV       0.002       -       -       1.14e+01       1.10e+01       1.10e+01         1       NM06       P.SV       0.002       -       -       1.14e+01       1.10e+01       1.10e+01         1       NM06       P.SV       0.002       SV.SH <td>6</td> <td>NM22</td> <td>0.11</td> <td>104</td> <td>176</td> <td>EHT</td> <td>SH</td> <td>0.016</td> <td><b>√</b> +</td> <td></td> <td>✓ 2.13e+03</td> <td>1.51e+01</td> <td>P To</td> <td>SH CT</td> <td>SV</td>	6	NM22	0.11	104	176	EHT	SH	0.016	<b>√</b> +		✓ 2.13e+03	1.51e+01	P To	SH CT	SV		
8       NM42       3.76       42       102       EHH       SV       0.107       0       0       9.8168+02       2.078+01         9       NM42       3.76       42       102       EHT       SH       0.125       0       +       0       1.138+03       1.798+01         10       NN07       3.13       338       105       EHI       SH       0.015       0       -       0       3.276+01       1.818+01         12       NN07       3.13       338       105       EHT       SH       0.047       0       -       0       2.268+01       1.548+01         12       NN07       3.13       338       105       EHT       SH       0.047       0       -       0       2.268+01       1.548+01         14       NN09       1.99       296       122       EH       SN       0.028       +       0       5.389+02       2.668+01       1.548+01         1       NM06       P SV       0.050        -       1       1.064,01       1.1064,01       1.064,01         1       NM06       P SV       0.002        -       -       1       1.064,01       1.064,01	8       NM42       3.76       42       102       EHR       SV       0.107       Image: model in the ima	7	NM42	3.76	42	102	EHU	Р	-0.023	<b>1</b> -		✓ -1.20e+02	1.15e+01			No No		
9       NM42       3.76       42       102       EHT       SH       0.125       #       1.13e+03       1.79e+01         10       NN07       3.13       338       105       EHU       P       0.015       #       #       3.27e+01       1.61e+01         11       NN07       3.13       338       105       EHT       SN       0.047       #       #       3.27e+01       1.61e+01         13       NN09       1.99       296       122       EHZ       P       0.011       #       #       5.36e+01       1.64e+01         14       NN09       1.99       296       122       EHX       SN       0.025       -       d       1.10e+01         1       NM03       PSH       SN       0.025       -       d       1.10e+01       1.10e+01       SN       F       H	9       NM42       376       42       102       EHT       SH       0.125       0       1.13e+03       1.79e+01         10       NN07       3.13       338       105       EHH       P       0.015       0       -       0.327e+01       1.81e+01         11       NN07       3.13       338       105       EHH       SH       0.015       0       -       0.272e+02       2.88e+01         13       NN09       1.99       266       122       EHX       SN       0.028       -       0.272e+02       2.86e+01         14       NN09       1.99       266       122       EHX       SN       0.028       -       0.13ee01       1.10ee01         1       NM03       P.5H       0.025       -       0.13ee03       1.10ee01       0       SN       0.28ee01       SN       0.28ee01       SN       0.28ee01       SN       0.28ee01       SN       SN       SN       SN       SN       0.28ee01       SN       0.28ee01       SN	8	NM42	3.76	42	102	EHR	SV	0.107	<b>1</b> -		✓ -9.16e+02	2.07e+01			((		
10       NN07       3.13       338       105       EHU       P       0.015       \$\vee\$ -       \$\vee\$ -       3.27e+01       1.81e+01         11       NN07       3.13       338       105       EHR       SV       0.034       \$\vee\$ -       \$\vee\$ -272e+02       228e+01         12       NN07       3.13       338       105       EHR       SV       0.047       \$\vee\$ -       \$\vee\$ -272e+02       228e+01         14       NN09       1.99       296       122       EHN       SN       0.028       \$\vee\$	10       NN07       3.13       338       105       EHU       P       0.015       \$\vee\$ -	9	NM42	3.76	42	102	EHT	SH	0.125	<b>v</b> +		✓ 1.13e+03	1.79e+01	$(\neg, +\circ/\neg)$		$H_{a} + 4$		
11       NN07       3.13       338       105       EHR       SV       0.034       -       -       2.72re402       2.26e+01         12       NN07       3.13       338       105       EHT       SH       0.047       -       -       -       2.26e+01         13       NN09       1.99       296       122       EHZ       P       0.001       +       - <t< td=""><td>11       NN07       3.13       338       105       EHR       SV       0.034       -       -       2.722402       2.26e+01         12       NN07       3.13       338       105       EHT       SH       0.047       -       -       2.26e+02       1.88e+01         13       NN09       1.99       286       122       EHZ       P       0.001       -       -       -       2.20e+02       1.88e+01         14       NN09       1.99       286       122       EHX       SN       0.025       -       -       -       1.10e+01         1       NN05       1.99       296       122       EHX       SN       0.025       -       -       1.10e+01       -       SN       -       SN       -       -       -       -       -       -       -       -       SN       -       -       -       -       -       -       SN       -</td><td>10</td><td>NN07</td><td>3.13</td><td>338</td><td>105</td><td>EHU</td><td>Р</td><td>0.015</td><td><u>-</u></td><td></td><td>✓ -3.27e+01</td><td>1.61e+01</td><td></td><td></td><td></td></t<>	11       NN07       3.13       338       105       EHR       SV       0.034       -       -       2.722402       2.26e+01         12       NN07       3.13       338       105       EHT       SH       0.047       -       -       2.26e+02       1.88e+01         13       NN09       1.99       286       122       EHZ       P       0.001       -       -       -       2.20e+02       1.88e+01         14       NN09       1.99       286       122       EHX       SN       0.025       -       -       -       1.10e+01         1       NN05       1.99       296       122       EHX       SN       0.025       -       -       1.10e+01       -       SN       -       SN       -       -       -       -       -       -       -       -       SN       -       -       -       -       -       -       SN       -	10	NN07	3.13	338	105	EHU	Р	0.015	<u>-</u>		✓ -3.27e+01	1.61e+01					
12       NN07       3.13       338       105       EHT       SH       0.047       \$	12       NN07       3.13       338       105       EHT       SH       0.047       \$	11	NN07	3.13	338	105	EHR	SV	0.034	-		✓ -2.72e+02	2.26e+01					
13       NN09       1.99       286       122       EHZ       P       0.001       Image: Minited and the state of the state	13       NN09       1.99       286       122       EHZ       P       0.001       Image: Minited in the state of the state o	12	NN07	3.13	338	105	EHT	SH	0.047	<b>1</b> -		-2.08e+02	1.88e+01					
11       NN09       1.99       286       122       EHN       SN       0.028       +       Ø       8.538+02       2.668+01         1       NN03       1.99       280       122       FHF       SF       0.025       -       of       1.10e.01         1       NM03       P.SH        0.025       -       of       1.10e.01       0.01         1       NM03       P.SH         0.025       -       of       1.10e.01       0.01         1       NM03       P.SH          0.025       -       of       0.01 <td>11       NN09       1.99       286       122       EHN       SN       0.028       +       Ø       8.538+02       2.668+01         1       NN03       1.99       286       1.22       FHE       SE       0.025       -       Ø       1.10e.01         1       NM03       PSH        0.025       -       Ø       1.10e.01       0.010</td> <td>13</td> <td>NN09</td> <td>1.99</td> <td>296</td> <td>122</td> <td>EHZ</td> <td>Р</td> <td>0.001</td> <td>₩ +</td> <td></td> <td>✓ 5.36e+01</td> <td>1.64e+01</td> <td></td> <td></td> <td></td>	11       NN09       1.99       286       122       EHN       SN       0.028       +       Ø       8.538+02       2.668+01         1       NN03       1.99       286       1.22       FHE       SE       0.025       -       Ø       1.10e.01         1       NM03       PSH        0.025       -       Ø       1.10e.01       0.010	13	NN09	1.99	296	122	EHZ	Р	0.001	₩ +		✓ 5.36e+01	1.64e+01					
Image: NNPA         1.99         296         122         FHF         SE         0.025         -         Image: NPA for the second s	I       NMA       1.99       296       122       FHE       SE       0.025       -       I 1.10a+01         1       NM3       P.5H       -       I       I.1.10a+01       1.10a+01       -       I       Image: Second Sec	14	NN09	1.99	296	122	EHN	SN	0.028	+		✓ 8.53e+02	2.66e+01		SN	SE		
Sta       Type       Penalty         1       NM03       PSH         2       NM06       PSV         3       MM42       PSV         4       MM42       PSV         5       NM42       PSV         6       NN07       PSV         6       NN07       PSV         7       NSH         8       NN07         9       SV/SH         10       NN17         9       PSH         11       NN17         11       NN17         9       PSH         13       NN19         14       NN19         9       PSH         13       NN19         14       NN19         15       NN16         16       NN07	Sta       Type       Penalty         1       NM03       PSH         2       NM06       PSV       0.050         3       M442       PSH       1         5       NM42       PSV       0.012         4       M42       PSH       1         5       NM42       PSV       0.027         6       NN07       PSV       0.002         7       NN07       PSV       0.002         8       NN07       SV:SH       9         9       NN17       PSV       10         10       NN17       PSH       11         11       NN17       SV:SH       9         12       N18       PSH       13         13       N19       PSH       14         14       N19       PSH       14         14       N19       PSH       14	10	NN09	1.99	296	122	FHF	SF	0.025	<u> </u>		✓ -1 14e+03	1 10e+01					
1       NM05       PSH         2       NM06       PSV         3       NM42       PSV         4       NM42       PSV         5       NM42       PSV         6       NN07       PSV         7       NN07       PSH         8       NN07       PSH         10       NN17       PSH         11       NN17       PSH         12       NN18       PSH         13       NN19       PSH         13       NN19       PSH         14       NN19       PSH	1       NM0       PSH         2       NM06       PSV       0.050         3       NM42       PSV       0.012         4       MM42       PSV       0.012         5       NM42       PSV       0.027         6       NN07       PSV       0.002         7       NN07       PSH          8       NN07       PSV       0.002         7       NN07       PSH          9       NN17       PSH          10       NN17       PSH          11       NN17       PSH          12       NN18       PSH          13       NN19       PSV          14       NN19       PSV          14       NN19       SV/SH		Sta	Type	-	Penalty	,											
-       NM06       Ø       PSV       0.050         3       NM42       Ø       PSV       0.012         4       NM42       Ø       PSH          5       NM42       Ø       PSV       0.027         6       NN07       Ø       PSV       0.002         7       NN07       Ø       PSH          8       NN07       Ø       PSH          9       NN17       Ø       PSH          10       NN17       Ø       PSH          11       NN16       Ø       Ø       PSV         13       NN18       Ø       PSV          14       NN19       Ø       PSV          14       NN19       Ø       PSV          14       NN19       Ø       SV/SH	2       NM06       Ø       PSV       0.050         3       NM42       Ø       PSN       0.012         4       NM42       Ø       PSN       0.027         5       NM42       Ø       SVSH       0.027         7       NN07       Ø       PSN       0.002         7       NN07       Ø       PSN       0.002         7       NN07       Ø       PSN       0.002         10       NN17       Ø       PSN       0.002         10       NN17       Ø       PSN       0.002         10       NN17       Ø       PSN       0.002         11       NN17       Ø       SN5H       0.002         12       NN18       Ø       PSN       0.002         13       NN19       Ø       PSN       0.002         14       NN19       SV/SH       0.002       0.002         14       NN19       SV/SH       0.002       0.002	1	NM03	P:S	4	( entirely									$\Gamma + 7$	$\Gamma$ $+$ 7		
Image: String	a       NM42       Ø PSV       0.012         4       NM42       Ø PSH          5       NM42       Ø SVSH       0.027         6       NN07       Ø PSH          7       NN07       Ø SV       Ø SVSH         9       NN17       Ø SV       Ø         9       NN17       Ø SV       Ø         9       NN17       Ø SV       Ø         10       NN17       Ø SV       SH         10       NN17       Ø SV       Ø         11       NN17       Ø SV       Ø         12       NN18       Ø SV       Ø         13       NN19       Ø SV       Ø         14       NN19       Ø SV SH       Ø	2	NM06	P:S	v (	0.050	-											
4       MM42       V       PSH         5       MM42       V       SVSH       0.027         6       NN07       V       PSV       0.002         7       NN07       PSH       B       NN07       SV5H         8       NN07       SV5H       B       PSH       B         10       NN17       PSH       B       PSH       B         11       NN18       PSH       B       PSH       B       PSH       B         13       NN19       PSH       PSH       B       B       PSH       B       B       PSH       B	4       MM42       V       P.SH         5       MM42       V       P.SH         5       NM42       V       SV-SH         6       NN07       VSV       OROZ         7       NN07       P.SV       OROZ         8       NN07       SV-SH       PSV         9       NN17       P.SV       PSV         10       NN17       P.SH       PSH         12       NN18       P.SH       PSH         13       NN19       P.SH       PSH         14       NN19       P.SH       PSH         14       NN19       SV.SH       PSH	3	NM42	P:S	v (	0.012	-											
5       NM42       V       SV:SH       0.027         6       NN07       V       PSV       0.002         7       NN07       PSH       B       NN07       SV:SH         8       NN07       SV:SH       B       PSV       D         10       NN17       PSH       D       PSH       D         11       NN17       PSH       D	5       NM42       V       SV:SH       0.002         6       NN07       V       PSV       0.002         7       NN07       PSH       B       NN07       SV:SH         9       NN17       PSH       11       NN17       PSH         10       NN17       PSH       11       NN17       SV:SH         12       NN18       PSH       13       NN19       PSV       14         14       NN19       SV:SH       SV:SH       SV:SH       SV:SH	4	NM42	✓ P:S	H		-									_		
6         NN07         PSV         0.002           7         NN07         PSH           8         NN07         SVSH           9         NN17         PSH           10         NN17         PSH           11         NN17         SVSH           13         NN19         PSH           14         NN19         PSH           15         NN19         SVSH	6       NN07       V       PSV       0.002         7       NN07       PSH       0.002       PSH         8       NN07       SV:SH       0.002         9       NN17       PSH       0.002         11       NN17       PSH       0.002         12       NN18       PSH       0.002         14       NN19       PSV       0.002         14       NN19       SV:SH       0.002	5	NM42	SV:	SH (	0.027	-											
7       NN07       PSH         8       NN07       SV:SH         9       NN17       PSV         10       NN17       PSH         11       NN17       SV:SH         12       NN18       PSH         13       NN19       PSH         14       NN19       PSH         1r       NN19       SV:SH	7       NN07       PSH         8       NN07       SV:5H         9       NN17       PSV         10       NN17       PSH         11       NN17       SV:5H         12       NN18       PSH         13       NN19       PSH         14       NN19       SV:5H         ver NN19       SV:5H	6	NN07	✓ P:S <sup>2</sup>	v i	0.002	-								AMPLITUDE RATIOS			
8         NN07         SV:SH           9         NN17         PSV           10         NN17         PSH           11         NN17         SV:SH           12         NN18         PSH           13         NN19         PSH           14         NN19         PSH           1x         NN19         SV:SH	8       NN07       SV:SH         9       NN17       PSV         10       NN17       PSH         11       NN17       SV:SH         12       NN18       PSH         13       NN19       PSV         14       NN19       SV:SH         vr. NN19       SV:SH	7	NN07	P:S	H		1											
9       NN17       PSV         10       NN17       PSH         11       NN17       SVSH         12       NN18       PSH         13       NN19       PSH         14       NN19       PSH         1x       NN19       SVSH	9       NN17       PSV         10       NN17       PSH         11       NN17       SVSH         12       NN18       PSH         13       NN19       PSH         14       NN19       PSH         1       SVSH       SVSH	8	NN07	SV:	SH		1							D.SH	D.SW	SV-SHT		
10       NN17       PSH         11       NN17       SV5H         12       NN18       PSH         13       NN19       PSH         14       NN19       PSH         1x       NN19       SV5H	10       NN17       PSH         11       NN17       SV:SH         12       NN18       PSH         13       NN19       PSV         14       NN19       PSH         1r       NN19       SV:SH	9	NN17	P:S	v		1											
11         NN17         SV:SH           12         NN18         PSH           13         NN19         PSV           14         NN19         PSH           1r         NN19         SV:SH	11       NN17       SV:SH         12       NN18       PSH         13       NN19       PSV         14       NN19       SV:SH         ve       NN19       SV:SH	10	NN17	P:S	н		1											
12         NN18         PSH           13         NN19         PSV           14         NN19         PSH           1c         NN19         SV/SH	12         NN18         PSH           13         NN19         PSV           14         NN19         PSH           1c         NN19         SV/SH	11	NN17	SV:	SH		1							HIVE H				
13         NN19         Ø         PSV           14         NN19         PSH           1c         NN19         SV/SH	13         NN19         Ø         PSV           14         NN19         PSH           1c         NN19         SV/SH	12	NN18	P:S	н		-											
14 NN19 PSH 11 NN19 SV/SH	14 NN19 PSH 17 NN19 SVSH	13	NN19	P:S	v		1											
		14	NN19	P:S	H		1								A.			
		10	NN19	□ sv	ян										401			



# ○ ○ ○

2014 Nov 17 3:34:37.422	UTC							North East Do	own	+V
Lat: 43.7283 Lon: -121	.311 Depth:	0.527				Solve		Fast 1 28e-01 -4 56e-02 -5 85	e-01	
45.45.0992 N 121	1.10.0774 ₩		_					Down 1.39e-01 -5.85e-02 -5.20	6e-02	+Dipol
										+CLV
								Scalar M0 = 2.704e-01		Dipole
Sta Dist Az	i Chan	Phase	Resid	Polarity	Penalty	Amp	Freq	I = 0.951  k = -0.506		
1 NM03 2.77 15	112 EHU	Р	0.023	<b>I</b> -		-2.21e+01	1.79e+01	Total Penalty = 0.155		-V
2 NM06 0.99 115	149 EHU	P	0.036	🗹 +		✓ 2.98e+02	3.59e+01			
3 NM06 0.99 115	149 EHR	SV	0.075	🗹 +		✓ 1.55e+03	8.63e+02		POLARITIES	
4 NM06 0.99 115	149 EHT	SH	0.038	🗹 +		✓ 1.41e+03	1.61e+01			
5 NM22 0.39 151	167 EHU	P	-0.026	🗹 +		✓ 3.88e+02	1.56e+01			
6 NM22 0.39 151	167 EHT	SH	-0.027	🗹 +		✓ 1.59e+03	1.51e+01	P SH		SV
7 NM40 2.78 114	112 EHU	Р	0.046	<b>v</b> -						$\langle \rangle$
8 NM40 2.78 114	112 EHT	SH	0.018	<b>I</b> -		✓ -2.96e+02	1.85e+01		$\backslash \bullet \land$	$\left( \cdot \right) $
9 NM42 3.58 46	103 EHU	Р	-0.010	<b>v</b> -		✓ -9.63e+01	1.07e+01		· +, / -]	+ + + +
10 NM42 3.58 46	103 EHR	sv	0.136	<b>v</b> -		✓ -7.50e+02	2.05e+01		<u>°</u> (°/	
11 NN07 2.80 337	109 EHU	P	0.033	<u> </u>		✓ -5.40e+01	1.34e+01			
12 NN07 2.80 337	109 EHR	sv	0.094	<u> </u>		✓ -3.70e+02	1.54e+01			
13 NN07 2.80 337	109 EHT	SH	0.066	<u> </u>	0.014	✓ -2.89e+02	1.31e+01			
14 NN09 1.80 287	126 EHU	Р	0.019	<b>V</b> -		✓ -2.48e+00	2.70e+01	SN		SE
1c NN09 1.80 287	126 FHR	sv	0.003	0 +		√ 2 92e+02	1 54e+01			
Sta Type	Penalty									
1 NM06 PSV	0.012							F	· + ']	F + 7
2 NM06 2 PSH	0.008								т /	\ T /
2 NM06 SV:SH	0.000							Ň		
4 NM22 PSH	0.013								$\mathbf{\mathbf{U}}$	$\mathbf{\Psi}$
F NM42 PSV	0.019									
c NN07 PSV	0.010							AME	PLITUDE RATIOS	
7 NN07 PSH										
A NN07 SV/SH										
8 NN07 3V.3H								P:SH P:S	Y BARA	SV:SH
g NN09 F.3V										
10 NN09 F.SH								All All All		A CONTRACTOR
11 NN09 SV:SH	0.007									Sector S
12 NN17 PSV	0.007							Viender V	Keessen .	
13 NN17										CARD -
14 NN17 SV:SH								ARGE.	12222	

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201	4 Nov 16	5 18:52	9.588	UTC								North	h East	Down	+V
Lat	43.727	4 Lon:	-121	.311	Depth:	0.6				Solve		North -2.70e	-01 1.51e-01	7.18e-02	
	43:43.6	541 N	121:	18.65	IW		_					Down 7.18e	-02 8.81e-02	8.50e-02	+Crac +Dipol
												20000 7.100	02 0.010 02	0.500 02	+CLV
												Scalar M0 = 2.	.759e-01		Dipole     Crack
	Sta	Dist	Az	i	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq	T = 0.100 K =	0.201		
1	NM06	0.92	110	153	EHU	Р	0.028	✓ +	0.010	✓ 1.99e+02	1.84e+01	Total Penalty :	= 0.173		-V
2	NM06	0.92	110	153	EHT	SH	0.042	🗹 +	0.002	✓ 1.62e+02	1.59e+01				
3	NM22	0.28	147	171	EHU	Р	-0.027	🗹 +		2.07e+02	1.58e+01			POLABITIES	
4	NM22	0.28	147	171	EHT	SH	-0.012	<b>√</b> +		✓ 6.72e+02	1.48e+01				
5	NM42	3.63	45	105	EHU	Р	0.053	+		✓ 8.92e+01	1.06e+01				
6	NM42	3.63	45	105	EHT	SH	0.089	- 1		✓ -1.91e+02	1.16e+01	P /		SH 🔨	SV
7	NN07	2.92	337	110	EHU	Р	0.019	<b>1</b> -		✓ -2.48e+01	1.45e+01	· / °			
8	NN07	2.92	337	110	EHR	SV	0.092	<b>√</b> +		✓ 1.46e+02	8.92e+00		~ • V		
9	NN07	2.92	337	110	EHT	SH	0.093	- +		✓ 1.96e+02	1.21e+01	F -	<b>★</b>	+ + + +	$F \rightarrow H$
10	NN09	1.86	290	126	EHU	Р	0.020	<b>√</b> +	0.013	✓ 5.25e+00	1.79e+01	•	× /	$F \mid /$	\ <u>`</u> • )/
11	NN09	1.86	290	126	EHR	SV	0.002	- +		✓ 1.41e+02	1.84e+01	~			
12	NN09	1.86	290	126	EHT	SH	0.035			✓ 1.11e+02	1.98e+01	<u> </u>		$\square$	$\smile$
13	NN17	1.53	241	134	EHU	Р	-0.012	<b>1</b> +		✓ 9.73e+00	2.83e+01				
14	NN17	1.53	241	134	EHR	SV	0.019	<u> </u>		✓ -5.33e+02	1.56e+01			SN /	SE /
10	NN17	1.53	241	134	FHT	SH	-0.008	<u> </u>		J -3.01e+02	1 20e+01				
	Sta	Tvn	•	Penalta	,										
1	NM06	J P	SH	renary											
1	NM22	J P	зн	0.069	-										
2	NM42	- P4	5H	0.000	-										
3	NN07	- P!	sv		-									Ť	Ť
5	NN07	- P1	SH		-										
6	NN07		:SH		-									AMPLITUDE RATIOS	
7	NN09	- P:	SV		-										
8	NN09	P1	SH I		-										au au Ar
0	NN09		(SH		-							P:SH	S STAN	P:Sy	SV:SALA
9	NN17	P1	sv		-							A Bar	ALC A		RESCHER
10	NN17		SH I		-							A SANCE			
11	NN17	F.4	USH		-										
12	NN19	0.04	21		-							23	7-887	19572 - S	A STARS
13	NN10		20	0.050	-							<u></u>	NY A	SIPP	No and a second
14	ININ18	Pa O Cl	ort .	0.056	-							2	22.9.4.0	2244.	
10	MN18	- SV	-SH I												



2014 No	v 16 16	44:39.1	38 UTC								North East Down		+V
Lat: 43.	7266 L	on: -12	21.311	Depth:	0.616				Solve		North - 1.49e-01 8.76e-02 7.87e-02 Fast 8.76e-02 2.02e-01 - 1.51e-01		
45.	43.3334	14 1	21.10.0	342 11							Down 7.87e-02 -1.51e-01 1.52e-02		+Dipol
												+0	
											Scalar M0 = $2.611e-01$ T = $_0 112$ k = $0.079$		Crack
Sta	Dis	t Az	1	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq	1 = -0.112 K = 0.079		
1 NM0	3 2.8	94 1	3 112	EHU	P	0.038	₫ -		✓ -7.81e+00	4.18e+01	Total Penalty = 0.152		-v
2 NM0	6 0.8	37 10	5 154	EHU	Р	0.024	<b>V</b> +		2.51e+02	1.32e+01			
3 NM2	2 0.2	20 13	9 1/4	EHU	P	-0.019	✓ +		✓ 4.75e+02	1.55e+01	POLARIT	TIES	
4 NM4	1 2.3	36 13	9 121	EHT	SH	0.026	₫-						
5 NM4	2 3.0	58 4	3 105	EHU	P	-0.016	• 🗹		✓ 1.70e+01	2.10e+01			
6 NM4	2 3.6	8 4	3 105	EHT	SH	0.059	-		✓ -5.11e+02	9.49e+00	P STO SH	S S	
7 NN0	7 3.0	0 33	7 109	EHU	P	0.003	<b>-</b>		✓ -7.22e+01	1.42e+01		• \	$\left( \begin{array}{c} \gamma \end{array} \right)$
8 NN0	7 3.0	0 33	/ 109	EHT	SH	0.061	✓ +	0.027	✓ 4.32e+02	1.27e+01		•	
9 NN0	9 1.8	92 29	2 126	EHU	P	0.007	<b>v</b> -		✓ -9.06e+00	2.21e+01			$\langle \cdot \rangle \subseteq I$
10 NN0	9 1.8	2 29	2 120	EHR	SV	-0.034	+		✓ 3.92e+02	1.38e+01		• /	
11 NN09	9 1.8	2 29	2 120	EHT	SH	0.002	+		2.51e+02	1.55e+01			
12 NN1	7 1.3	24	5 135	EHU	P	-0.010	✓ +		2.08e+01	2.23e+01			
13 NN1	7 1.4	1 24	5 100	EHR	SV	0.033	✓ -		✓ -1.19e+03	1.64e+01	SN	<u> </u>	
14 NN1	7 1.8	24	5 135	EHT	SH	0.001	₫ -		✓ -5.62e+02	1.30e+01	SIV P	3	P <sup>E</sup> P '
ie NN1	8   14	+0   2	9 138	FHU	P	-0.007	<b>V</b> -	0.016	✓ -7 04e+01	1 62e+01			( )
Sta	1	Туре	Penalt	y							F +	<b>-</b>	$\left( + \frac{1}{2} \right)$
1 NM4	2	P:SH		_									
2 NN0	7	P:SH		_									$\backslash$
3 NN05	•	P:SV		_								/	
4 NN0	•	P:SH		_									
5 NN0		SV:SH		_							AMPLITUDE	RATIOS	
6 NN1		P:SV		_									
7 NN1		P:SH		_								4	
8 NN1		SV:SH		_							P:SH P:SV	S S	V:SH
9 NN18	3 🗹	P:SV	0.015	_							STREET STREET	RYX.	
10 NN18	3	P:SH		_									
11 NN18	3	SV:SH		_									
12 NN19		P:SV	0.05-	_								1510	ASSEE S
13 NN19		P:SH	0.053	_									
14 NN19		SV:SH	0.013	_							THE TEST	E.a	
1c NN2		pisv											



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$\langle a \rangle$		
V		- 7

2014 Nov Lat: 43.72 43:4	21 9:57: 273 Lon: 3.6398 N	35.096 -121 121	UTC .311 .:18.6	Depth: 504 W	0.76				Solve		North East North -3.77e-01 1.34e-0: East 1.34e-01 -1.29e-01 Down 7.08e-02 -2.17e-0 Scalar M0 = 3.221e-01	Down 1 7.08e-02 1 -2.17e-02 2 4.15e-02	+Crip +Dipole
Sta	Dist	Az	1	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq	T = 0.574 k = -0.347		Crack
14 MN17	1.53	242	138	EHU	P.	-0.012			✓ 1.0001.01	1 990+01	Total Penalty = 0.176		-1
16 NN17	1.53	242	138	EHT	SH	0.007	<b>V</b> -		✓ -1.44e+03	2.30e+01			
17 NN18	1.34	32	143	EHU	P	0.002	<b>√</b> -		✓ -1.89e+02	1.66e+01		POLARITIES	
18 NN18	1.34	32	143	EHR	sv	0.006	<u> </u>		✓ -2.24e+03	1.39e+01			
19 NN19	1.05	163	150	EHU	Р	-0.002	<b>√</b> +	0.013	✓ 4.58e+02	1.76e+01			
20 NN19	1.05	163	150	EHT	SH	0.051	<b>v</b> -	0.021	-1.53e+03	1.64e+01		SH	SV
21 NN21	1.81	69	133	EHU	Р	-0.009	<b>v</b> -		✓ -6.16e+01	1.64e+01		$\langle \rangle$ , $\lambda$	
22 NN21	1.81	69	133	EHT	SH	0.068	- 🗌		✓ -1.36e+03	1.79e+01		$+$ $\frac{1}{4}$	
23 NN24	0.55	17	164	EHU	Р	-0.008	<b>v</b> -		✓ -6.56e+01	2.06e+01		6 %	
24 NN24	0.55	17	164	EHR	sv	-0.001	<b>√</b> +		2.16e+03	3.19e+01			
25 NN24	2.03	207	114	EHT	SH	-0.041	✓ +		✓ 1.09e+03	3.66e+01			
26 NN32	2.93	207	114	EHU	P	0.018	<b>v</b> -		✓ -5.95e+01	1.40e+01			
27 NN32	2.93	207	114	EHR	SV	0.050	-		<ul> <li>-1.35e+03</li> <li>0.080+02</li> </ul>	1./80+01		SN P	SE
5 Sta 6 NN07 7 NN09 8 NN09	Typ P: P: P:	e SH SV SH	Penalty										( + ) 
9 NN09	S S	/:SH		_									
10 NN17	✓ P: 0	SH		_								AMPLITUDE RATIOS	
11 NN18	Pa	SV	0.016	-									
12 NN21	• F.	SH	0.010								P:SH	PSV	SV:SH
14 NN24	I P:	sv		-							REE FROM	ALL SELLA	
15 NN24	✓ P:	SH	0.003	-									
16 NN24	SV SV	/:SH	0.030	-									
17 NN32	P:	sv		_								N. S. S. S. S. N.	
18 NN32	🗹 P:	SH	0.089	-								N SS N	
19 NN32	S\	/:SH									~ & A A A	2 8 B 8 2	

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