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WEEKLY REPORT #4 TO ALTAROCK ENERGY INC.

PROCESSING OF INDUCED EARTHQUAKES ASSOCIATED WITH THE NEWBERRY EGS INJECTION STARTING SEPTEMBER 2014

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Brief summary

Difficulties with transferring the full data from the ISTI system to our computers have settled down. A few channels are still missing or mis-timed, but these problems are minor and not significantly impacting the quality of the results we are able to produce.

We have completed relative relocations for the earthquakes up to 19 October with good results. The earthquakes clearly define a N 45° W striking fault, dipping at ~ 87° to the NE and activated in two depth intervals. One depth interval is the lowest ~ 250 m of the borehole and the other is ~ 200 m below the bottom of the borehole. The along-strike length of the activated fault is ~ 250 m.

During the forthcoming week we will update these results with earthquakes that occurred after 19 October, and we will also relatively locate the largest earthquakes using the high-quality arrival time measurements made for moment tensor calculations.

We derived an additional 10 moment tensors, bringing the currently available set to 34. The pattern of source types observed earlier remains constant with the addition of more results. The source types range from +Dipole to -Dipole with approximately equal numbers of earthquakes showing crack-opening and crack-closure. The T-axes, which gives an indication of the direction of σ_3 , cluster sub-horizontally S±20° or so. The P- and I-axes are more scattered.

1 Task 1 – Planning, conference calls, discussion of work, correspondence, followup

We continued to maintain contact with team members. The issues associated with data completeness and formatting have subsided and the number of missing or incorrectly timed traces is now reduced. We have thus not needed to exchange many emails with ISTI, and our work has proceeded smoothly over the reporting week.

2 Task 2 – System Setup

Tailoring our system setup to the data supplied by ISTI, and tuning the relative location software parameters to the 2014 dataset is now essentially complete.

3 Task 3 – Quality control of prepicked MEQs and preparation for relocation and moment tensor calculation

We continued to derive moment tensors, prioritorising the largest earthquakes as in previous weeks. We continue to use the same procedure as described in our Weekly Report #1. We report here an additional 10 moment tensors. The entire list of earthquakes processed to date is given in

Table 1. We have provided the locations and moment tensor decomposition data of these new moment tensors to Trenton Cladouhos of AltaRock electronically, by email attachment.



Table 1: The 34 earthquakes for which moment tensors have been obtained. Locations given be	ow are
from the webpage http://fracture.lbl.gov/Newberry/locations.txt.	

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287	10	14	5	46	14.161	43.71765	-121.31087	0.161	0.904	

4 Task 4 – Improved locations and relative locations

4.1 Absolute locations

We updated our relocation of the earthquakes to date using **qloc**. The epicentral locations up to Oct. 26 are shown in Figure 1, and a depth vs. time plot for the same locations is shown in Figure 2.

Figure 3 shows the week-by-week development of the seismic sequence for the five weeks to date.

Figure 4 shows ISTI epicentral locations for comparison with Figure 1.

The general picture has not changed with an additional week of earthquakes. The cluster is still centered centered 100 to 200 m north of the bottom of well NWD 55-29 and is quasi-circular with a diameter of \sim 500 m.

Figure 5 and Figure 6 show the locations of the MEQs for which moment tensors were derived. These earthquakes are the largest and most accurately located earthquakes available to date. They form two clusters near the bottom of well NWD 55-29, a shallower cluster slightly to the north of the well and a deeper cluster slightly to the south. The pattern of locations of these earthquakes is similar to the relative locations (see below), providing some "ground truth" to the bimodal spatial distribution observed. Interestingly, this pattern, first reported for the moment-tensor-earthquake locations in last week's report, is now confirmed by the relative location work.





2014 ISTI Picks

Focal Depth, km

Figure 1: Estimated hypocenters of 297 microearthquakes between Sept. 26 and Oct. 26, 2014 within the NMSA network. Most events lie within a circle about 500 m in diameter and centered 100 to 200 m north of the bottom of well NWD 55-29, which is shown in blue. These locations were obtained by using the **qloc** program to invert *P*- and *S*-phase arrival times measured by personnel of the ISTI Corporation on digital seismograms from the NMSA network.





Figure 2: Estimated depths, with respect to sea level, of 297 microearthquakes within the NMSA network as a function of time. The average depth appears to be decreasing slightly with time because of a decrease in the number of deeper events. These depths were obtained by using the **qloc** program to invert *P*- and *S*-phase arrival times measured by personnel of the ISTI Corporation on digital seismograms from the NMSA network.



Figure 3: Hypocenters of microearthquakes within the NMSA network as a function of time. (a) 2014 Sept. 26 - Oct. 02; (b) Oct. 03 - Oct. 09; (c) Oct. 10 - Oct. 16; (d) Oct. 17 - Oct. 23; (e) Oct. 24 - Oct. 26 (shorter interval). There is no clear tendency for the events to migrate with time.



2014 ISTI Catalog



Figure 4: Hypocenters of 297 microearthquakes between Sept. 26 and Oct. 26, 2014 within the NMSA network, as given in the earthquake catalog of the ISTI Corporation. These locations are slightly but significantly west of those shown in Figure 1, which were derived from substantially the same seismic data but using a different computer program. Well NWD 55-29 is shown in blue.



2014



Figure 5: High quality estimated hypocenters of 34 microearthquakes that occurred between Sept. 30 and Oct. 15, 2014, and for which moment tensors were derived. These locations are computed using arrival times measured carefully in connection with the moment-tensor analysis. Well NWD 55-29 is shown in blue.



Figure 6: Expanded view of the locations of the earthquakes for which moment tensors were derived.

4.2 Relative locations

We are well advanced with the relative loction work for the earthquakes that occurred from the start of the sequence up to 19 October. We used program **hypocc**, a relative-location program based on the approach of Waldhauser and Ellsworth [2000] but written in the C programming language. This carries with it many advantages, including extreme speed. This enabled us to explored numerous run-time options to obtain the best possible result with the Newberry data.

Absolute hypocenter location methods such as the method ISTI is using, and our **qloc** locations, analyze one earthquake at a time. The results contain systematic errors caused by by errors in the crustal velocity model.

The relative location method works on a different principle, locating many earthquakes simultaneously, using as data the *differences* between the seismic-wave arrival times at common stations for pairs of earthquakes. The program divides the earthquakes into discrete "clusters" of closely grouped earthquakes, and relocates the events in each cluster relative to one another. This method greatly reduces the effect of systematic errors in the crustal model, and provides much higher resolution of the locations of nearby earthquakes *relative to other earthquakes in the same cluster*.

It is important to realize that the *absolute location of the cluster* is not improved by the relative location process. In order to fix the absolute location of the cluster, we pinnned it to a earthquake well located usign **qloc**. This was the M 1.1 earthquake of 2014 10 02 06:47:52.710, located at a latitude of 43.725296, longitude of -121.308326 and depth of 1.21 km b.s.l.



Our work proceeded as follows:

- We used the hand-measured arrival times provided by ISTI;
- We performed over 20 program runs, systematically varying three parameters in particular. These were:
 - o *minclust*-the minimum number of earthquakes to define a cluster (a value of 10 was used);
 - \circ *maxit*-the maximum allowed number of relocation iterations (optimal value identified = 25);
 - \circ *maxsep*-the maximum separation allowed between linked pairs of earthquakes (optimal value identified = 0.15 km);
 - *minlinks*-the minimum number of "links" (i.e., measured station/phases in common between pairs of earthquakes) needed for an earthquake to be passed to the final relocated set (optimal values identified = 12 or 14);

We present two sets of results, using *minlinks* of 12 and 14.

The results using *minlinks*=12 are shown in Figure 7, Figure 8 and Figure 9. The original input dataset comprised 288 earthquakes, totalling 3411 arrival times. 129 earthquakes passed the stringent quality control parameters. Of these, 16 earthquakes failed the *maxsep* and *minclust* thresholds and were rejected as singlets. 113 earthquakes remained, comprising one cluster.



Figure 7: Map of relative locations of 113 earthquakes that occurred in the time period 26 September - 19 October, 2014. Runtime parameters used were *minclust* = 10, *maxit* = 25, *maxsep* = 0.15 km, minlinks = 12.



Figure 8: Same as Figure 7 except in cross section looking north.



Figure 9: Same as Figure 7 except in cross section looking northwesterly, along the strike of the elongate cluster.

The results using *minlinks*=14 are shown in Figure 10, Figure 11 and Figure 12. 80 earthquakes passed the more-stringent *minlinks* setting. Of these, 14 earthquakes failed the *maxsep* and *minclust* thresholds and were rejected as singlets. 66 earthquakes remained, comprising one cluster.



Figure 10: Map of relative locations of 66 earthquakes that occurred in the time period 26 September - 19 October, 2014. Runtime parameters used were *minclust* = 10, *maxit* = 25, *maxsep* = 0.15 km, *minlinks* = 14.



Figure 11: Same as Figure 10except in cross section looking north.



Figure 12: Same as Figure 10 except in cross section looking northwesterly, along the strike of the elongate cluster.

A brief interpretation is as follows. The epicentral region apparent in ISTI locations is quasi-circular, and the earthquake depths show a single diffuse cloud. In the **qloc** locations, more structure is visible and northwesterly orientated structure can marginally be discerned. This structure is greatly enhanced in the relative locations, which show a clear linear zone striking at N 45°W. In depth section, the cluster clearly forms two subclusters separated by a zone ~ 200 m in depth extent that is almost devoid of earthquakes. When viewed along strike in depth section (Figure 9 and Figure 12), it can be seen that a steeply dipping structure is defined (dip ~ 87°) that is defined most sharply on its southwesterly side.

These results suggest that the stimulation activated a northwesterly trending fault ~ 250 m in length. Two portions of the fault plane separated in depth were activated. The shallower one extends



throughout approximately the lower 250 m of the borehole and the other is approximately 100 m in height, with its top about 200 m below the bottom of the well.

More work needs to be done to fine-tune and study in detail these dimensions and depths and this will comprise our work in the forthcoming week. Numerical data for these interim results have been provided to AltaRock by email attachment to Trenton Cladouhos.

5 Task 5 Moment tensor calculations

Moment tensors were derived for an additional 10 earthquakes using the same procedure as described in Weekly Report #1. The numerical results of the catalog to date are given in

Table 2. Graphical results for the additional events are shown in Appendix 1.

The source types for the entire 34-event set are shown in source-type space in Figure 13. The events form a distribution from the +Dipole to the -Dipole points, indicating a mixture of crack-opening and crack-closing events in approximately equal numbers.

Figure 14 shows a plot of the P-, T- and I-axes, approximately corresponding to the directions of σ_1 , σ_3 and σ_2 . The addition of more earthquakes has strengthened the distribution seen earlier whereby most T axes cluster systematically subhorizontally and to the S \pm 20° or so. The orientations of the P- and I-axes are more scattered.

NN	NE	EE	ND	ED	DD	Yea	М	Da	H	mi	Sec	Quality
						r	0	У	r	n		
1.578e-	3.466e-	6.671e-	2.482e-	6.317e-	8.338e-	201	1	01	1	53	05.23	excelle
01	02	02	01	02	02	4	0		4			nt
2.172e-	-3.673e-	-6.417e-	2.346e-	7.204e-	3.184e-	201	1	01	1	05	16.54	excelle
01	02	02	01	02	02	4	0		9			nt
8.713e-	1.262e-	-4.193e-	1.814e-	8.429e-	8.722e-	201	1	04	1	51	12.00	excelle
02	01	02	01	02	02	4	0		8			nt
-1.029e-	1.325e-	-1.185e-	1.480e-	5.508e-	1.074e-	201	1	04	1	32	52.76	excelle
01	01	01	01	02	01	4	0		7			nt
-1.165e-	1.705e-	-1.989e-	1.394e-	-2.430e-	1.639e-	201	1	02	0	07	04.16	excelle
01	01	01	01	02	02	4	0		7			nt
2.406e-	-7.298e-	-9.789e-	1.731e-	4.297e-	8.349e-	201	1	02	1	01	42.38	excelle
01	02	02	01	02	02	4	0		1			nt
-1.461e-	9.643e-	-3.978e-	2.595e-	1.691e-	-4.693e-	201	1	02	0	47	52.94	excelle
02	02	01	02	01	03	4	0		6			nt
6.066e-	-2.231e-	-9.157e-	1.941e-	3.367e-	-6.184e-	201	1	03	0	06	22.76	excelle
03	01	02	01	02	04	4	0		6			nt
-5.772e-	-1.655e-	-1.427e-	1.464e-	7.811e-	-1.952e-	201	1	03	1	54	53.93	fair
02	01	01	01	02	02	4	0		8			
2.004e-	-1.410e-	-1.461e-	1.400e-	-8.713e-	7.412e-	201	1	01	1	03	16.94	good
01	01	01	01	03	02	4	0		2			
5.304e-	6.783e-	-1.175e-	1.615e-	7.508e-	2.206e-	201	1	05	0	07	20	excelle
02	02	01	01	02	01	4	0		4			nt
-1.777e-	-1.053e-	-1.512e-	7.111e-	1.063e-	1.057e-	201	1	01	0	03	14.49	excelle
01	01	01	02	01	01	4	0		1			nt
-2.667e-	1.320e-	-6.399e-	6.063e-	1.031e-	7.787e-	201	0	30	2	30	43.50	excelle
01	01	02	02	01	02	4	9		1		3	nt

Table 2: Numerical moment tensor results for the 34 MEQs studied to date. N=North, E=East, D=Down.



-1.871e-	8.995e-	-9.473e-	-1.446e-	-2.491e-	1.992e-	201	1	05	2	22	16.49	good
01	02	02	01	02	01	4	0		3		9	
1.684e-	-3.350e-	-9.826e-	2.952e-	3.542e-	9.350e-	201	1	04	0	29	08.25	fair
01	02	03	01	02	02	4	0		5		8	
2.449e-	-8.111e-	-1.972e-	1.741e-	1.624e-	1.507e-	201	1	03	1	27	57.66	good
01	02	01	01	02	02	4	0		5		1	
-2.209e-	-8.132e-	-2.190e-	-1.520e-	3.521e-	2.201e-	201	1	01	1	56	11.34	good
01	02	02	01	02	01	4	0		6		3	
1.477e-	-1.175e-	-1.492e-	1.577e-	-3.130e-	9.546e-	201	1	01	0	08	57.99	excelle
01	01	01	01	02	02	4	0		8		8	nt
-3.263e-	2.220e-	-3.373e-	1.644e-	7.162e-	9.879e-	201	1	01	1	50	55.10	excelle
02	01	01	02	02	03	4	0		0		7	nt
-1.038e-	1.463e-	-2.541e-	1.246e-	-1.332e-	7.335e-	201	1	01	1	01	54.95	excelle
01	01	01	01	02	02	4	0		5		0	nt
2.306e-	-1.802e-	-9.214e-	2.203e-	-4.354e-	9.593e-	201	1	02	1	54	03.15	dood
03	01	02	01	03	02	4	0		8		2	5
1.619e-	4.200e-	-2.041e-	2.158e-	-2.044e-	7.759e-	201	1	02	0	39	02.99	excelle
01	02	01	01	02	02	4	0		6		8	nt
-6.570e-	-1.851e-	-1.140e-	1.691e-	4.183e-	2.826e-	201	1	02	1	39	24.31	dood
02	01	01	01	02	02	4	0		2		7	5
1.420e-	-1.373e-	-1.638e-	1.721e-	1.076e-	5.384e-	201	1	02	2	37	06.04	dood
01	01	01	01	02	02	4	0		0		3	2
-1.365e-	-1.837e-	-5.911e-	1.611e-	-1.124e-	9.224e-	201	1	05	0	06	16.96	excelle
01	01	02	01	02	02	4	0		2		7	nt
2.866e-	-3.707e-	-1.787e-	9.263e-	1.263e-	2.268e-	201	1	05	1	07	32.77	excelle
01	02	01	02	01	02	4	0		6		7	nt
-2.286e-	1.607e-	-7.209e-	-9.281e-	8.007e-	-3.216e-	201	1	05	1	55	21.00	dood
01	01	02	02	02	02	4	0		5		7	2
-1.352e-	-1.174e-	-4.098e-	1.996e-	-5.345e-	8.302e-	201	1	12	1	12	29	doop
01	01	02	01	02	02	4	0		0			2
-2.211e-	1.542e-	4.959e-	9.042e-	8.191e-	7.603e-	201	1	12	2	10	23.31	doop
01	01	02	02	02	02	4	0		1		1	J
-4.882e-	-1.017e-	5.620e-	5.965e-	-1.844e-	1.292e-	201	1	12	1	37	43.28	excelle
01	01	02	02	03	01	4	0		6	• • •	7	nt
-5.873e-	-1.252e-	-2.804e-	6.116e-	1.409e-	6.331e-	201	1	13	0	57	06.71	boop
02	01	01	02	01	03	4	0	10	0		7	yoou
2.607e-	-1.181e-	-2.888e-	8.025e-	1.234e-	4.154e-	201	1	13	õ	12	29.12	excelle
02	01	01	02	01	02	4	0	10	4		6	nt
-1.162e-	-1.387e-	-1.174e-	1.514e-	5.536e-	7.558e-	201	1	13	1	22	29.08	excelle
01	01	01	01	02	02	4	0	10	Ô		4	nt
_1.128e-	-2.729e-	-2.406e-	5.661e-	5.175e-	3.7530-	201	1	14	õ	46	13.91	exellen
01	02	01	02	02	01	4	0		5	10	4	t
~ -	~ -	~ -	~ -	~ -	~ -	-	-		-		-	-



Figure 13: Source-type plot showing the earthquakes for which moment tensors have been derived to date.



Figure 14: Plot of pressure $(P \sim \sigma_1)$ and tension $(T \sim \sigma_3)$ and intermediate $(I \sim \sigma_2)$ axes for the 34 earthquakes for which moment tensors have been derived to date.



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Appendix 1: The additional nine moment tensors derived over the reporting week.



Image Image <t< th=""><th>00</th><th>)</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>/Use</th><th>rs/foulger/Seisr</th><th>nicProcessin</th><th>/Nev</th><th>wberry/Data/2014/10/0</th><th></th><th>141005160722.or</th><th></th></t<>	00)								/Use	rs/foulger/Seisr	nicProcessin	/Nev	wberry/Data/2014/10/0		141005160722.or	
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Sta Dist Az I Cha Phase Resid Polarity Penalty Arpo Peea 1 NM03 2.55 10 121 N P 0.029 9 + Ø 2.58e-01 2.16e-01 3 MM22 0.11 198 177 EHU P 0.003 Ø 4 Ø 1.50e-02 1.98e-01 1.98e-01 <td></td> <td>Scalar M0 = 2.885e-01</td> <td></td> <td></td> <td>Dipole</td>														Scalar M0 = 2.885e-01			Dipole
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Image Image <thimage< th=""> <thimage< th=""> <thim< td=""><td>1</td><td>NM03</td><td>2.95</td><td>10</td><td>121</td><td>EHU</td><td>Р</td><td>0.029</td><td>V +</td><td></td><td>2.58e+01</td><td>2.16e+01</td><td></td><td>Total Penalty = 0.174</td><td></td><td></td><td>-V</td></thim<></thimage<></thimage<>	1	NM03	2.95	10	121	EHU	Р	0.029	V +		2.58e+01	2.16e+01		Total Penalty = 0.174			-V
INA22 0.1 19 17 ENU P -0.03 Ø W Ø 138e401 INA22 0.11 199 17 ENU P -0.03 Ø W Ø 138e401 INA42 380 41 115 ENU P -0.001 Ø Ø 0.0620 1.17e401 INA42 380 41 115 ENU P -0.005 - Ø 4.86e401 1.71e401 INA42 380 41 115 ENU P -0.005 - Ø 4.86e401 1.71e401 INA00 2.08 22 131 BNT ENU P -0.002 · Ø 1.86e401 1.98e101 INN0 2.08 22 134 ENU P 0.000 · Ø 4.18e402 1.75e401 I NN18 136 22 146 ENU P 0.001 Ø 2.88e401 1.98e	2	NM06	0.70	105	162	EHR	SV	0.123	⊻ +		✓ 1.50e+02	1.09e+01					
I NA22 0.11 199 17 EHH SV 0.000 I I 0.004e01 1.71e401 S NA42 380 41 115 EHH SV 0.0029 I I I.71e401 NM42 380 41 115 EHH SV 0.0029 I I.71e401 I.71e401 NM42 380 41 115 EHT SH 0.002 I I.148e402 1.71e401 NM07 3.11 383 117 EHT SH 0.002 I I.448e402 1.77e401 10 NM08 2.09 222 131 EHT SH 0.002 I I.48e402 1.77e401 12 NM08 2.09 222 131 EHT SH 0.008 I I.0004 I.77e401 13 NN17 1.85 248 140 EHT SH 0.008 I.62e401 I.89e401 1 NM42 I.95V I I.000 I.62e401 I.82e401 1 <td< td=""><td>3</td><td>NM22</td><td>0.11</td><td>199</td><td>1/7</td><td>EHU</td><td>P</td><td>-0.003</td><td>✓ +</td><td></td><td>✓ 1.35e+02</td><td>1.54e+01</td><td></td><td></td><td></td><td>POLARITIES</td><td></td></td<>	3	NM22	0.11	199	1/7	EHU	P	-0.003	✓ +		✓ 1.35e+02	1.54e+01				POLARITIES	
5 NVM42 0.00 - V 0.00 V	4	NM22	3.60	199	115	EHR	SV	-0.001	+		✓ 1.08e+03	1.04e+01					
6 NM42 0.00 1 0 4.884102 1.176401 8 NN07 311 335 117 EHT SH 0.005 - 0 4.884102 1.176401 9 NN07 311 335 117 EHU P 0.005 - 0 1.884102 1.176401 10 NN07 311 335 117 EHT SH 0.002 - 0 1.484102 1.986401 2.016401 11 NN08 2.09 222 131 EHT SH 0.004 + 0 3.546402 1.916401 12 NN09 2.09 222 131 EHT SH 0.004 + 0 3.546402 1.916401 13 NN17 1.56 244 EHU P 0.010 - 2.288401 1.996401 1 1.896401 1 NM42 Ø P.SV 1 0.80411 1.828401 1.828401 1.828401 1.828401 1.828401 1.828401 1 NM42	5	NM42	3.60	41	115	EHU	P	0.029	<u> </u>		✓ -6.80e+01	1./10+01					
Inverte Invert Inverte Inverte	6	NM42	3.60	41	115	EHT	SH	0.075	<u> </u>		✓ -4.580+02	1.17e+01		P .			34
B NN07 11 335 117 EH SI Output Image: Signature state sta	/	NN07	3.11	335	117	EHU	P	-0.005	• -		✓ -1.040+03	1.176+01			\setminus		
I NN0 209 292 131 EHU P 0.002 Ø Ø Saget0 2.016401 11 NN09 2.09 292 131 EHT SH 0.044 Ø 4 Ø 5.898+01 2.016401 11 NN09 2.09 292 131 EHT SH 0.044 Ø Ø 1.038+01 2.758+01 13 NN17 1.65 244 HU P 0.010 Ø I Ø 3.548+02 1.918+01 14 NN18 1.38 22 146 EHU P 0.010 Ø I Ø 3.548+02 1.918+01 1 NM42 Ø P.SV I NM42 Ø SV.SH I I I.0200 Ø I.0300 Ø A.011 1.828+01 I.2010	0	NN07	3.11	335	117	EHT	SH	0.002	0-		✓ -1.48e+02	1.99e+01		[[-] [*] → [*]	+		(+)
11 NN09 209 292 131 EHR SV -0.003 + - 4.16e+02 1.75e+01 12 NN09 2.02 222 131 EHT SH 0.040 ////.4 - 3.54e+02 1.91e+01 13 NN17 1.85 248 140 EHU P 0.001 ///.4 //.4.36e+02 1.91e+01 14 NN18 1.36 22 146 EHU P 0.010 //.4 //.2.28e+01 1.99e+01 1 NM42 //.P.SV 1 3.0 //.4 9.5V 1 1.80e+01 1.82e+01 1.82e+01 1 NM42 //.P.SV 1 3.0 //.4 9.5V 1 1.000 //.4 1.82e+01 1.82e+01 1.82e+01 1 NM42 //.P.SV 1 3.0 //.4 9.5V.5 1 1.000 //.4 1.82e+01 1.82e+01 1.82e+01 1 NM42 //.P.SV 1 9.5V.5 1 1.000 1.6 1.600 1.6 1.	10	NN09	2.09	292	131	EHU	P	0.002	√ +		✓ 5.89e+01	2.01e+01			/	(• /	$\langle \langle \cdots \rangle$
12 NN09 208 292 131 EHT SH 0.040 Ø + Ø 3.546+02 1.91e+01 13 NN17 1.65 224 140 EHU P 0.010 Ø + Ø 1.03e+01 2.77e+01 14 NN18 1.36 22 146 EHU P 0.010 Ø - Ø -2.88e+01 1.99e+01 1 NM42 Ø PSV 1 NM42 Ø PSV 1 NM42 Ø PSV 1 NM42 Ø PSV 0.038 Ø + 0.030 Ø R 81a+01 1.82e+01 1 8.248 1 9.9401 1 8.248 1 1.99e+01 1 1.92e+01 1 1 1.92e+01 1	11	NN09	2.09	292	131	EHR	sv	-0.003	- +		✓ 4.16e+02	1.75e+01					
13 NN17 1.65 2.48 140 EHU P 0.001 Ø + Ø 1.03e+01 2.77e+01 14 NN18 1.38 22 1.46 EHU P 0.011 Ø - Ø 2.288e+01 1.99e+01 1 NN18 1.38 22 1.46 EHU P 0.018 Ø 2.88e+01 1.99e+01 1 NM42 Ø P.SV Image: Stress of the stres stress of the stress of the stress of the	12	NN09	2.09	292	131	EHT	SH	0.040	√ +		3.54e+02	1.91e+01					\square
14 NN18 1.36 22 146 PHU P -0.010 Image: second	13	NN17	1.65	248	140	EHU	Р	0.001	v +		✓ 1.03e+01	2.77e+01					
ive NM18 1.38 22 146 FHR SV -0.038 Ø + 0.030 Ø R 916±01 1.826±01 1 NM42 Ø PSV 2 N42 Ø PSV - - - +<	14	NN18	1.36	22	146	EHU	Р	-0.010	I -		✓ -2.88e+01	1.99e+01				SN	SE
Sta Type Penalty 1 NM42 Ø PSV 2 NM42 Ø PSV 3 NM42 Ø SVSH 4 N07 PSH 5 N09 Ø PSH 6 N09 Ø PSH 7 N09 Ø SVSH 8 N18 PSV 9 N18 PSV 9 N18 PSV 10 N18 Ø PSH 11 N19 Ø PSH 12 N19 Ø PSH 13 N19 Ø VSH 14 N191 PSV 14 N191 PSV	10	NN18	1.36	22	146	FHR	sv	-0.038	J +	0.030	Ø 891e+01	1 62e+01					
1 NM42 V PsV 2 NM42 V PsH 3 NM42 V PsH 4 NN07 PsH 5 NN09 V PsH 6 NN09 V PsH 7 NN09 V PsH 8 N18 PsV PsH 10 N18 VSH 0.085 11 N19 PsH PsH 13 N19 SVSH 0.085 13 N19 PsV PsV 14 N21 PsV PsV		Sta	Тур	e	Penalty	1										(- '+ º-)	(+ '+ º-)
2 NM42 Ø PSH 3 NM42 Ø SVSH 4 NN07 PSH 5 NN09 Ø PSH 6 NN09 Ø PSH 7 NN09 Ø SVSH 8 NN18 PSH 9 NN18 PSH 10 NN18 Ø SVSH 11 NN19 Ø PSH 12 NN19 Ø PSH 13 NN19 Ø SVSH 14 NN21 PSV 14 NN21 PSV	1	NM42	🗹 P:	sv													
3 NM42 M SVSH 4 N07 PSH 5 N09 M PSV 6 N09 M PSH 7 N09 M PSH 8 NN18 PSV 9 NN18 PSH 10 NN18 M SVSH 12 NN19 PSV 13 NN19 PSV 14 NN21 PSV 14 NN21 PSV	2	NM42	✓ P:	SH		_											
4 NNUV PSH 5 NN09 PSV 6 NN09 PSH 7 NN09 PSH 7 NN09 SV:SH 8 NN18 PSV 9 NN18 PSH 10 NN18 PSH 11 NN19 PSH 12 NN19 PSH 13 NN19 PSV 14 NN21 PSV 12 PSV 13 PSH	3	NM42	✓ s\	SH:		_											\smile
5 NV09 V F-SV 6 NV09 V PSH 7 NV09 V PSH 8 NV18 PSV 9 NV18 PSH 10 NV18 VSVSH 9 SVSH 0.085 11 NV19 PSH 12 NV19 PSH 13 NV19 PSV 14 NV21 PSV 14 NV21 PSV	4	NN07	P:	SH		_											
0 NV09 Ø F-sh 7 NV09 Ø SVSH 8 NN18 PSV 9 NN18 PSH 10 NN18 PSH 12 NN19 PSH 13 NN19 SVSH 14 NN21 PSV 12 NN19 PSV	5	NN09	P3	50		_										AMPLITUDE RATIOS	
NN18 PSV 9 NN18 PSV 9 NN18 PSH 10 NN18 PSV 12 NN19 PSV 13 NN19 PSV 14 NN21 PSV	6	NN09				-											
8 MINIS P.S.L 9 NNIS P.S.L 10 NNIS VSNH 11 NNI9 P.S.V 12 NNI9 P.S.V 14 NN21 P.S.V	0	NN18	P:	sv		-								AAR		ARBA	
10 NN18 ✓ SV:SH 0.085 11 NN19 P:SV 12 12 NN19 ✓ P:SH 13 13 NN19 P:SV 14 NN21 P:SV	9	NN18	- P:	SH		-								PISH		P:S	SV:SH 1
11 NN19 P.SV 12 NN19 SVSH 13 NN19 SVSH 14 NN21 P.SV 12 NN19 SVSH	10	NN18	√ sv	SH	0.085	-									\backslash		$(, \langle \rangle)$
12 NN19 Ø P.SH 13 NN19 SV.SH 14 NN21 P.SV 17 NN21 P.SV	11	NN19	P:	SV		-									A		
13 NN19 SV.SH 14 NN21 P.SV 15 NN21 P.SV 16 NN21 P.SV	12	NN19	✓ P:	ы		-									夙		A Second Second
14 NN21 PSV 15 NN21 PSH	13	NN19	S S	:SH		-									50		
TT NN21 P:SH	14	NN21	P:	SV		1											N South
	10	NN21	□ P:	SH		1											



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20 Lat	4 Oct 5 43.726 43:43.	15:55: 1 Lon 5666 N	21.007 -121 123	UTC .308 L:18.4	Depth: 71 W	1.111				Solve	
	Sta	Dist	Az	i	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq
1	NM03	2.95	9	124	EHU	Р	0.015	I -			
2	NM22	0.13	222	177	EHR	sv	0.083	√ +			
3	NM42	3.57	40	118	EHU	Р	-0.003	I -	0.005	✓ -3.16e+01	1.24e+01
4	NM42	3.57	40	118	EHR	sv	0.032	I -		-1.76e+02	1.08e+01
5	NM42	3.57	40	118	EHT	SH	0.063	₫-	0.036	✓ -2.83e+02	1.02e+01
6	NN07	3.14	334	119	EHU	P	-0.006	v -		-1.22e+01	1.66e+01
7	NN07	3.14	202	120	EHT	SH	-0.008	⊻ -	0.017	✓ -5.21e+01	1.96e+01
8	NN09	2.14	292	133	EHU	P	-0.019	✓ +	0.016	✓ 1.36e+01	2.11e+01
9	NN09	2.14	292	133	EHR	51	0.021	• +		▼ 1.08e+02	2.260+01
10	NN17	1.69	249	141	EHU	P	0.000			3 75e+00	3.01e+01
11	NN17	1.69	249	141	EHT	SH	-0.016	▼ +		3.05e+01	2.03e+01
12	NN18	1.36	20	148	EHU	P	-0.001	v -	0.001	✓ -2.55e+00	2.23e+01
14	NN18	1.36	20	148	EHR	sv	-0.009	<u>-</u>	0.007	✓ -1.57e+02	1.16e+01
10	NN18	1.36	20	148	FHT	SH	-0.039	J -	0.001	√ -2 16e+01	2 16e+01
	Sta	Ту	e	Penalty	y						
1	NM42	🗹 Р	sv	0.005							
2	NM42	🗹 Р	SH	0.015							
3	NM42	🗹 s	V:SH	0.025							
4	NN07	P	SH								
5	NN09	P	sv		_						
6	NN09	P	SH		_						
7	NN09	S S	V:SH		_						
8	NN17		5H 6V		_						
9	NN18	J P	SH SH		-						
10	NN18	J s	V:SH		-						
12	NN19	S S	V:SH		-						
13	NN21	√ P	sv		-						
14	NN21	- P	SH		-						
10	NN21	J s	/·SH	0 045							



00									/Usei	rs/foulger/Seisn	nicProcessir	g/Newberry/Data/2014/10/12/20	141012101229.or	
Ø		2	N ?											
2014 Lat:	Oct 12 43.726 43:43.6	2 10:12: 8 Lon: 5104 N	29.63 -121 12	2 UTC 311 1:18.66	Depth: 56 W	0.483				Solve		North East North -1.35e-01 -1.17e-01 East -1.17e-01 -4.10e-02 Down 2.00e-01 -5.34e-02	Down 2.00e-01 -5.34e-02 8.30e-02	+Cra+++++++++++++++++++++++++++++++++++
	S+2	Dict	A -7		Chan	Phare	Porid	Polarity	Banalty	Amo	From	$T = -0.188 \ k = -0.102$		Crack
1.1	IM03	2.92	14	108	EHU	P	0.012	V -	renarcy	✓ -6.62e+00	2.51e+01	Tatal Baralta 0.110		
2 1	IM03	2.92	14	108	EHB	sv	0.016			2.68e+02	1.71e+01	Total Penalty = 0.119		
3	IM06	0.92	106	151	EHU	P	0.023	√ +		✓ 1.61e+02	1.40e+01			
4	IM06	0.92	106	151	EHT	SH	0.059	√ +		✓ 3.58e+02	1.62e+01		POLARINES	
S M	IM22	0.25	136	172	EHU	P	-0.018	√ +		✓ 1.92e+02	1.42e+01			
6 1	IM42	3.69	44	101	EHU	P	-0.008	I -		✓ -5.75e+01	2.45e+01	P Colo	SH	SV
7	IN07	2.96	338	105	EHU	Р	0.003	I -		✓ -3.17e+01	1.37e+01			
8	IN07	2.96	338	105	EHT	SH	0.007	I -		✓ -1.28e+02	1.80e+01		$(\cdot (\cdot \cdot))$	
9 1	IN09	1.87	292	123	EHZ	Р	0.010							
10	IN09	1.87	292	123	EHR	SV	-0.018	√ +	0.025	✓ 1.66e+02	1.58e+01	· · · · /		
11	IN09	1.87	292	123	EHT	SH	0.041	🗹 +	0.046	✓ 1.11e+02	3.55e+01			
12	IN17	1.49	243	132	EHU	Р	-0.004	√ +	0.006	✓ 6.53e+00	2.36e+01		\cup	\cup
13	IN17	1.49	243	132	EHR	SV	0.049	- 🗌		✓ -7.09e+02	8.92e+00			
14	IN17	1.49	243	132	EHT	SH	0.018	I -		✓ -3.24e+02	1.19e+01		SN	SE P
10 1	IN18	1.40	31	136	FHU	P	-0.004	J -	1	✓ -6 93e±01	1 74e+01			
	Sta	Тур	e	Penalty	r								(- + -)	(+ + -)
1	IM03	P:	sv											
2	IM06	P:	SH											
3	IN07	✓ P:	SH		_									
4	IN09	√ s\	/:SH	0.029	_									
5	IN17	P:	sv		_								AMPLITUDE RATIOS	
6	IN17	✓ P:	SH	0.012	_									
7	IN17	S\	/:SH		_									
8	IN18	P3	57		-							PSH	P:SY PIG	SV:SH
9	10110	P:	ori veu		-							Constant of	Franker	
10	INITO		7.5H		-								El San San	
11	IN 19		20		-									
12	IN24	P3 	SV SV		-							Contraction of the second s	NE STAT	V SSSS V
13	IN32		sv									Kets	Not and	CP 9 P I
10 1	IN32	J P	SH									VBBC	108	



0 0 0 /Users/fo	oulger/SeismicProcessing	/Newberry/Data/2014/10/12/2	0141012211019.or	
2014 Oct 12 21:10:23.311 UTC Lat: 43.7274 Lon: -121.311 Depth: 0.467 43:43.647 N 121:18.6408 W	olve	North East North -2.21e-01 1.54e-02 East 1.54e-01 4.96e-02 Down 9.04e-02 8.19e-02 Scalar M0 = 2.593e-01	Down 1 9.04e-02 8.19e-02 2 7.60e-02	+Crart +Diport +CLV
Sta Dist Az i Chan Phase Resid Polarity Penalty	Amp Freq	T = 0.154 k = -0.107		Crack
1 NM06 0.91 111 151 EHU P 0.039 √ +	1.97e+02 1.82e+01	Tatal Paralty 0.171		<u> </u>
2 NM06 0.91 111 151 EHT SH 0.055 V +	355e+02 119e+01	Total Penalty = 0.171		
2 NM22 0.28 151 171 EHU P -0.023 V -	3.470+02 1.500+01			
	1.160.02 1.000+01		POLARITIES	
	-1.10e+03 1.0/e+01			
5 NM42 2.91 336 105 FHH D 0.013 -	-2.040+02 1.400+01			
6 NN07 2.31 336 105 EHU P 0.515 V -	-2.46e+01 1.55e+01	P 8	SH	SV P
7 NN07 2.51 330 103 EHT SH 0.510 V -	-1.29e+02 1.19e+01		$(\setminus \cdot , \lambda)$	
8 NN09 1.87 290 122 EHU P 0.018 V +	2.43e+00 3.16e+01			
9 NN09 1.87 290 122 EHR SV 0.007 V +	1.06e+02 2.64e+01			
10 NN09 1.87 290 122 EHT SH 0.034 +	1.17e+02 3.13e+01			
11 NN17 1.55 241 130 EHU P -0.011 V +	7.24e+00 3.42e+01			
12 NN17 1.55 241 130 EHR SV 0.022 V -	-7.16e+02 1.64e+01			
13 NN17 1.55 241 130 EHT SH 0.003 V -	-3.67e+02 1.31e+01			77
14 NN18 1.32 31 137 EHU P -0.019 +	1.38e+01 2.68e+01			SE P
10 NN18 1.32 31 137 FHR SV 0.005	I -5 04e+02 1 09e+01			
Sta Type Penalty			+ + + -	+++
			\т'/	\ T ' /
3 NN07 P.SH				
4 ININO F.SV 0.004				
			AMPLITUDE RATIOS	
7 NN1/ P'SV				
8 NN17 P:SH		D.CU	D.CV	CV/CL
9 NN17 SV:SH 0.000		P.SP	P.SV	SV. SR ANSA
10 NN18 P:SV 0.077		ALL SAL		LE STREET
11 NN18 P:SH				
12 NN18 SV:SH		The second		
13 NN21 V P:SH 0.005				15385
14 NN24 V P:SV 0.025				X
		-84v	19 4. v	



2.92

3.64

SV:SH

P:SH P:SV P:SH

SV:SH 13 NN19 V P:SV 0.016 14 NN21 ✓ P:SV 16 NN24 P:SV

0.038

2 NM03

3 NM06

4 NM06

5 NM22

8 NM42

9 NM42

10 NN07

11 NN07

12 NN09

13 NN09

14 NN09

1c NN17 Sta

1 NM03

2 NM06

3 NM41 4 NM42

5 NN07

6 NN09

7 NN09 8 NN09

9 NN17 10 NN18 11 NN18 12 NN18



P:SV

SV-SH

P:SH









None North Est															
Image Image <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>/User</td><td>s/foulger/Seisn</td><td>nicProcessin</td><td>g/Ne</td><td>ewberry/Data/2014/10/13/2</td><td>0141013041229.or</td><td></td></th<>									/User	s/foulger/Seisn	nicProcessin	g/Ne	ewberry/Data/2014/10/13/2	0141013041229.or	
2014 Oct 13 4:12:29:126 UTC 4: 43:265 Dox - 121:13: 0 Depth: 0.795	0 🖥] 🎍	k?												
Sta Dist Az I Chan Pasa Resid Polarity Panaly Amp Test 1 NM02 2.94 12 117 HU P 0.001 U - U 1.922-012 <td< td=""><td>2014 Oct Lat: 43.7 43:4</td><td>13 4:12: 265 Lon: 3.5906 N</td><td>29.126 : -121 12:</td><td>UTC 31 D 1:18.60</td><td>epth: ()72 W</td><td>0.795</td><td></td><td></td><td></td><td>Solve</td><td></td><td></td><td>North East North 2.61e-02 -1.18e-0 East -1.18e-01 -2.89e-0 Down 8.03e-02 1.23e-0 Scalar M0 = 2.802e-01</td><td>Down 1 8.03e-02 1 1.23e-01 1 4.15e-02</td><td>+Crav +Dipple +Cly</td></td<>	2014 Oct Lat: 43.7 43:4	13 4:12: 265 Lon: 3.5906 N	29.126 : -121 12:	UTC 31 D 1:18.60	epth: ()72 W	0.795				Solve			North East North 2.61e-02 -1.18e-0 East -1.18e-01 -2.89e-0 Down 8.03e-02 1.23e-0 Scalar M0 = 2.802e-01	Down 1 8.03e-02 1 1.23e-01 1 4.15e-02	+Crav +Dipple +Cly
1 NM00 244 17 EHU P 0.001 Ø Ø Ø Ø 1.82e-01 2.01e-01 2 NM22 0.11 147 175 EHU P 0.000 Ø Ø Ø 1.82e-001 2.01e-01 4 NM22 0.17 147 175 EHT SH 0.015 Ø 4 Ø 2.01e-01 1.52e+02 1.58e+01 1.56e+01 1.52e+02 1.04e+01 56e+01 1.52e+02 1.04e+01 50e+01 1.52e+02 1.52e+02 1.04e+01 50e+01 1.52e+02 1.04e+01 50e+01 1.52e+02 1.5	Sta	Dist	Az	i	Chan	Phase	Resid	Polarity	Penalty	Amp	Freq		$T = 0.755 \ k = -0.196$		Crack
2 NM22 0.17 147 175 EHU P 0.088 \vec{H} \vec{M} 5.10e-02 1.46e-01 3 NA22 0.17 147 175 EHR SV 0.086 \vec{M} \vec{M} 2.33e-03 9.24e-00 5 NA42 3.86 43 110 EHR SV 0.051 \vec{M} \vec{M} 2.13e-02 1.38e-03 1.56e-01 6 NA42 3.86 43 110 EHR SV 0.052 \vec{M} 3.25e-02 1.33e-01 6 NN07 3.03 3.36 114 EHT SH 0.044 \vec{M} 0.055 \vec{M} 3.25e-01 1.04e-10 10 NN07 3.38 114 EHT SH 0.045 \vec{M} 1.05e-01 1.59e-01 . SH \vec{U} \vec{U} \vec{U} . S \vec{U} . S S . S S . . S S . . S S .	1 NM03	2.94	12	117	EHU	P	0.001	I -	. enarcy	✓ -1.92e+01	2.01e+01	11	Total Penalty = 0.189		~
3 NM22 0.77 147 175 EHR SV 0.034 Ø I Ø 238-03 9.24+00 4 NM22 0.077 147 175 EHR SV 0.008 Ø I.50e-01 1.50e-01 6 NM42 366 43 100 EHH SV 0.007 Ø Ø I.52e-02 1.50e-01 7 NM42 386 44 100 EHH SV 0.007 Ø Ø I.52e-02 1.50e-01 7 NM42 386 144 110 EHH SV 0.004 Ø 0.001 Ø I.52e-02 1.50e-01 8 NN07 338 114 EHH P 0.004 Ø 0.025 Ø 3.26e-01 2.68e-01	2 NM22	0.17	147	175	EHU	Р	-0.008	√ +		✓ 5.10e+02	1.46e+01		Total reliaity = 0.105		
4 MM22 0.17 147 175 EHT SH 0.015 Ø I IS6e+01 IS6e+01 <td>3 NM22</td> <td>0.17</td> <td>147</td> <td>175</td> <td>EHR</td> <td>sv</td> <td>0.054</td> <td>√ +</td> <td></td> <td>✓ 2.33e+03</td> <td>9.24e+00</td> <td></td> <td></td> <td>POLABITIES</td> <td></td>	3 NM22	0.17	147	175	EHR	sv	0.054	√ +		✓ 2.33e+03	9.24e+00			POLABITIES	
S NM42 366 43 10 EHU P 0.000 I I 1.52e402 1.33e401 6 NM42 366 43 100 EHT S 0.024 I I 9.32e402 1.04e401 7 NM42 366 43 110 EHT SH 0.024 I SS55402 1.06e01 9 NN07 303 336 114 EHU P 0.001 I I SS55402 1.06e01 10 NN09 1.95 292 130 EHT SH 0.025 I I J2ee10 Z SS I	4 NM22	0.17	147	175	EHT	SH	0.015	v +		✓ 1.25e+03	1.56e+01				
6 M42 3.66 43 110 EHR SV 0.057 \$\vee\$ -	5 NM42	3.66	43	110	EHU	Р	0.009	v -		✓ -1.52e+02	1.33e+01	1			
7 NM42 3.66 43 110 EHT SH 0.024 + ✓ 55.5602 1.06e+01 8 NN07 303 336 114 EHU P 0.004 ✓ - 0.041 ✓ 1.18e+02 1.58e+01 10 NN09 1.95 292 130 EHU P 0.010 ✓ ✓ Ø 9.82e+00 2.63e+01 11 NN09 1.95 292 130 EHT SH 0.025 ✓ 1.08e+01 V V Ø 3.22e+01 2.63e+01 12 NN09 1.95 292 130 EHT SH 0.025 ✓ Ø 3.22e+01 2.63e+01 V V V 0.85e+02 1.98e+01 V V V 0.85e+02 1.98e+01 V V V V V V V V V V V V V V V V V	6 NM42	3.66	43	110	EHR	sv	0.057	I -		✓ -9.23e+02	1.04e+01		P	SH	SV
8 NN07 3.08 3.36 114 EHU P 0.004 Image: descent to the state of the	7 NM42	3.66	43	110	EHT	SH	-0.024	- +		✓ 5.55e+02	1.06e+01				
9 NN07 3.03 336 114 EHT SH 0.046 Ø 4 0.025 Ø 4.32e+02 1.08e+01 10 NN09 1.95 292 130 EHU P 0.010 Ø # Ø 9.2e+00 2.63e+01 12 NN09 1.95 292 130 EHT SH 0.025 Ø # Ø 1.08e+01 12 NN09 1.95 292 130 EHT SH 0.025 Ø # Ø 3.2e+01 2.49e+01 13 NN17 1.54 245 138 EHT SH 0.025 Ø # Ø 3.86e+02 1.95e+01 1 NM42 PSV 38 FHT SH 0.007 Ø S N Ø N O N Ø A N N Ø N O N Ø N O N Ø N	8 NN07	3.03	336	114	EHU	Р	0.004	I -	0.041	🗹 -1.18e+02	1.59e+01	1	(• ° ° °)	(•) <u>•</u>	(• Ň•))
10 NN09 1.95 292 130 EHU P 0.010 \$\vee{T}\$ + \$\vee{T}\$ 9.92e+00 2.63e+01 11 NN09 1.95 292 130 EHR SV -0012 \$\vee{T}\$ + \$\vee{T}\$ 1.72e+01 12 NN09 1.95 292 130 EHR SV -0012 \$\vee{T}\$ + \$\vee{T}\$ 1.72e+01 1.51e+01 12 NN07 1.54 245 138 EHR SV 0.028 \$\vee{T}\$ + \$\vee{T}\$ 3.66e+02 1.95e+01 14 NN17 1.54 245 138 EHR SV 0.028 \$\vee{T}\$ + \$\vee{T}\$ 3.66e+02 1.95e+01 14 NM42 PSV 0.037 \$\vee{T}\$ + \$\vee{T}\$ 3.66e+02 1.95e+01 \$\vee{T}\$ 4.201 \$\vee{T}\$ 4.201 <t< td=""><td>9 NN07</td><td>3.03</td><td>336</td><td>114</td><td>EHT</td><td>SH</td><td>0.046</td><td>🗹 +</td><td>0.025</td><td>✓ 4.32e+02</td><td>1.08e+01</td><td></td><td></td><td></td><td></td></t<>	9 NN07	3.03	336	114	EHT	SH	0.046	🗹 +	0.025	✓ 4.32e+02	1.08e+01				
11 NN09 1.95 292 130 EHR SV -0.012 Ø I.08e+03 I.72e+01 12 NN09 1.95 292 130 EHR SV -0.012 Ø I.08e+03 1.72e+01 12 NN09 1.54 245 138 EHR SV 0.028 Ø I.08e+03 1.72e+01 14 NN17 1.54 245 138 EHR SV 0.028 Ø I.08e+02 1.95e+01 1 NM42 PSV 2 40.25e+02 2.14e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+01 I.08e+03 I.07e+03 I.08e+03 I.0	10 NN09	1.95	292	130	EHU	Р	0.010	✓ +		✓ 9.92e+00	2.63e+01				
12 NN09 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 1.98 1.99 <	11 NN09	1.95	292	130	EHR	sv	-0.012	✓ +		✓ 1.08e+03	1.72e+01				
13 NN17 1.54 245 138 EHU P -0.003 \$\vee + \$\vee 3.22e+01 2.49e+01 14 NN17 1.54 245 138 EHU \$\vee V 0.028 \$\vee + \$\vee 3.86e+02 1.95e+01 1 NM42 P.SV 2 \$\vee V 0.028 \$\vee + \$\vee 3.86e+02 2.14e+01 1 NM42 P.SV 2 \$\vee V 0.021 \$\vee - \$\vee \$\vee A.256e+07 2.14e+01 1 NM42 P.SV 2 \$\vee V 0.021 \$\vee - \$\vee A.256e+07 2.14e+01 1 NM42 P.SH 3 \$\vee V \$\ve	12 NN09	1.95	292	130	EHT	SH	0.025	✓ +		₹ 7.37e+02	1.51e+01				
14 NN17 1.54 243 138 EHR SV 0.028 Ø + Ø 366e+02 1.95e+01 1 NN17 1.54 245 138 EHR SV 0.028 Ø + Ø 366e+02 1.95e+01 1 NM42 PSV PSV 0.027 Ø - Ø - R 25e+02 2.14e+01 1 NM42 PSV 0.007 S NM42 PSV 0.007 5 NN09 Ø PSV 0.007 S NN09 Ø PSV 0.001 6 NN09 Ø PSV 0.001 SV-SH AMPLITUDE RATIOS SV-SH 8 NN17 Ø PSV 0.041 SV-SH SV-SH SV-SH SV-SH 10 NN17 Ø PSV 0.041 SV-SH <	13 NN17	1.54	245	138	EHU	P	-0.003	✓ +		✓ 3.22e+01	2.49e+01				ст. —
Sta Type Penalty 1 NM42 PSV 2 NM42 PSV 3 NM42 SVSH 4 NV07 PSV 6 NN09 PSV 6 NN09 PSV 6 NN09 PSV 6 NN07 PSH 7 NN09 SVSH 8 NN17 PSV 10 NN17 PSV 10 NN17 PSV 11 NN18 PSV 12 NN18 PSV 13 NN18 SVSH 14 NN07 PSU 13 NN18 SVSH 14 NN19 PSV 13 NN18 SVSH 14 NN19 PSV 13 NN18 VSH 14 NN19 PSV 13 NN18 VSH 14 NN19 PSV	14 NN17	1.54	245	138	EHR	SV	0.020	✓ +		✓ 3.66e+02	1.95e+01				
Image Prope Penalty 1 NM42 PSV 2 NM42 PSH 3 NM42 SVSH 4 NO7 PSV 5 NN09 PSV 6 NN09 PSV 7 NN09 PSV 8 NN17 PSV 9 N177 PSV 10 NN17 PSV 10 NN17 PSV 11 NN18 PSV 12 NN18 PSV 13 NN18 PSV 12 NN18 PSV 13 NN18 PSV 14 NN04 PSV	10 1017		240		- HI	SH	0.021	- W		WI -6 258±02	214e±01			P	(P)
1 NM42 P.S4 2 NM42 PSH 3 NM42 SV:SH 4 N007 Ø PSH 6 N009 Ø PSV 6 N009 Ø PSH 7 N009 Ø SV:SH 8 NN17 Ø PSV 9 NN17 Ø PSV 11 NN18 PSV 12 NN18 Ø PSH 13 NN18 Ø VSH 14 NN17 Ø PSV 15 NU9 Ø SV:SH 8 NN17 Ø PSV 10 N17 Ø PSV 11 NN18 Ø VSH 12 NN18 Ø PSH 13 NN18 Ø VSH 14 NN18 Ø VSH 15 NN18 Ø VSH 16 NN17 Ø PSV 12 NN18 Ø VSH 14 NN18 Ø VSH 14 NN18 Ø VSH 15 Ø PSV 16 Ø	Sta	Typ	e ev	Penalty								ш		+ + -	+ + -
2 NM42 1 0.01 3 NM42 5 0.07 5 NN09 Ø PSH 4 NN07 Ø PSH 6 NN09 Ø PSH 6 NN09 Ø PSH 6 NN09 Ø SVSH 8 NN17 Ø PSH 10 NN17 Ø PSH 11 NN18 PSV 12 NN18 Ø PSH 13 NN18 Ø PSH 14 NN19 Ø PSV 12 NN18 Ø PSH 14 NN19 Ø PSV 14 NN19 Ø PSV	1 NM42		оv сн		-							ш		\т/	\ т /
A NNO7 V PSH 0.007 S NNO9 V PSV 6 6 NNO9 V PSV 6 6 NNO9 V SVSH 8 8 NN17 V PSH 0.013 10 NN17 SVSH 111 NN18 PSV 122 113 NN18 V PSH 0.041 13 NN18 V PSH 0.041 13 NN18 V PSH 0.041 14 NN19 PSH 0.041 15 NVSH 14 NN19 PSH 0.041 15 NVSH 14 NV19 PSH 0.041 15 NVSH	2 NM42		VSH		-										
NN09 PSV AMPLITUDE PATIOS 6 NN09 PSH 7 NN09 SVSH 8 NN17 PSV 0.041 9 NN17 PSH 10 NN17 SVSH 11 NN18 PSV 12 NN18 PSN 13 NN18 PSN 14 NN19 PSV	4 NN07	I P:	SH	0.007	-									\mathbf{T}	\mathbf{J}
6 NN09 Ø P:SH AMPLITUDE RATIOS 7 NN09 Ø SV:SH B 8 NN17 Ø P:SV 0.041 9 N177 Ø P:SH 0.013 10 NN17 Ø P:SV 0.041 11 NN18 Ø P:SH 0.041 12 NN18 Ø P:SH 0.041 13 NN18 Ø P:SH 0.041 14 NN19 Ø P:SV Image: Control of the second	5 NN09	I P:	sv	0.007	-										
7 NN09 Ø SV:SH 8 NN17 Ø PSV 9 N17 Ø PSH 10 NN17 SV:SH 11 NN18 PSV 12 NN18 Ø PSH 13 NN18 SV:SH 14 NN19 PSH vir NN24 Ø PSV	6 NN09	I P:	SH		-									AMPLITUDE RATIOS	
8 NN17 V PSV 0.041 9 NN17 V PSH 0.013 10 NN17 SVSH 11 11 NN18 PSV 12 12 NN18 V PSH 0.041 13 NN18 SVSH 14 14 NN19 PSH 0.041 13 NN18 SVSH 14 14 NN19 PSH 14 17 PSU 14 14	7 NN09	√ sv	V:SH		-										
9 NN17 V P:SH 0.013 10 NN17 SV:SH 11 NN18 P:SV 12 NN18 V P:SH 0.041 13 NN18 SV:SH 14 NN19 P:SH 14 NN19 P:SH 15 V:SH 15 V:SH 16 V:SH 17 V:SH 17 V:SH 17 V:SH 18 V P:SH 18 V P:SH 17 V:SH 19 V:SH 10 V:SH 1	8 NN17	P:	sv	0.041	1								DICU	D.C.	CV/CL
10 NN17 SVSH 11 NN18 PSV 12 NN18 V PSH 0.041 13 NN18 SVSH 14 NN19 PSH 15 NN24 V PSV	9 NN17	🗹 P:	SH	0.013	1								r.sr	r.sv	34.34
11 NN18 PSV 12 NN18 V PSH 0.041 13 NN18 SV:SH 14 NN19 PSH 17 NN24 V PSV	10 NN17	SV	V:SH		1										
12 NN18 V P:SH 0.041 13 NN18 SV:SH 14 NN19 P:SH 14 NN19 V:SH 14 NN19 V:SH 15 NN24 V P:SV	11 NN18	P:	sv		1										
13 NN18 SVSH 14 NN19 PSH 17 NN24 JPSV	12 NN18	🗹 P:	SH	0.041	1									的名称种语言	ALL
14 NN19 PSH 77 NN24 PSV	13 NN18	S	V:SH		1										1998 Production
11 NN24	14 NN19	📄 P:	SH										BALL	18 Jan	
	1 E NN24	J P	sv												



								/Use	rs/foulger/Seis	micProcessin	/Newberry/Data/2014/10/13/	20141013102229.or	
0] 🎍	₩?											
2014 Oct 1 Lat: 43.72 43:43	13 10:22: 66 Lon: 8.596 N	29.084 -121 121:	4 UTC .311 18.654	Depth: 46 W	0.456				Solve		North East North -1.16e-01 -1.39e- East -1.39e-01 -1.17e-0 Down 1.51e-01 5.54e-0	Down 01 1.51e-01 1 5.54e-02 2 7.56e-02	+Crat +Dipo +CLV
					-					1	Scalar M0 = 2.484e-01 T = 0.359 k = -0.169		Crack
Sta	2.94	Az 14	106	Chan	Phase	Resid 0.012	Polarity	Penalty	Amp	Freq			
	0.90	105	151	EHU7	P	0.037	v -				Total Penalty = 0.173		
2 NM22	0.22	134	173	EHU	P	-0.019	1		1 670+02	1.470+01			
4 NM42	3.70	44	100	EHU	P	0.000	J -		✓ -8 22e+01	1.47C+01		POLARITIES	
5 NM42	3.70	44	100	EHR	sv	0.099	1 -		✓ -2.22e+02	1.51e+01			
6 NN07	2.99	338	104	EHU	Р	-0.004	V -		-2.02e+01	1.44e+01	P olo	SH CT	SV
7 NN07	2.99	338	104	EHT	SH	-0.003	v -		✓ -9.60e+01	1.95e+01			
8 NN09	1.89	293	121	EHU	Р	0.021	√ +		9.55e+00	1.07e+01		(•	
9 NN09	1.89	293	121	EHR	SV	0.012	🗹 +		✓ 1.12e+02	1.51e+01			$\vdash \leftarrow \forall$
10 NN09	1.89	293	121	EHT	SH	0.033	🗹 +		✓ 1.08e+02	3.47e+01	(\cdot , \cdot)	$\langle \gamma \rangle \langle \gamma \rangle$	
11 NN17	1.49	244	132	EHU	Р	-0.005	🗹 +		✓ 7.23e+00	3.03e+01			
12 NN17	1.49	244	132	EHR	sv	0.044			✓ -7.33e+02	1.72e+01		$\mathbf{\mathbf{U}}$	Ŷ
13 NN17	1.49	244	132	EHT	SH	0.017	I -		✓ -3.01e+02	1.62e+01			6T.
14 NN18	1.41	30	135	EHU	Ρ	-0.016	1 -		✓ -6.26e+01	1.42e+01		SN	SE
15 NN18	1.41	30	135	EHT	SH	0.045	v -		✓ -4.16e+02	1.34e+01			
16 NN19	0.97	161	147	EHU	P	0.005	₫ +		9.60e+01	1.79e+01		+ + -	+ + -
Sta	Tur		Panalta										T
1 NM42	P:	sv	renatty	/									
2 NN07	I P:	SH	0.044	-									
3 NN09	✓ P:	sv	0.014	-									
4 NN09	✓ P:	SH		-								AMPLITUDE RATIOS	
5 NN09	√ sv	/:SH	0.037	1									
6 NN17	- P:	sv											
7 NN17	🗹 P:	SH	0.023								P:SHE	P.SY 71	SV:SH 1
8 NN17	S	/:SH		-								- BARREN	
9 NN18	P:	SH		-							Le a Alt	15 15 K	
10 NN19	🗹 P:	SH											
11 NN21	🗹 P:	SH	0.055								KR R R P		VERBER V
12 NN24	🗹 P:	sv									V Starter	A A A A A A A A A A A A A A A A A A A	CB C L
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